

ΠΑΡΑΜΕΤΡΙΚΗ
ΔΙΕΡΕΥΝΗΣΗ
ΛΕΙΤΟΥΡΓΙΚΟΥ
ΠΡΟΒΛΗΜΑΤΟΣ

ΠΡΟΣΑΡΤΗΜΑ Β

ΠΑΡΑΜΕΤΡΙΚΗ
ΔΙΕΡΕΥΝΗΣΗ
ΛΕΙΤΟΥΡΓΙΚΟΥ
ΠΡΟΒΛΗΜΑΤΟΣ

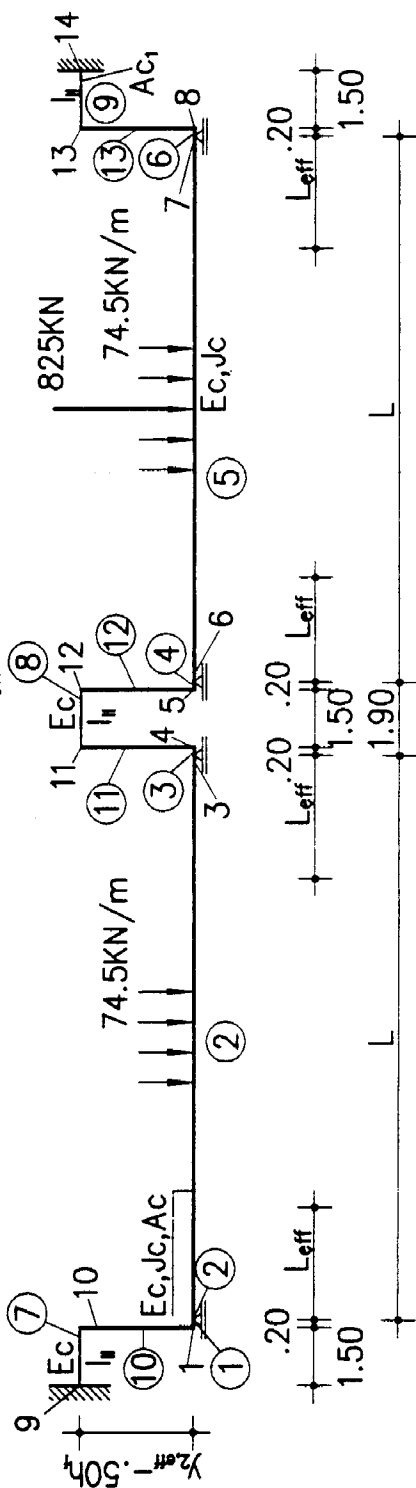
(1)

ΠΡΟΣΑΡΤΗΜΑ Β

208

$$A_{C1} = \frac{1.50}{1.50 + L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$

$$A_{C2} = \frac{1.50}{1.50 + 2L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$



ΠΙΝΑΚΑΣ ΔΕΔΟΜΕΝΩΝ

$L = 33.0m$	$E_c = 32 \text{ GPa}$
$b = 12.0m$	$a = 6.25$
$A_{c,eff} = 5.100m^2$	$g_1 = 30.7kN/m$
$J_{c,eff} = 2.784m$	$q = 43.8kN/m$
$h_b = 2.15m$	$g_1 + q = 74.5kN/m$
$h_{it} = 0.275m$	$Q = 825kN$
$h_{t,eff} = 0.20m$	$A_{st} = 986 \text{ cm}^2 (4\phi 14/75)$
$h_{(np.)} = 0.075m$	$\rho = 4.1\%$
$\chi_{2,eff} = 0.73m$	$A_{sb} = 10.7 \text{ cm}^2/m (\phi 14/15n + \phi 14/15k)$
	$T = -60^\circ / 70^\circ \text{ C}$
	$L_{eff} = L/4$
$\rho_b = 0.006 (\phi 14/150)$	
$I_{II} = 3.544 \alpha g b h_{t,eff}^3 / 12 = 0.1772 \rho_b \approx 0.0011 \text{ m}^4$	

```

1 PROG GENF
2 $ Dat : C:\...\sofistik\dat\it\133\12-7-02a\new.dat  (.#01)  09/11/2002
3 $ Job : 12-7-02a/TEGOS:002367 13:58
4 HEAD
5 HEAD
6 PAGE LINE 75 LANO 1 LANI 1 MARG 3 FIRS 1
7 ECHO FULL FULL
8 SYST OPTI NO
9 SYST SPAC
10 CONC 1 B 35 EC 32000
11 CONC 2 B 35 EC 32000
12 STEE 3 BST 500
13 LET#1 33.00
14 NODE 1 1.50 0.00 0.58
15 2 1.70 ==
16 3 1.70+#1 ==
17 4 1.70+#1+0.20 ==
18 5 1.70+#1+1.70 ==
19 6 1.70+#1+1.90 ==
20 7 1.70+#1+1.90+#1 ==
21 8 1.70+#1+1.90+#1+0.20 ==
22 9 0.00 0.00 0.00
23 10 1.50 ==
24 11 1.70+#1+0.20
25 12 1.70+#1+1.70
26 13 1.70+#1+1.90+#1+0.20
27 14 1.70+#1+1.90+#1+1.70
28 NODE (1 4 3) FIX PYM
29 NODE (2 3 1) FIX XPYM
30 NODE (5 8 3) FIX PYM
31 NODE (6 7 1) FIX XPYM
32 NODE (10 13 1) FIX PYM
33 NODE (9 14 5) FIX PPM
34 NODE 10 FIX KF NREF 2
35 1 FIX KF NREF 2
36 11 FIX KF NREF 3
37 4 FIX KF NREF 3
38 12 FIX KF NREF 6
39 5 FIX KF NREF 6
40 13 FIX KF NREF 7
41 8 FIX KF NREF 7
42 $
43 SVAL NO 2 MNO 1 A 5.10 IY 2.784
44 SVAL NO 3 MNO 2 A 0.1138 IY 0.0011
45 SVAL NO 4 MNO 2 A 0.0616 IY 0.0011
46 $
47 BEAM 2 2 3 NCS 2
48 5 6 7 NCS 2
49 7 9 10 NCS 3
50 8 11 12 NCS 4
51 9 13 14 NCS 3
52 BSEC 2 8.10 2 SECT
53 BSEC 2 24.90 2 SECT
54 BSEC 5 8.10 2 SECT
55 BSEC 5 24.90 2 SECT
56 END

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N O D A L C O O R D I N A T E S A N D S U P P O R T S

Number	X[m]	Y[m]	Z[m]	eq.PX	eq.PY	eq.PZ	eq.MX	eq.MY	eq.MZ	eq.MB
1	1.500	.000	.580	*	*	*	*	*	*	*
2	1.700	.000	.580		PY	PZ	MX		MZ	
3	34.700	.000	.580		PY	PZ	MX		MZ	
4	34.900	.000	.580	*	*	*	*	*	*	*
5	36.400	.000	.580	*	*	*	*	*	*	*
6	36.600	.000	.580		PY	PZ	MX		MZ	
7	69.600	.000	.580		PY	PZ	MX		MZ	
8	69.800	.000	.580	*	*	*	*	*	*	*
9	.000	.000	.000	PX	PY	PZ	MX	MY	MZ	
10	1.500	.000	.000	*	*	*	*	*	*	*
11	34.900	.000	.000	*	*	*	*	*	*	*
12	36.400	.000	.000	*	*	*	*	*	*	*
13	69.800	.000	.000	*	*	*	*	*	*	*
14	71.300	.000	.000	PX	PY	PZ	MX	MY	MZ	

MIN	.000	.000	.000							
MAX	71.300	.000	.580							

K I N E M A T I C C O N S T R A I N T S

Node	LV	type	reference	dx	dy	dz	df
10	1	KF	2	-.200	.000	-.580	
1	1	KF	2	-.200	.000	.000	
11	1	KF	3	.200	.000	-.580	
4	1	KF	3	.200	.000	.000	
12	1	KF	6	-.200	.000	-.580	
5	1	KF	6	-.200	.000	.000	
13	1	KF	7	.200	.000	-.580	
8	1	KF	7	.200	.000	.000	

M A T E R I A L S

No. 1 B 35 (DIN 1045)

Young-module	32000	[MPa]	Safetyfactor	1.00	[-]
Poisson-Ratio	.20	[-]	Strength fc	23.00	[MPa]
Shear-module	13333	[MPa]	Nominal Strength	35.00	[MPa]
Compress.module	17778	[MPa]	Tens.Str. fctm	3.21	[MPa]
Weight	25.0	[kN/m3]	Tens.Str. fctk	2.67	[MPa]
Weight buoyancy	.0	[kN/m3]	Tens.Str. fctk	3.85	[MPa]
Temperat. coeff.	1.00E-05	[-]	Compr.fail.ener.	20.00	[kN/m]
			Tens.fail.energ.	.05	[kN/m]
			Friction crack	.20	[-]

No. 2 B 35 (DIN 1045)

Young-module	32000	[MPa]	Safetyfactor	1.00	[-]
Poisson-Ratio	.20	[-]	Strength fc	23.00	[MPa]
Shear-module	13333	[MPa]	Nominal Strength	35.00	[MPa]
Compress.module	17778	[MPa]	Tens.Str. fctm	3.21	[MPa]
Weight	25.0	[kN/m3]	Tens.Str. fctk	2.67	[MPa]
Weight buoyancy	.0	[kN/m3]	Tens.Str. fctk	3.85	[MPa]
Temperat. coeff.	1.00E-05	[-]	Compr.fail.ener.	20.00	[kN/m]
			Tens.fail.energ.	.05	[kN/m]
			Friction crack	.20	[-]

No. 3 BST 500 (DIN 1045)

Young-module	210000	[MPa]	Safetyfactor	1.00	[-]
Poisson-Ratio	.30	[-]	Yield stress fy	500.00	[MPa]
Shear-module	80769	[MPa]	Tensile str. ft	550.00	[MPa]
Compress.module	175000	[MPa]	Plastic strain	10.00	[o/o]
Weight	78.5	[kN/m3]	Relaxation .70ft	.00	[-]
Weight buoyancy	.0	[kN/m3]	Relaxation .55ft	.00	[-]
Temperat. coeff.	1.20E-05	[-]	nat. bond coeff.	200.00	[-]
			EC2 bondcoeff K1	.80	[-]
			Hardening module	.00	[MPa]

C R O S S S E C T I O N S - S T A T I C P R O P E R T I E S									
No	MNo	A[m2]	Ay/Az/Ayz	Iy/Iz/Iyz	ys/zs	y/z-sc	modules	gam	
	MNs	It[m4]	[m2]	[m4]	[m]	[m]	[MPa]	[kN/m3]	
1	1	1.0000E+02		8.333E+02	.000	.000	32000	25.0	
	3	1.400E+03		8.333E+02	.000	.000	13333		
		= 1000./1000. [cm]							
		= (H-AS 100./100. [cm])							
2	1	5.1000E+00		2.784E+00	.000	.000	32000	25.0	
		3.078E+00		2.784E+00	.000	.000	13333		
3	2	1.1380E-01		1.100E-03	.000	.000	32000	25.0	
		1.931E-03		1.100E-03	.000	.000	13333		
4	2	6.1600E-02		1.100E-03	.000	.000	32000	25.0	
		1.658E-04		1.100E-03	.000	.000	13333		

Summary of used sections in system

No.	Total Length	Total Volume	max. length	Title
	[m]	[t]	[m]	
1	.000	.000	.000	1000./1000. [cm]
2	66.000	841.500	33.000	
3	3.000	.854	1.500	
4	1.500	.231	1.500	

B E A M E L E M E N T S									
beam	node	x[m]	NoS	Ref	hinges	direction local y-axis			
2	2	.000	2			.000	1.000	.000	
		8.100	2						
		24.900	2						
	3	33.000	2						
5	6	.000	2			.000	1.000	.000	
		8.100	2						
		24.900	2						
	7	33.000	2						
7	9	.000	3			.000	1.000	.000	
	10	1.500	3						
8	11	.000	4			.000	1.000	.000	
	12	1.500	4						
9	13	.000	3			.000	1.000	.000	
	14	1.500	3						

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1 PROG STAR2
2 $ Dat : C:\...\sofistik\dat\it\133\12-7-02a\new.dat (.#03) 09/11/2002
3 $ Job : 12-7-02a/TEGOS:002367 13:58
4 HEAD ENTATIKA MEPEOH
5 PAGE FIRS 1 LINE 75 MARG 3 LANO 1 LANI 1
6 ECHO FULL FULL
7 ECHO NODE FULL
8 CTRL I
9 LC 1 TITL 'ΦOPTIA MONIMA+KINHHTA'
10 UL 2 PZ 74.50
11 UL 5 PZ 74.50
12 SL NO 5 TYPE PZ P 825 A 16.5
13 $
14 LC 2 TITL 'ΦOPT. MON.+KIN.+(-70o C)'
15 UL 2 PZ 74.50
16 UL 5 PZ 74.50
17 SL NO 5 TYPE PZ P 825 A 16.5
18 UL 2 TS -70
19 UL 5 TS -70
20 UL (7 9 1) TS -70
21 END
```

ENTATIKA METEΘH

LOAD CASE 1 ΦOPTIA MONIMA+KINHTA
 load - factor 1.000
 factor dl-x .000
 factor dl-y .000
 factor dl-z .000

BEAM LOADS

Beamno	type	a[m]	l[m]	load1	load2 [dim]	ya[m]	za[m]	ye[m]	ze[m]
2	ULPZ	.000	33.000	74.50	KN/M				
5	SLPZ	16.500		825.00	KN				
5	ULPZ	.000	33.000	74.50	KN/M				

LOAD CASE 2 ΦOPT. MON.+KIN.+(-70o C)
 load - factor 1.000
 factor dl-x .000
 factor dl-y .000
 factor dl-z .000

BEAM LOADS

Beamno	type	a[m]	l[m]	load1	load2 [dim]	ya[m]	za[m]	ye[m]	ze[m]
2	ULPZ	.000	33.000	74.50	KN/M				
2	ULTS	.000	33.000	-70.00	K				
5	SLPZ	16.500		825.00	KN				
5	ULPZ	.000	33.000	74.50	KN/M				
5	ULTS	.000	33.000	-70.00	K				
7	ULTS	.000	1.500	-70.00	K				
8	ULTS	.000	1.500	-70.00	K				
9	ULTS	.000	1.500	-70.00	K				

Analysis has been selected:
 for group: 0

KINEMATIC CONSTRAINTS

Node	LV	type	reference	dx	dy	dz	df
10	1	KF	2	-.200	.000	-.580	
1	1	KF	2	-.200	.000	.000	
11	1	KF	3	.200	.000	-.580	
4	1	KF	3	.200	.000	.000	
12	1	KF	6	-.200	.000	-.580	
5	1	KF	6	-.200	.000	.000	
13	1	KF	7	.200	.000	-.580	
8	1	KF	7	.200	.000	.000	

NODAL COORDINATES AND SUPPORTS

Number	X[m]	Y[m]	Z[m]	eq.PX	eq.PY	eq.PZ	eq.MX	eq.MY	eq.MZ
1	1.500	.000	.580	-7	-8	-9	-10	-11	-12
2	1.700	.000	.580	1	PY	PZ	MX	2	MZ
3	34.700	.000	.580	3	PY	PZ	MX	4	MZ
4	34.900	.000	.580	-19	-20	-21	-22	-23	-24
5	36.400	.000	.580	-31	-32	-33	-34	-35	-36
6	36.600	.000	.580	5	PY	PZ	MX	6	MZ
7	69.600	.000	.580	7	PY	PZ	MX	8	MZ
8	69.800	.000	.580	-43	-44	-45	-46	-47	-48
9	.000	.000	.000	PX	PY	PZ	MX	MY	MZ
10	1.500	.000	.000	-1	-2	-3	-4	-5	-6
11	34.900	.000	.000	-13	-14	-15	-16	-17	-18
12	36.400	.000	.000	-25	-26	-27	-28	-29	-30
13	69.800	.000	.000	-37	-38	-39	-40	-41	-42
14	71.300	.000	.000	PX	PY	PZ	MX	MY	MZ
MIN	.000	.000	.000		-48				
MAX	71.300	.000	.580		8				

MATERIALS

ENTATIKA MEFEQH

M A T E R I A L S

No. 1 B 35 (DIN 1045)

Young-module	32000	[MPa]	Safetyfactor	1.00	[-]
Poisson-Ratio	.20	[-]	Strength fc	23.00	[MPa]
Shear-module	13333	[MPa]	Nominal Strength	35.00	[MPa]
Compress.module	17778	[MPa]	Tens.Str. fctm	3.21	[MPa]
Weight	25.0	[kN/m3]	Tens.Str. fctk	2.67	[MPa]
Weight buoyancy	.0	[kN/m3]	Tens.Str. fctk	3.85	[MPa]
Temperat. coeff.	1.00E-05	[-]	Compr.fail.ener.	20.00	[kN/m]
			Tens.fail.energ.	.05	[kN/m]
			Friction crack	.20	[-]

No. 2 B 35 (DIN 1045)

Young-module	32000	[MPa]	Safetyfactor	1.00	[-]
Poisson-Ratio	.20	[-]	Strength fc	23.00	[MPa]
Shear-module	13333	[MPa]	Nominal Strength	35.00	[MPa]
Compress.module	17778	[MPa]	Tens.Str. fctm	3.21	[MPa]
Weight	25.0	[kN/m3]	Tens.Str. fctk	2.67	[MPa]
Weight buoyancy	.0	[kN/m3]	Tens.Str. fctk	3.85	[MPa]
Temperat. coeff.	1.00E-05	[-]	Compr.fail.ener.	20.00	[kN/m]
			Tens.fail.energ.	.05	[kN/m]
			Friction crack	.20	[-]

No. 3 BST 500 (DIN 1045)

Young-module	210000	[MPa]	Safetyfactor	1.00	[-]
Poisson-Ratio	.30	[-]	Yield stress fy	500.00	[MPa]
Shear-module	80769	[MPa]	Tensile str. ft	550.00	[MPa]
Compress.module	175000	[MPa]	Plastic strain	10.00	[o/o]
Weight	78.5	[kN/m3]	Relaxation .70ft	.00	[-]
Weight buoyancy	.0	[kN/m3]	Relaxation .55ft	.00	[-]
Temperat. coeff.	1.20E-05	[-]	nat. bond coeff.	200.00	[-]
			EC2 bondcoeff K1	.80	[-]
			Hardening module	.00	[MPa]

C R O S S - S E C T I O N S S T A T I C P R O P E R T I E S

No	MNo	A[m2]	Ay/Az/Ayz	Iy/Iz/Iyz	ys/zs	y/z-sc	modules	gam
	MNs	It[m4]	[m2]	[m4]	[m]	[m]	[MPa]	[kN/m3]
1	1	1.0000E+02		8.333E+02	.000	.000	32000	25.0
	3	1.400E+03		8.333E+02	.000	.000	13333	
		= 1000./1000. [cm]						
		= (H-AS 100./100. [cm])						
2	1	5.1000E+00		2.784E+00	.000	.000	32000	25.0
		3.078E+00		2.784E+00	.000	.000	13333	
3	2	1.1380E-01		1.100E-03	.000	.000	32000	25.0
		1.931E-03		1.100E-03	.000	.000	13333	
4	2	6.1600E-02		1.100E-03	.000	.000	32000	25.0
		1.658E-04		1.100E-03	.000	.000	13333	

B E A M E L E M E N T S

beam	node	x[m]	NoS	Ref	hinges	direction	local	y-axis
2	2	.000	2			.000	1.000	.000
		8.100	2					
		24.900	2					
	3	33.000	2					
5	6	.000	2			.000	1.000	.000
		8.100	2					
		24.900	2					
	7	33.000	2					
7	9	.000	3			.000	1.000	.000
	10	1.500	3					
8	11	.000	4			.000	1.000	.000
	12	1.500	4					
9	13	.000	3			.000	1.000	.000
	14	1.500	3					

ENTATIKA METEΘH

linear results Loadfactor 1.00

BEAM FORCES AND MOMENTS

Loadcase	1	ΦOPTIA MONIMA+KINHHTA					
beam	X	N	Q-Y	Q-Z	M-T	M-Y	M-Z
No	[m]	[kN]	[kN]	[kN]	[kNm]	[kNm]	[kNm]
2	.000	1600.3	.0	1233.8	.00	-1073.17	.00
	8.100	1600.3	.0	630.3	.00	6476.38	.00
	24.90	1600.3	.0	-621.3	.00	6552.28	.00
	33.00	1600.3	.0	-1224.7	.00	-924.08	.00
5	.000	1600.3	.0	1638.9	.00	-1061.47	.00
	8.100	1600.3	.0	1035.4	.00	9769.38	.00
	16.50	1600.3	.0	409.6	.00	15838.54	.00
	16.50	1600.3	.0	-415.4	.00	15838.54	.00
	24.90	1600.3	.0	-1041.2	.00	9720.97	.00
	33.00	1600.3	.0	-1644.6	.00	-1156.59	.00
7	.000	1600.3	.0	-126.3	.00	69.82	.00
	1.500	1600.3	.0	-126.3	.00	-119.69	.00
8	.000	1600.3	.0	-72.3	.00	-10.34	.00
	1.500	1600.3	.0	-72.3	.00	-118.81	.00
9	.000	1600.3	.0	199.1	.00	-188.57	.00
	1.500	1600.3	.0	199.1	.00	110.00	.00

BEAM DISPLACEMENTS

Loadcase	1	ΦOPTIA MONIMA+KINHHTA					
beam	X	U	V-Y	V-Z	PHI-X	PHI-Y	PHI-Z
No	[m]	[mm]	[mm]	[mm]	[mrad]	[mrad]	[mrad]
2	.000	.043	.000	.000	.000	-1.063	.000
	8.100	.122	.000	7.926	.000	-.780	.000
	24.90	.287	.000	7.954	.000	.779	.000
	33.00	.366	.000	.000	.000	1.072	.000
5	.000	-.012	.000	.000	.000	-1.680	.000
	8.100	.068	.000	12.520	.000	-1.247	.000
	16.50	.150	.000	18.152	.000	.001	.000
	16.50	.150	.000	18.152	.000	.001	.000
	24.90	.232	.000	12.501	.000	1.248	.000
	33.00	.312	.000	.000	.000	1.674	.000
7	.000	.000	.000	.000	.000	.000	.000
	1.500	.659	.000	-.213	.000	-1.063	.000
8	.000	-.255	.000	-.214	.000	1.072	.000
	1.500	.963	.000	-.336	.000	-1.680	.000
9	.000	-.659	.000	-.335	.000	1.674	.000
	1.500	.000	.000	.000	.000	.000	.000

NODAL REACTIONS

Loadcase	1	ΦOPTIA MONIMA+KINHHTA				
nodes	P-X	P-Y	P-Z	M-X	M-Y	M-Z
No	[kN]	[kN]	[kN]	[kNm]	[kNm]	[kNm]
2	.0	.0	-1360.1	.00	.00	.00
3	.0	.0	-1152.4	.00	.00	.00
6	.0	.0	-1711.2	.00	.00	.00
7	.0	.0	-1843.7	.00	.00	.00
9	-1600.3	.0	126.3	.00	-69.82	.00
14	1600.3	.0	199.1	.00	110.00	.00

NODAL DISPLACEMENTS

Loadcase	1	ΦOPTIA MONIMA+KINHHTA				
nodes	V-X	V-Y	V-Z	PHI-X	PHI-Y	PHI-Z
No	[mm]	[mm]	[mm]	[mrad]	[mrad]	[mrad]
1	.043	.000	-.213	.000	-1.063	.000
2	.043	.000	.000	.000	-1.063	.000
3	.366	.000	.000	.000	1.072	.000
4	.366	.000	-.214	.000	1.072	.000
5	-.012	.000	-.336	.000	-1.680	.000
6	-.012	.000	.000	.000	-1.680	.000
7	.312	.000	.000	.000	1.674	.000

ENTATIKA METEΘH

N O D A L D I S P L A C E M E N T S

Loadcase	1	ΦOPTIA MONIMA+KINHΤA				
nodes	V-X	V-Y	V-Z	PHI-X	PHI-Y	PHI-Z
No	[mm]	[mm]	[mm]	[mrad]	[mrad]	[mrad]
8	.312	.000	-.335	.000	1.674	.000
9	.000	.000	.000	.000	.000	.000
10	.659	.000	-.213	.000	-1.063	.000
11	-.255	.000	-.214	.000	1.072	.000
12	.963	.000	-.336	.000	-1.680	.000
13	-.659	.000	-.335	.000	1.674	.000
14	.000	.000	.000	.000	.000	.000

E L I M I N A T E D F O R C E S F R O M C O N S T R A I N T S

Loadcase	1	ΦOPTIA MONIMA+KINHΤA					
Nodeno	PX[kN]	PY[kN]	PZ[kN]	MX[kNm]	MY[kNm]	MZ[kNm]	MB[kNm2]
1	.0	.0	.0	.00	.00	.00	
4	.0	.0	.0	.00	.00	.00	
5	.0	.0	.0	.00	.00	.00	
8	.0	.0	.0	.00	.00	.00	
10	1600.3	.0	-126.3	.00	-119.69	.00	
11	-1600.3	.0	72.3	.00	10.34	.00	
12	1600.3	.0	-72.3	.00	-118.81	.00	
13	-1600.3	.0	-199.1	.00	188.57	.00	

S U M

	P-X [kN]	P-Y [kN]	P-Z [kN]
Loads	.0	.0	5742.0
Reactions	.0	.0	-5742.0

ENTATIKA MEPEOH

linear results Loadfactor 1.00

B E A M F O R C E S A N D M O M E N T S

Loadcase 2 ΦOPT. MON.+KIN.+(-70o C)

beam	X	N	Q-Y	Q-Z	M-T	M-Y	M-Z
No	[m]	[kN]	[kN]	[kN]	[kNm]	[kNm]	[kNm]
2	.000	23688.3	.0	1227.5	.00	-13566.8	.00
	8.100	23688.3	.0	624.0	.00	-6068.19	.00
	24.90	23688.3	.0	-627.6	.00	-6097.99	.00
	33.00	23688.3	.0	-1231.0	.00	-13625.3	.00
5	.000	23688.3	.0	1645.2	.00	-13762.7	.00
	8.100	23688.3	.0	1041.7	.00	-2880.88	.00
	16.50	23688.3	.0	415.9	.00	3241.11	.00
	16.50	23688.3	.0	-409.1	.00	3241.11	.00
	24.90	23688.3	.0	-1034.9	.00	-2823.61	.00
	33.00	23688.3	.0	-1638.3	.00	-13650.2	.00
7	.000	23688.3	.0	150.3	.00	-83.06	.00
	1.500	23688.3	.0	150.3	.00	142.39	.00
8	.000	23688.3	.0	-72.3	.00	99.46	.00
	1.500	23688.3	.0	-72.3	.00	-9.01	.00
9	.000	23688.3	.0	-77.6	.00	73.51	.00
	1.500	23688.3	.0	-77.6	.00	-42.88	.00

B E A M D I S P L A C E M E N T S

Loadcase 2 ΦOPT. MON.+KIN.+(-70o C)

beam	X	U	V-Y	V-Z	PHI-X	PHI-Y	PHI-Z
No	[m]	[mm]	[mm]	[mm]	[mrad]	[mrad]	[mrad]
2	.000	9.441	.000	.000	.000	1.264	.000
	8.100	4.946	.000	-6.314	.000	.409	.000
	24.90	-4.375	.000	-6.325	.000	-.408	.000
	33.00	-8.869	.000	.000	.000	-1.268	.000
5	.000	9.224	.000	.000	.000	.660	.000
	8.100	4.730	.000	-1.760	.000	-.060	.000
	16.50	.069	.000	-1.097	.000	-.002	.000
	16.50	.069	.000	-1.097	.000	-.002	.000
	24.90	-4.592	.000	-1.739	.000	.059	.000
	33.00	-9.086	.000	.000	.000	-.653	.000
7	.000	.000	.000	.000	.000	.000	.000
	1.500	8.707	.000	.253	.000	1.264	.000
8	.000	-8.134	.000	.254	.000	-1.268	.000
	1.500	8.842	.000	.132	.000	.660	.000
9	.000	-8.707	.000	.131	.000	-.653	.000
	1.500	.000	.000	.000	.000	.000	.000

N O D A L R E A C T I O N S

Loadcase 2 ΦOPT. MON.+KIN.+(-70o C)

nodes	P-X	P-Y	P-Z	M-X	M-Y	M-Z
No	[kN]	[kN]	[kN]	[kNm]	[kNm]	[kNm]
2	.0	.0	-1077.2	.00	.00	.00
3	.0	.0	-1158.7	.00	.00	.00
6	.0	.0	-1717.5	.00	.00	.00
7	.0	.0	-1560.7	.00	.00	.00
9	-23688.	.0	-150.3	.00	83.06	.00
14	23688.3	.0	-77.6	.00	-42.88	.00

N O D A L D I S P L A C E M E N T S

Loadcase 2 ΦOPT. MON.+KIN.+(-70o C)

nodes	V-X	V-Y	V-Z	PHI-X	PHI-Y	PHI-Z
No	[mm]	[mm]	[mm]	[mrad]	[mrad]	[mrad]
1	9.441	.000	.253	.000	1.264	.000
2	9.441	.000	.000	.000	1.264	.000
3	-8.869	.000	.000	.000	-1.268	.000
4	-8.869	.000	.254	.000	-1.268	.000
5	9.224	.000	.132	.000	.660	.000
6	9.224	.000	.000	.000	.660	.000
7	-9.086	.000	.000	.000	-.653	.000

ENTATIKA MEPEOH

N O D A L D I S P L A C E M E N T S

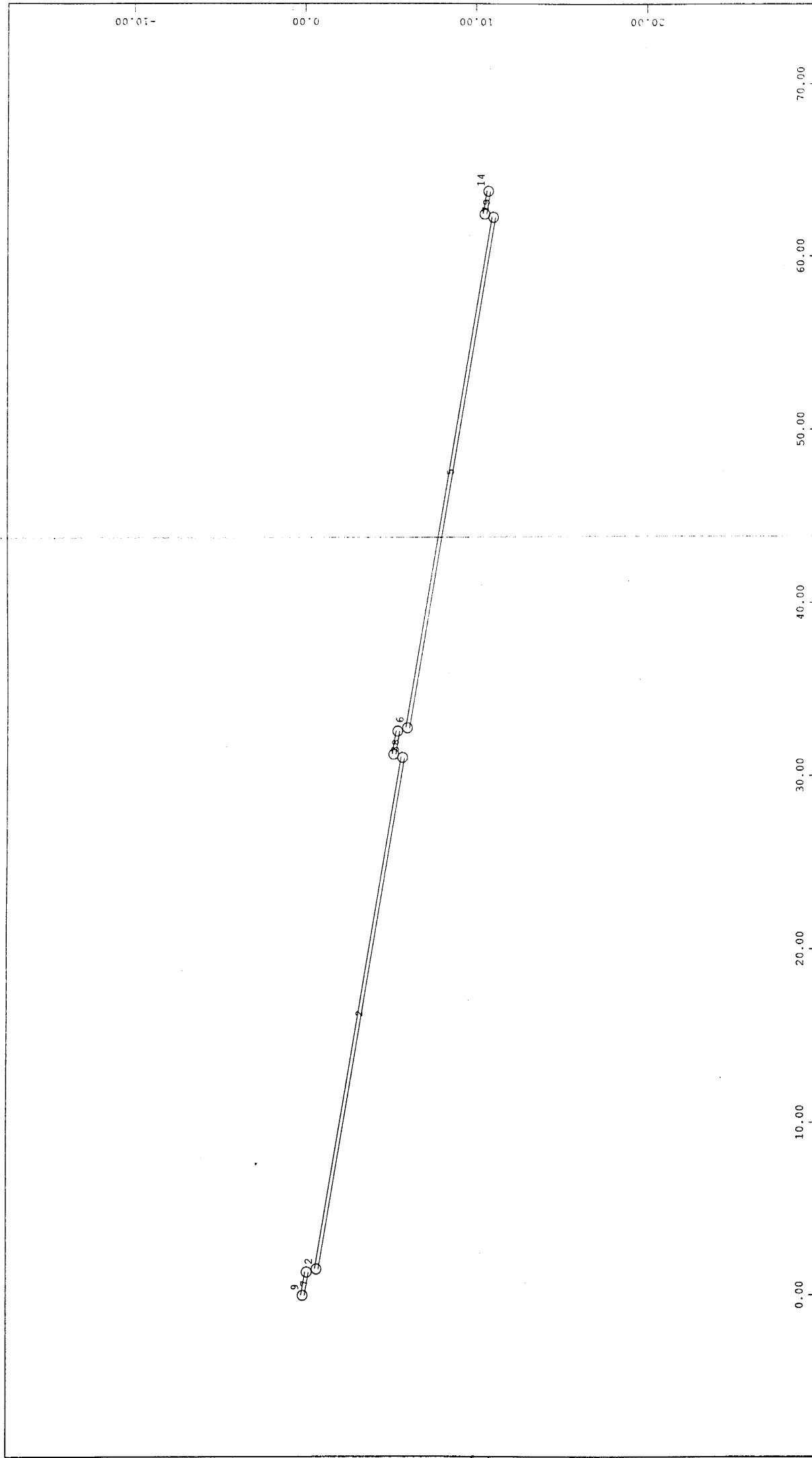
Loadcase	2	ΦOPT. MON.+KIN.+(-70o C)				
nodes	V-X	V-Y	V-Z	PHI-X	PHI-Y	PHI-Z
No	[mm]	[mm]	[mm]	[mrad]	[mrad]	[mrad]
8	-9.086	.000	.131	.000	-.653	.000
9	.000	.000	.000	.000	.000	.000
10	8.707	.000	.253	.000	1.264	.000
11	-8.134	.000	.254	.000	-1.268	.000
12	8.842	.000	.132	.000	.660	.000
13	-8.707	.000	.131	.000	-.653	.000
14	.000	.000	.000	.000	.000	.000

E L I M I N A T E D F O R C E S F R O M C O N S T R A I N T S

Loadcase	2	ΦOPT. MON.+KIN.+(-70o C)					
Nodeno	PX[kN]	PY[kN]	PZ[kN]	MX[kNm]	MY[kNm]	MZ[kNm]	MB[kNm2]
1	.0	.0	.0	.00	.00	.00	
4	.0	.0	.0	.00	.00	.00	
5	.0	.0	.0	.00	.00	.00	
8	.0	.0	.0	.00	.00	.00	
10	23688.3	.0	150.3	.00	142.39	.00	
11	-23688.3	.0	72.3	.00	-99.46	.00	
12	23688.3	.0	-72.3	.00	-9.01	.00	
13	-23688.3	.0	77.6	.00	-73.51	.00	

S U M

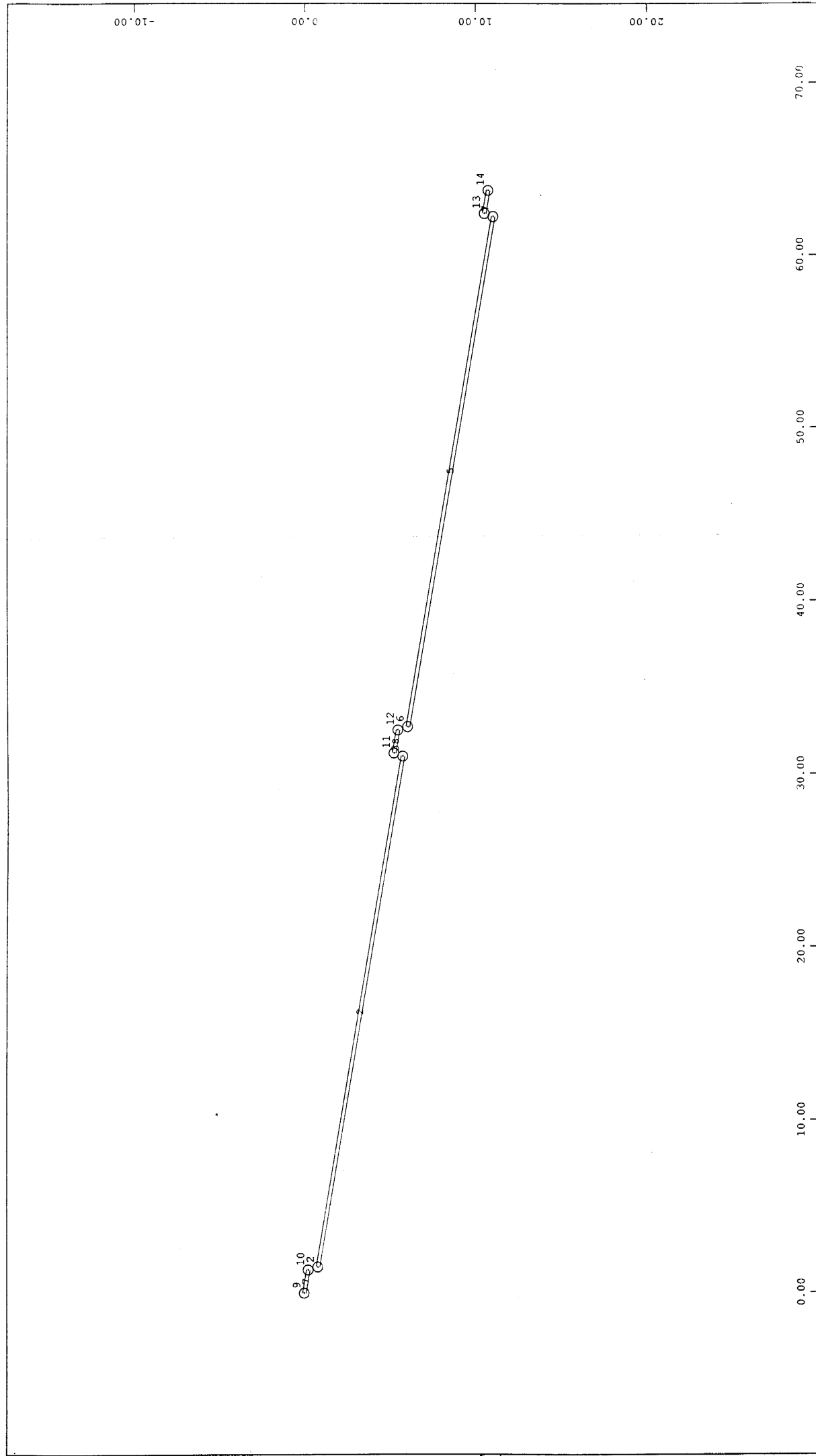
	P-X [kN]	P-Y [kN]	P-Z [kN]
Loads	.0	.0	5742.0
Reactions	.0	.0	-5742.0



FINITE ELEMENT DISCRETIZATION
SECTOR OF SYSTEM, ELEMENT GROUP 0 1
ELEMENT NUMBERS

x
y z

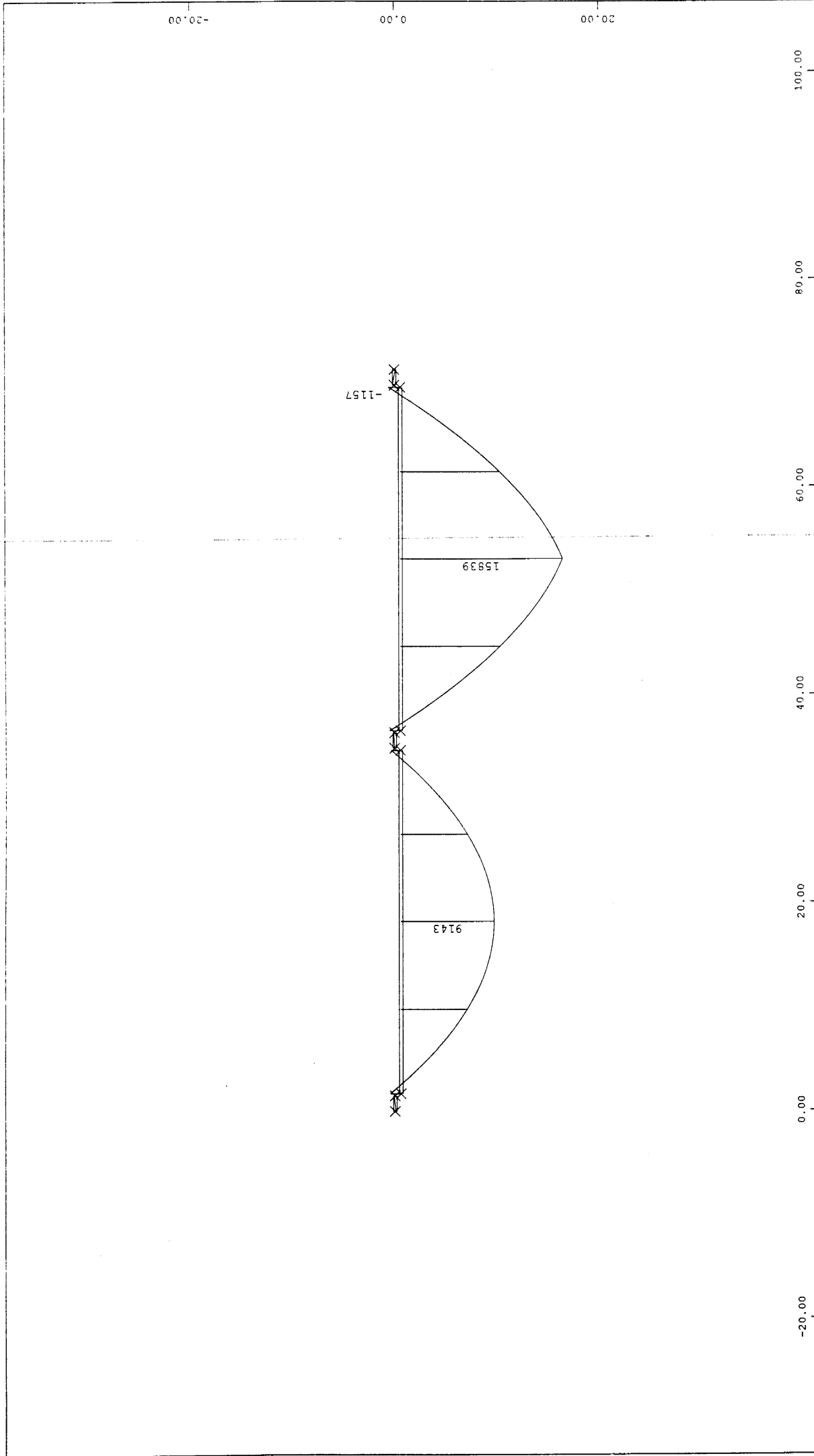
M 1 : 300
X : 0.907
Y : 0.539
Z : 0.942

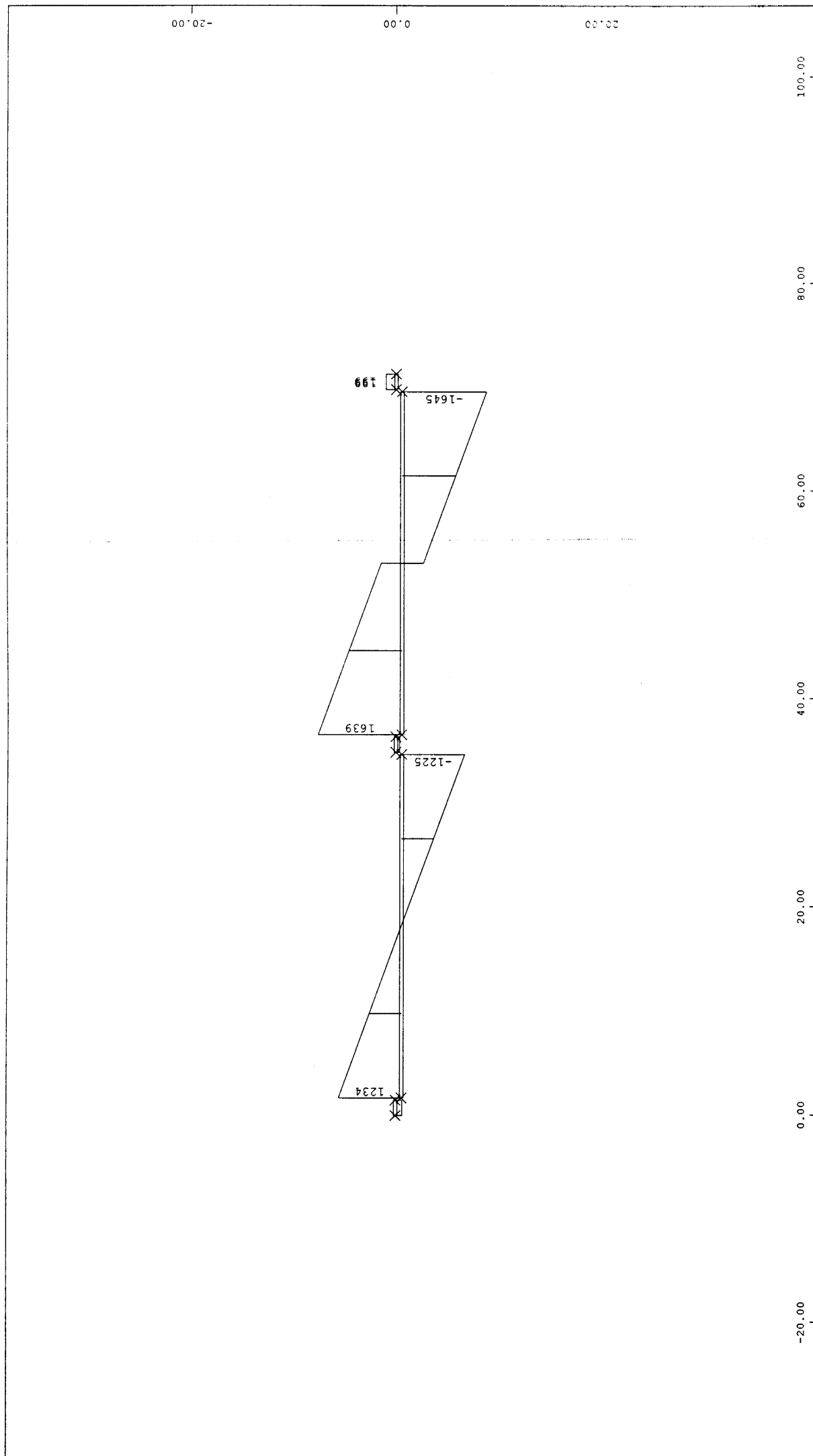


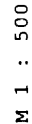
FINITE ELEMENT DISCRETIZATION
SECTOR OF SYSTEM, ELEMENT GROUP 0 1
NODE NUMBERS



M 1 : 300
X : 0.907
Y : 0.539
Z : 0.942







INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
-----BEAM NORMAL FORCES LC 1 LOAD CASE 1 1 CM = 300.0 kN

ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ (ΔΙΑΔΟΧΙΚΩΝ ΠΡΟΣΕΓΓΙΣΕΩΝ)

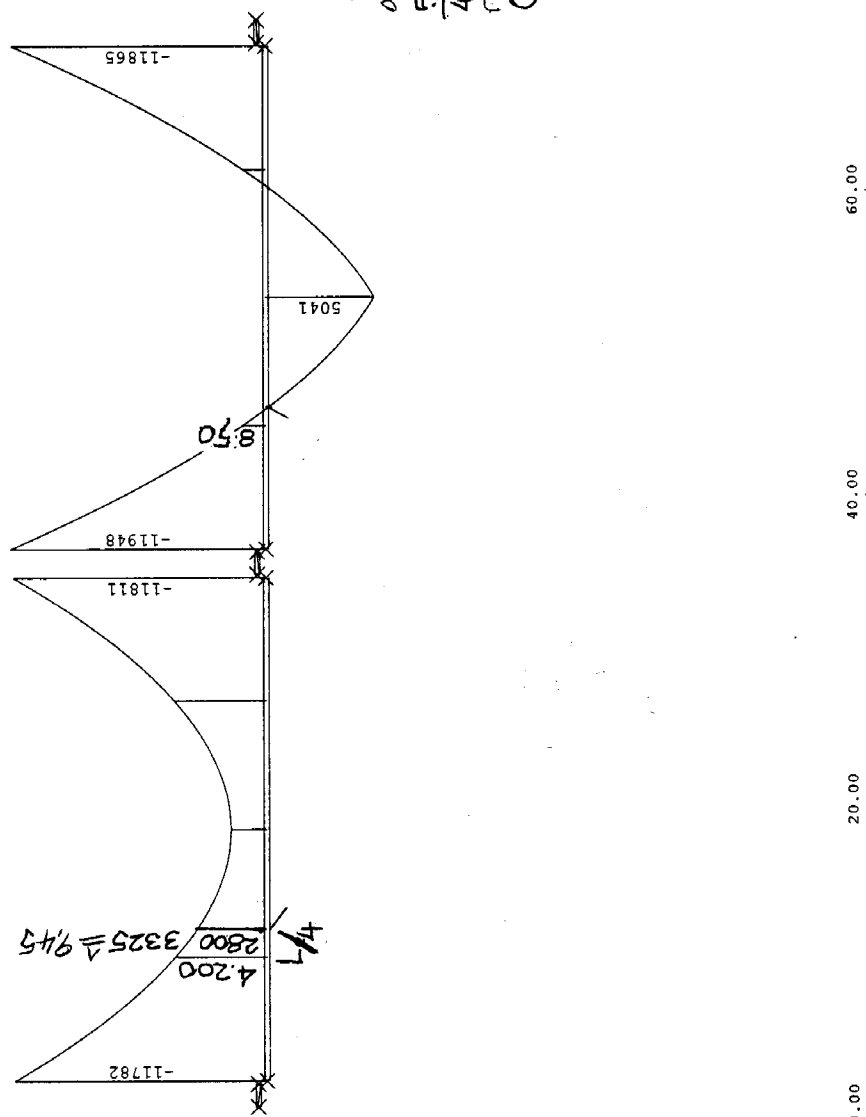
$$\begin{aligned} \text{υπ}\Delta M(x=L_{\text{eff}}) (Y_2=0.5 h_{\text{eff}}) \Delta N &= \frac{J_{\text{eff}}}{Y_2} \left(f_{\text{ctmi}} - \frac{N+\Delta N}{A_{\text{eff}}} \right) \rightarrow 0.5 (4.200+850) + (0.73-0.10) \Delta N_1 = \frac{2.784}{0.73} (3.500 - \frac{20.533}{5.1}) - \frac{2.784}{0.73} \Delta N_1 \rightarrow \Delta N_1 = -60^\circ\text{C} \\ &= -3.283 \text{ kN} \rightarrow N_1 = 20.533 - 3.283 = 17.250 \text{ kN} \rightarrow \frac{17.250}{20.533} = \frac{2 L_{\text{eff}} + 2.65}{2 L_{\text{eff}} + 2.65} \rightarrow L_{\text{eff},1} = 10.0 \text{ m} \rightarrow \text{υπ}\Delta M(x=10.0) = 0.5 (2.800 + \varnothing) = \\ &= 1.400 \text{ kNm} \rightarrow 1.400 + 2.007 = 1.38 \Delta N_2 \rightarrow \Delta N_2 = -2470 \text{ kN} \rightarrow N_2 = 18.060 \text{ kN} \rightarrow \frac{18.060}{20.533} = \frac{2 L_{\text{eff},2} + 2.65}{20.533} \rightarrow L_{\text{eff},2} = 9.55 \text{ m} \rightarrow \text{υπ}\Delta M(x=9.55) = \\ &= 0.5 (3325 + \varnothing) = 1.660 \rightarrow 1.660 + 2.007 = 3670 = 1.38 \Delta N_3 \rightarrow \Delta N_3 = -2660 \text{ kN} \rightarrow N_3 = 17.900 \text{ kN} \rightarrow X_3 = 21.95 \text{ m} \rightarrow L_{\text{eff}} = 9.55 \text{ m} \end{aligned}$$

ΣΥΓΚΡΙΣΗ ΜΕ ΠΕΡΙΠΤΩΣΗ
 $E=31\%$ $T=-60^\circ\text{C}$:

$$\begin{aligned} N &= 17900 \triangleq 16800 \\ L_{\text{eff}} &= 9.55 \triangleq 7.65 \text{ m} \end{aligned}$$

Η 201 = Αύξηση της οπίσθιας κλίσης
 1/3 (από το 3.1 στο 4.1) αντιστοιχεί
 σε αύξηση του N κατά 1/18
 δηλαδή αναλογικά 1:5.

Με άλλα λόγια: Η εφάρμοση της
 τάσης στο ξύλο θα κατα 20%
 ανάξει αύξηση οπίσθιας
 $\frac{5}{4} \times 20 = 25\%$ όπου το 1/5
 προκύπτει από την ένταση
 (απόκλιση).

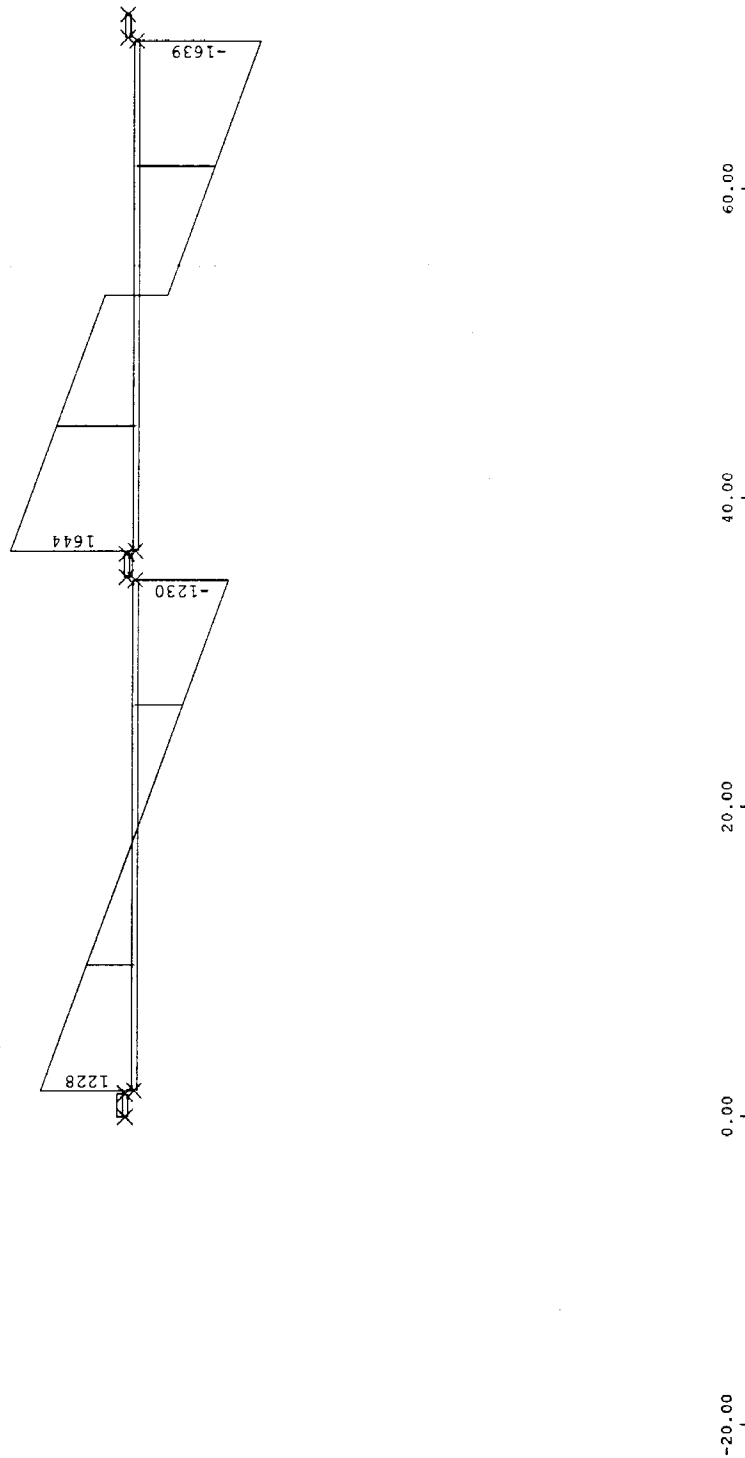


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500

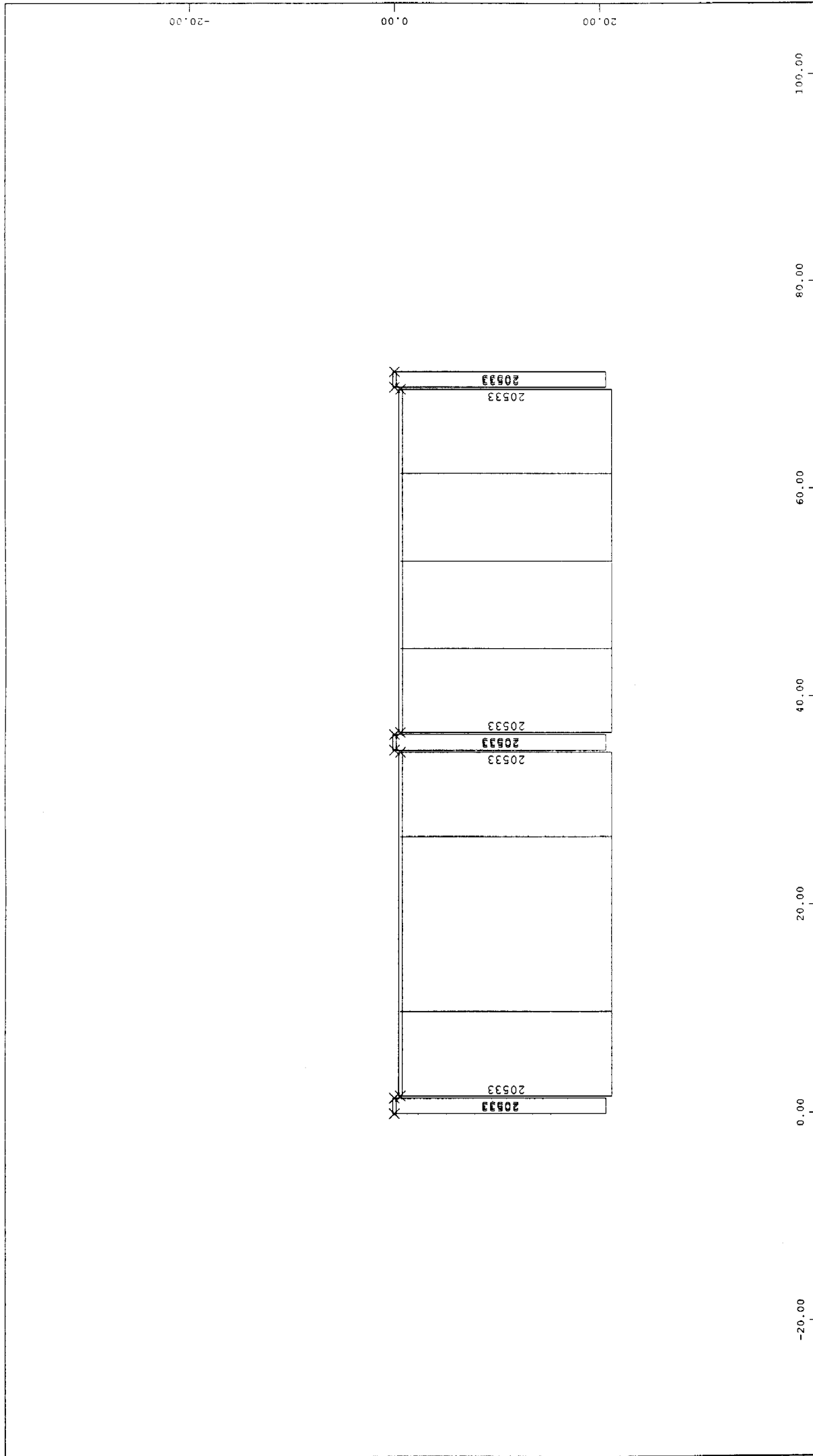


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM SHEAR FORCES QZ LC 2 LOAD CASE 2 1 CM = 1000 kN

M 1 : 500

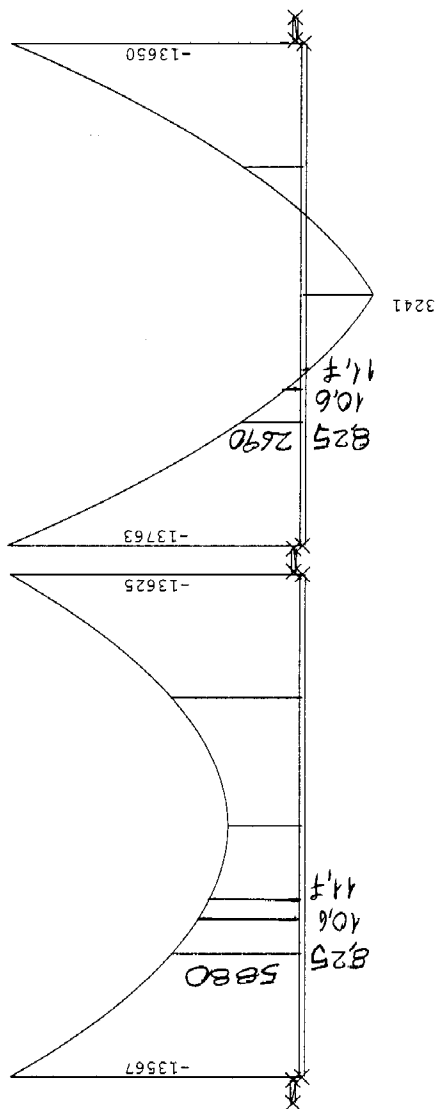


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 ———— BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

M 1 : 500

ΘΑ ΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$\Delta M(x=L/4) + (x_2 - 0.5 h_{p,eff}) \Delta N = W_{2,eff} (f_{ctmi} - \frac{N + \Delta N}{A_{c,eff}}) \rightarrow 0.5(5880 + 2690) + 4366 = -1.38 \Delta N_1 \rightarrow \Delta N_1 = -6270$
 $N_1 = 23688 - 6270 = 17420 \text{ kN} \rightarrow x_1 = 2.65 + 2 L_{eff,1} = (2 \times 8.25 + 2.65) \frac{23688}{17420} = 2.605 \text{ m} \rightarrow L_{eff,1} = 11.7 \text{ m} \rightarrow \Delta M(x=11.5) = 0.5(4290 + 4366) + 4366 = -1.38 \Delta N_2 \rightarrow \Delta N_2 = -4720 \text{ kN} \rightarrow N_2 = 23688 - 4720 = 18970 \text{ kN} \rightarrow x_2 = 19.15 + 23688/18970 = 23.90 \text{ m} \rightarrow L_{eff,2} = 10.60 \text{ m} \rightarrow \Delta M(x=10.60) = 0.5(4620 + 420) = 2520 \text{ kNm} \rightarrow \Delta N_3 = -4990 \text{ kN} \rightarrow N_3 = 18700$
 $x_3 = 24.25 \text{ m} \rightarrow L_{eff,3} = 10.80 \text{ m}$



ΣΥΓΚΡΙΣΗ ΜΕ ΤΗΝ ΠΕΡΙΠΤΩΣΗ
 $\rho = 31\%$ και $T = -70^\circ\text{C}$
 $N = 18700 \triangleq 17350 \text{ kN}$
 $L_{eff} = 10.80 \triangleq 8.75 \text{ m}$

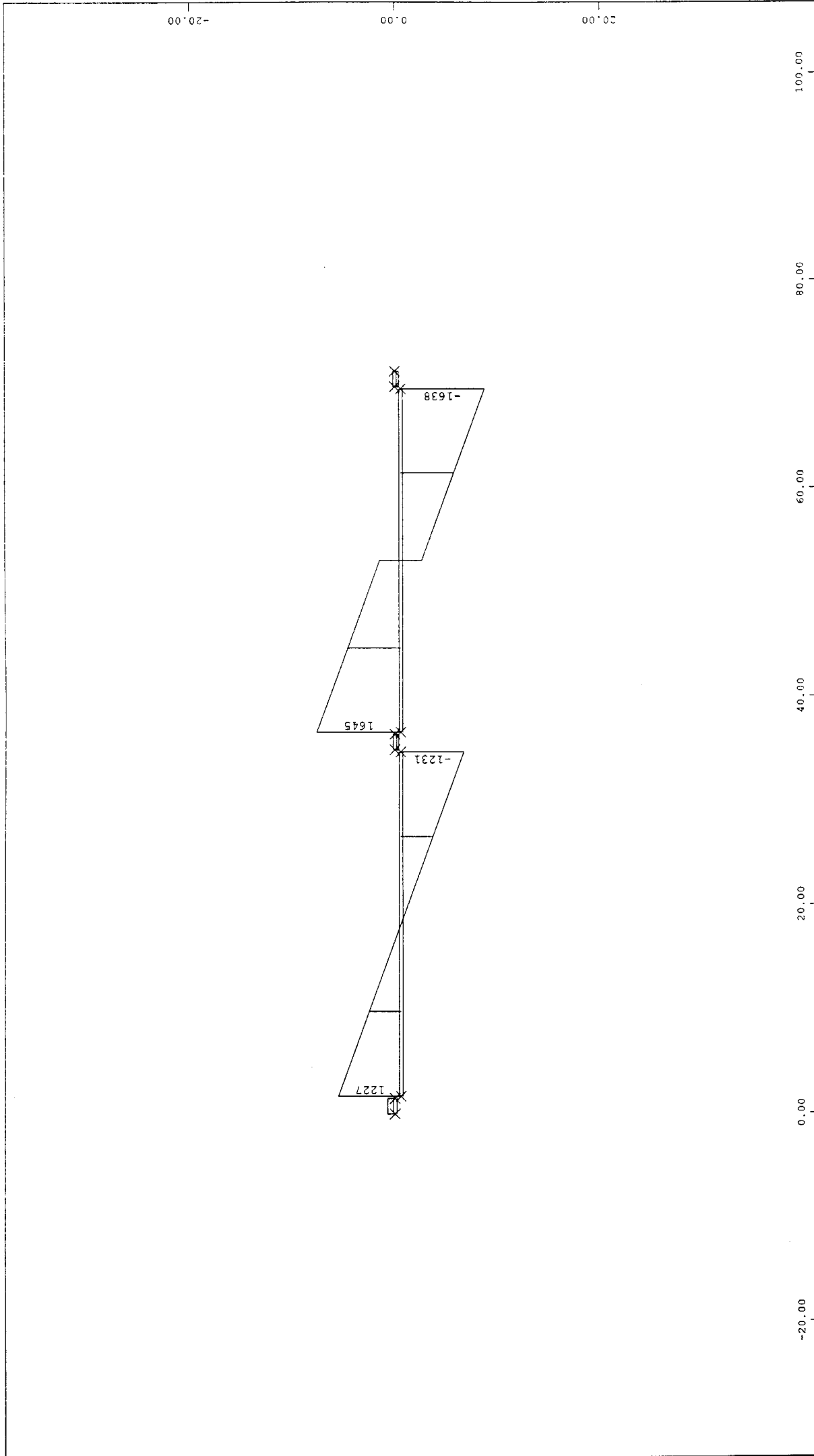
Η ΖΟΝΗ ΔΙΣΤΡΟΦΗΣ ΔΕ ΔΙΕΚΤΕΙΝΕΣ ΚΑΘΑ 1/3
 ΓΕΝΕΔΕΙΣΤΕΣ ΚΑΙ ΔΙΣΤΡΟΦΗ ΣΥΝ ΕΥΔΕΙΣ
 ΚΑΘΑ 7.8% (ΑΝΩΔΕΙΑ)

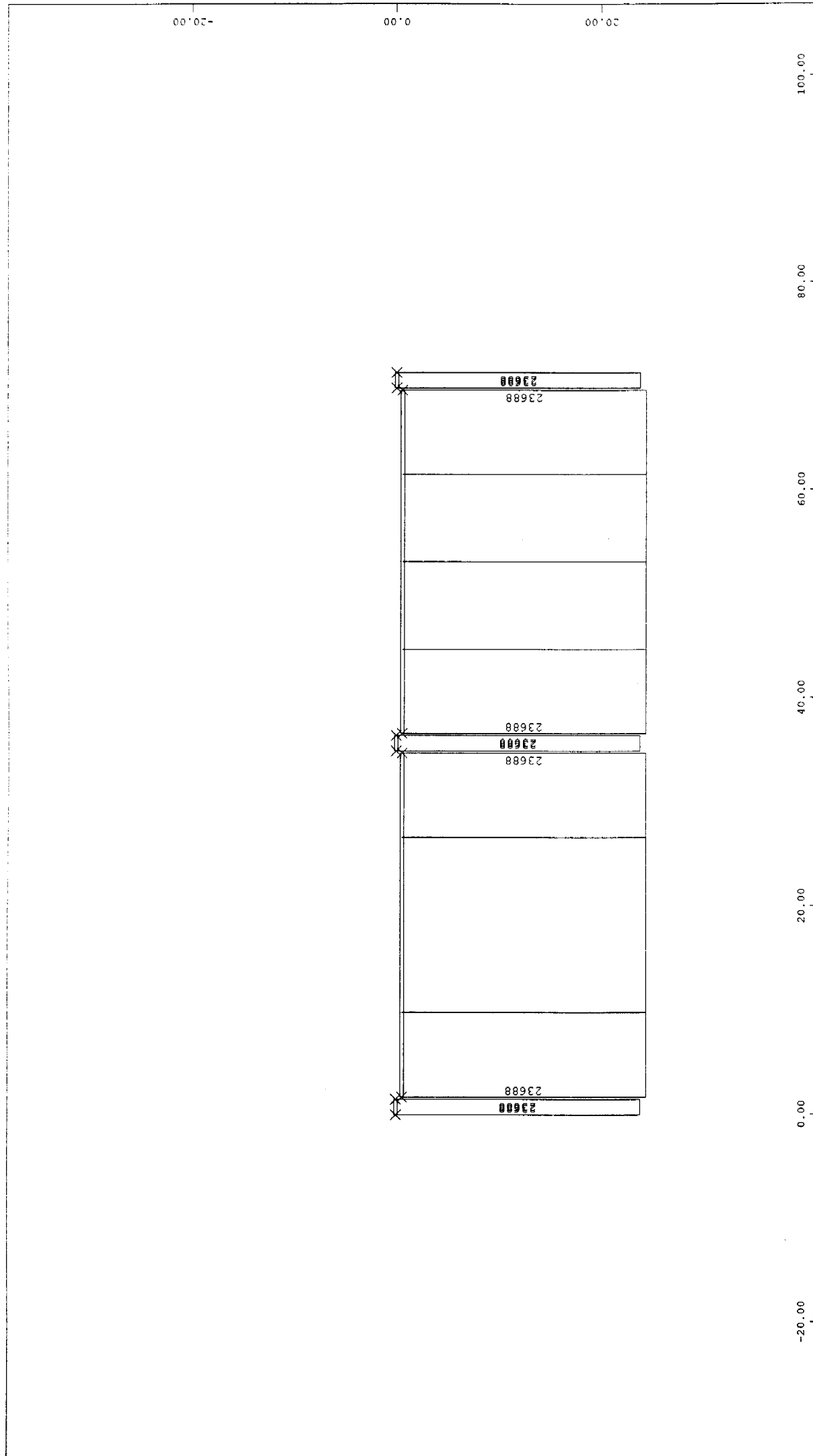
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM MOMENTS MY LC 2 ΦΟΡΤ. ΜΟΝ. + ΚΙΝ. + ΘΕΡΜΟΚΡ. 1 CM = 3500 kNm

M 1 : 500



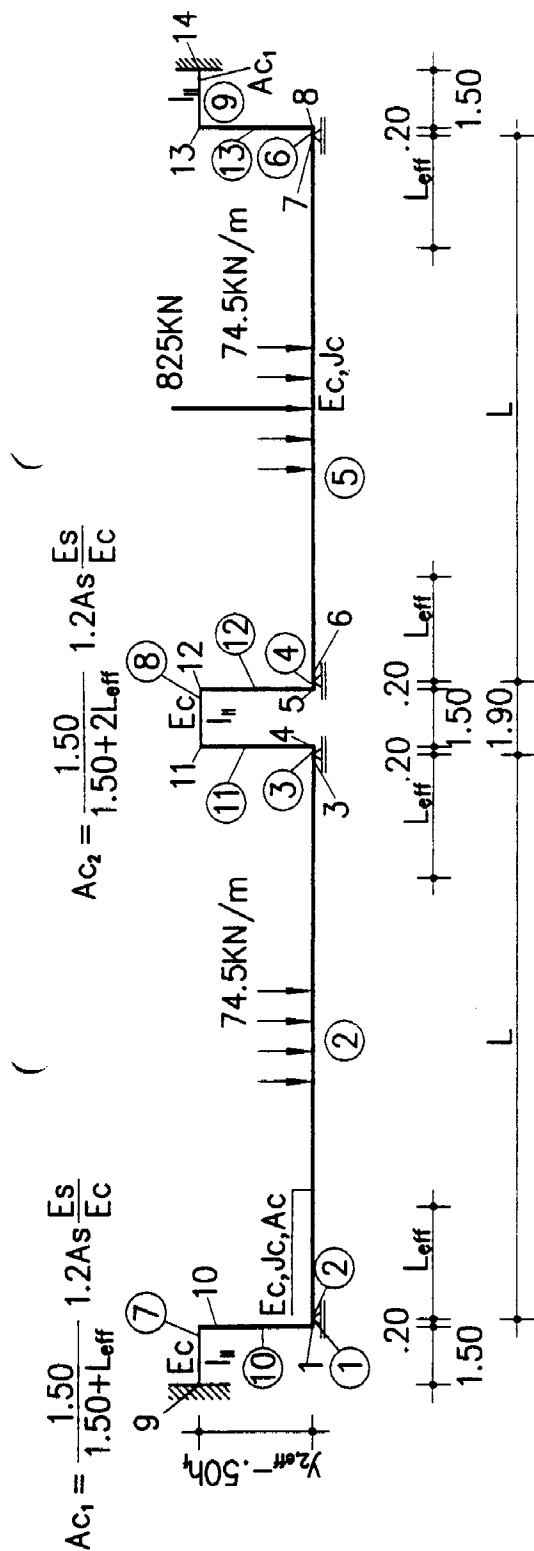


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

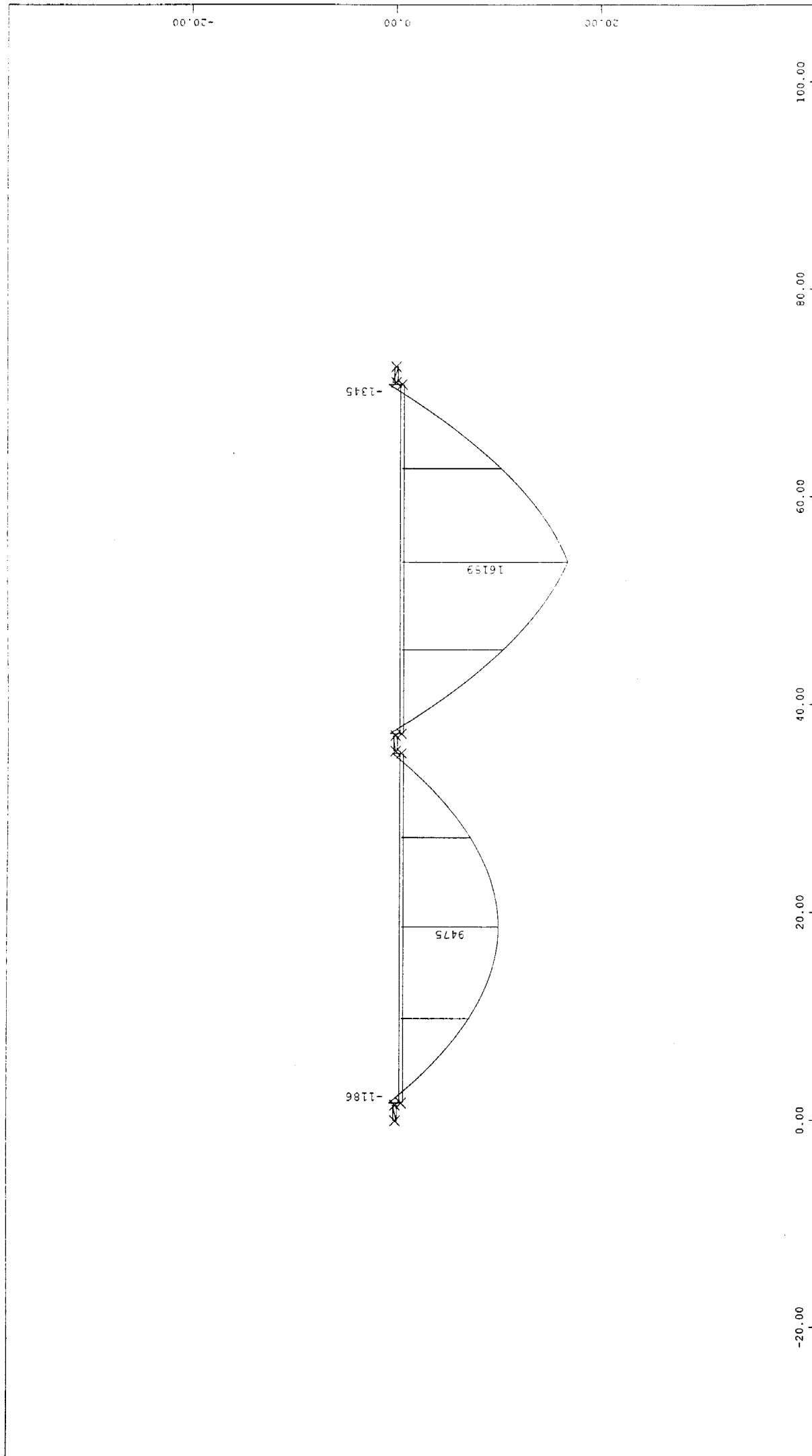
——— BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

M 1 : 500



ΠΙΝΑΚΑΣ ΔΕΔΟΜΕΝΩΝ

$L = 33.0m$	$E_c = 32 \text{ GPa}$
$b = 12.0m$	$a = 6.25$
$A_{c,eff} = 5.100m^2$	$g_1 = 30.7kN/m$
$J_{c,eff} = 2.784m$	$q = 43.8kN/m$
$h_b = 2.15m$	$g_1 + q = 74.5kN/m$
$h_{ft} = 0.275m$	$Q = 825kN$
$h_{t,eff} = 0.20m$	$A_{st} = 739cm^2 (3\phi 14/75)$
$h_{(np.)} = 0.075m$	$\rho = 3.1\% \quad +\phi 4/75k$
$y_{2,eff} = 0.73m$	$A_{sb} = 20.5cm^2/m (\phi 4/75n)$
	$T = -5^\circ C$
$\rho_b = 0.012 (\phi 14/75)$	$L_{eff} = 1/5 = 6.6m$
$I_{II} = 3.544 \alpha \rho b h_{t,eff}^3 / 12 = 0.1772 \rho \approx 0.002 / m^4$	

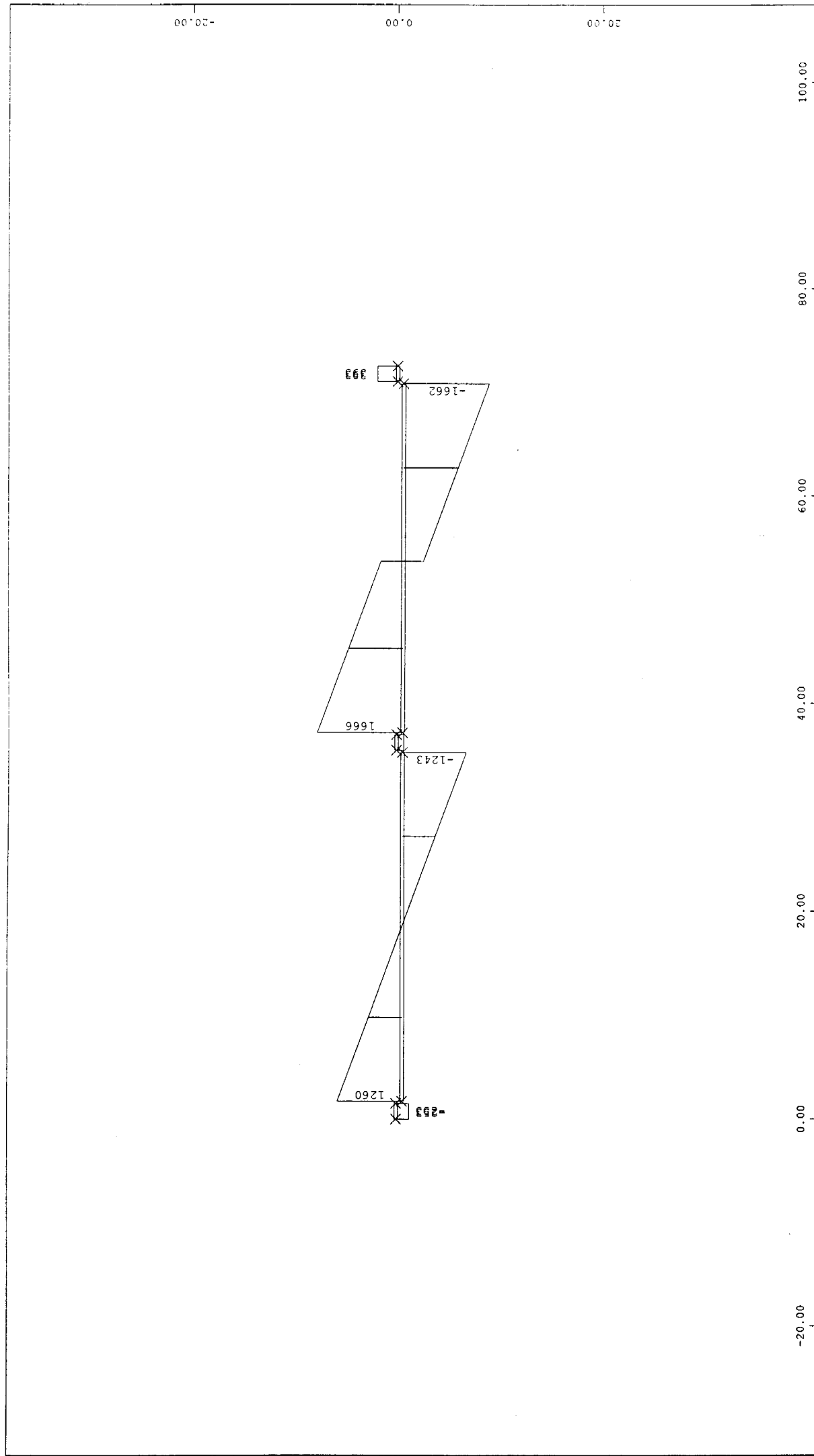


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM MOMENTS MY LC 1 MONIMA+KINHHTA ΦOPTIA 1 CM = 5000 kNm

M 1 : 500

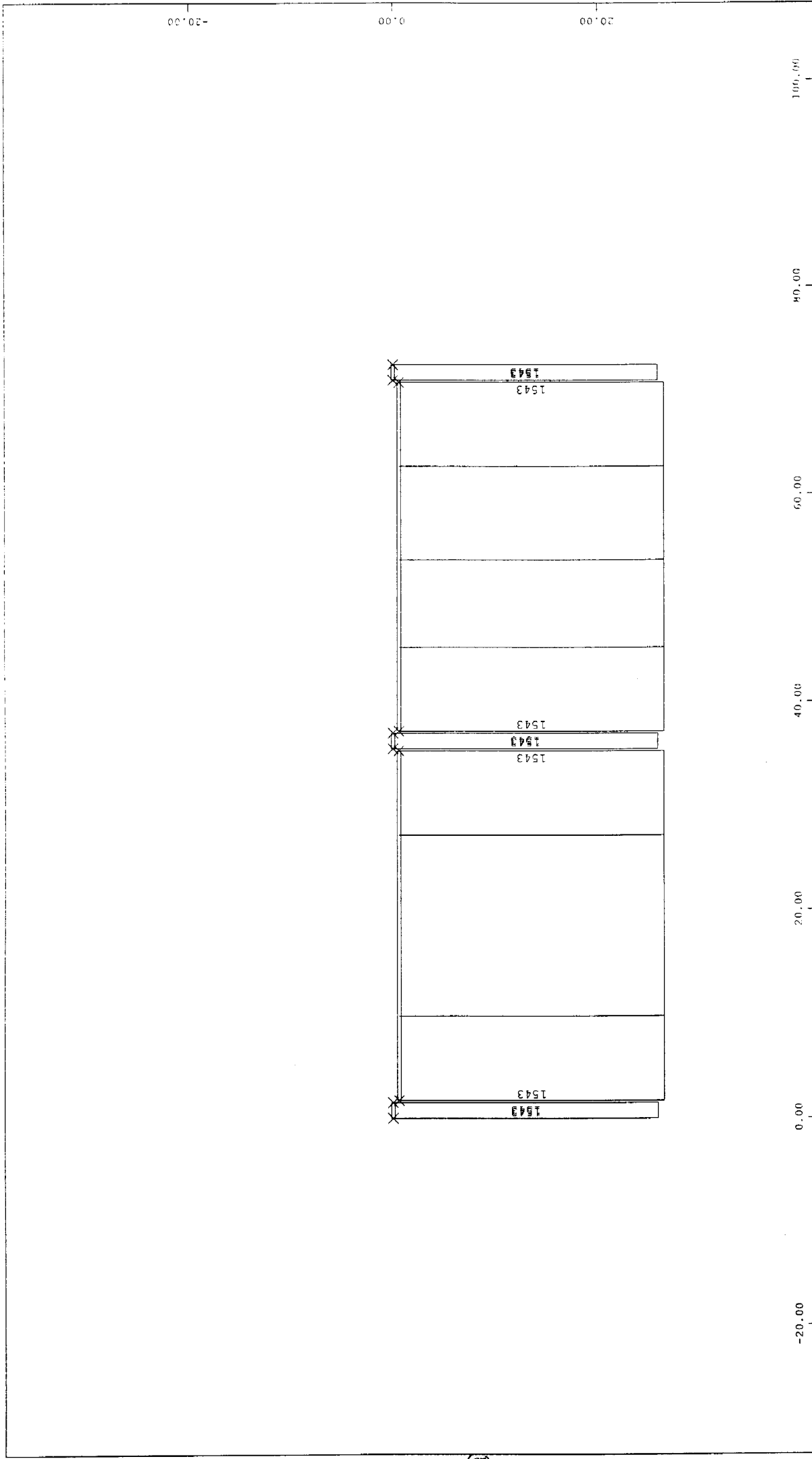


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM SHEAR FORCES QZ LC 1 MONIMA+KINHHTA ΦOPTIA 1 CM = 1000 kN

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

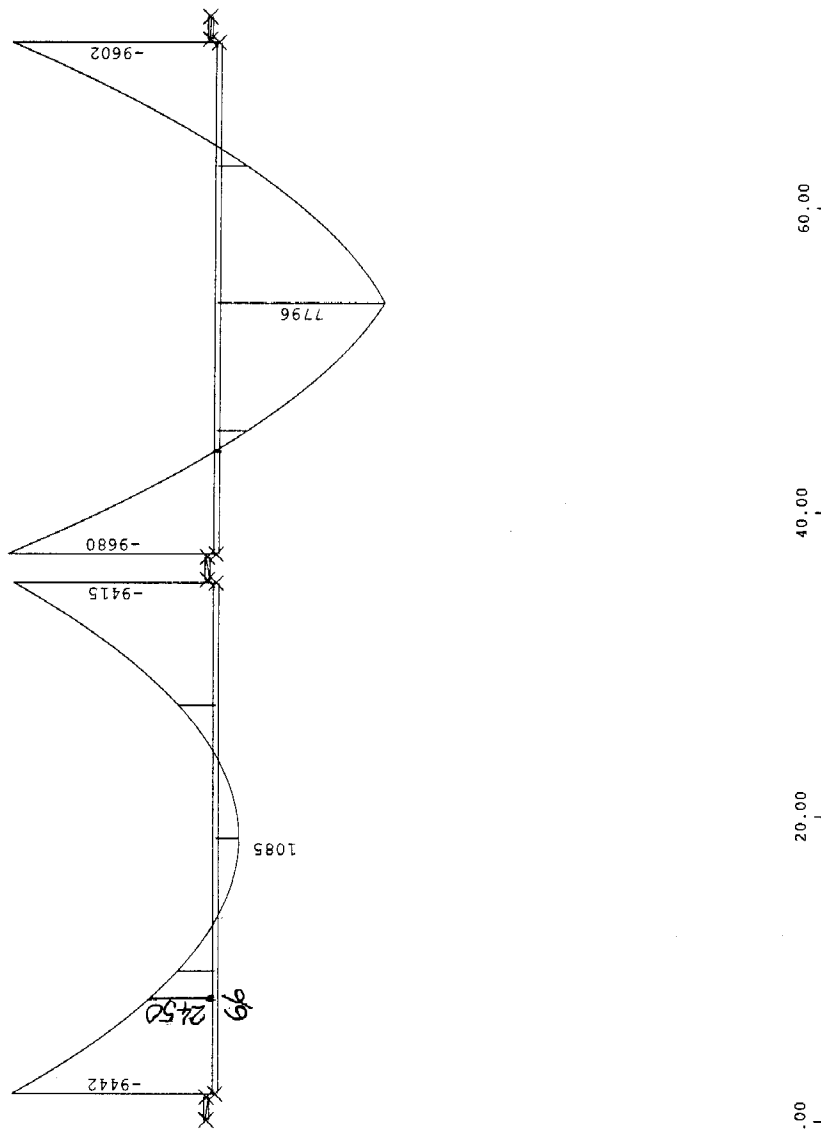
BEAM NORMAL FORCES LC 1 MONIMA+KINHTA ΦOPTIA 1 CM = 300.0 kN

M 1 : 500

ΘΑΜΙΣΤΙΚΑ ΜΕΘΟΔΟΣ

$$v_n \Delta M(x=L_{eff}) - M_{cr} = - \left[\gamma_{eff} \cdot 0.5 h_{f,eff} \right] + \frac{W_{2,eff}}{A_{c,eff}} \Delta N \rightarrow 0.5(2450 + \phi) - 3814 \left(3500 - \frac{16485}{5.1} \right) = -1.38 \Delta N \rightarrow \Delta N = -150 \text{ kN}$$

$$N = 16485 - 150 = 16335 \text{ kN} \rightarrow x = 1585 \times 16485 / 16.335 = 16,00 \text{ m} \rightarrow L_{eff} = 6.65 \text{ m} \rightarrow N = 16400 \text{ kN}$$

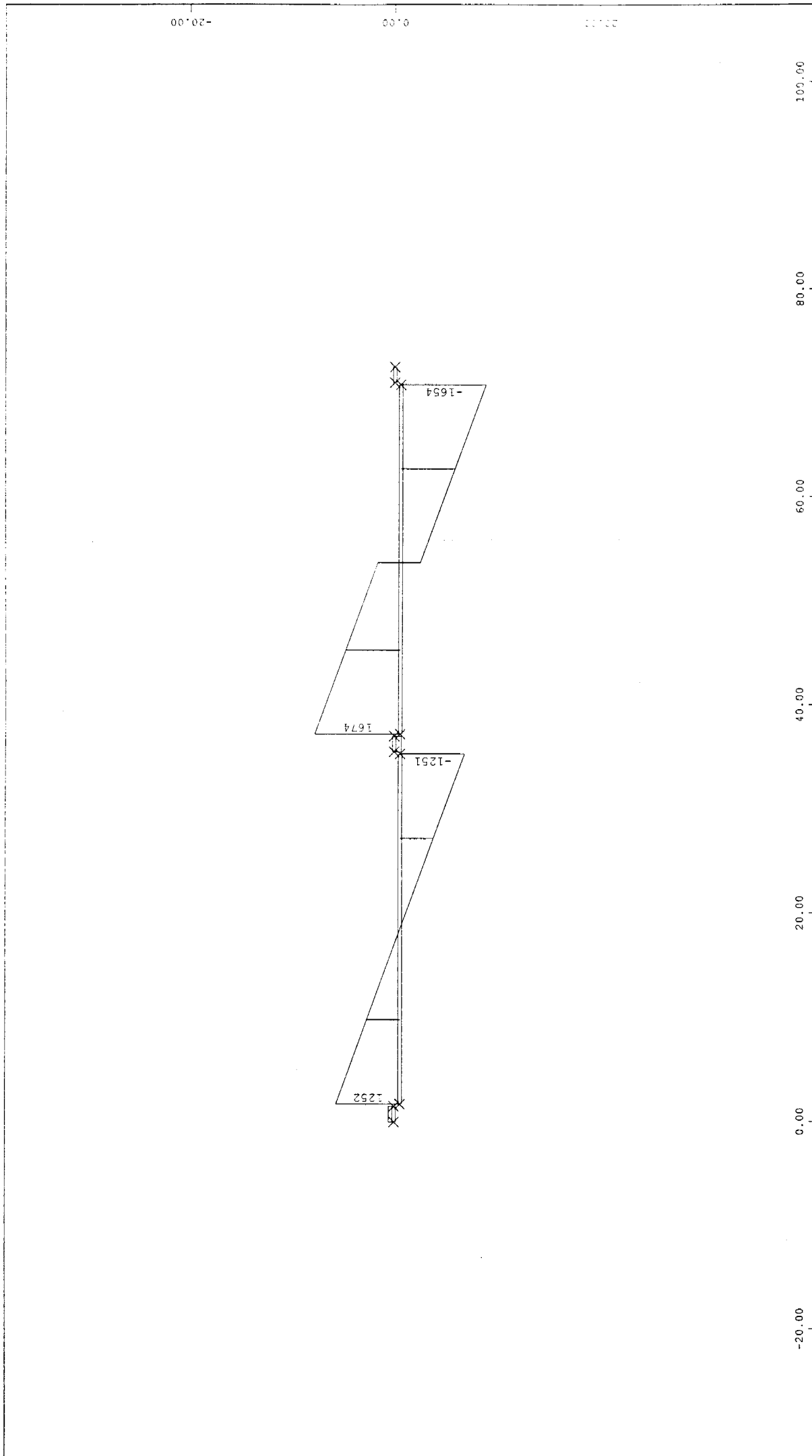


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM MOMENTS MY LC 2 OPT. MON.+KIN.+ΘΕΡΜΟΚΡ. 1 CM = 3500 kNm

M 1 : 500

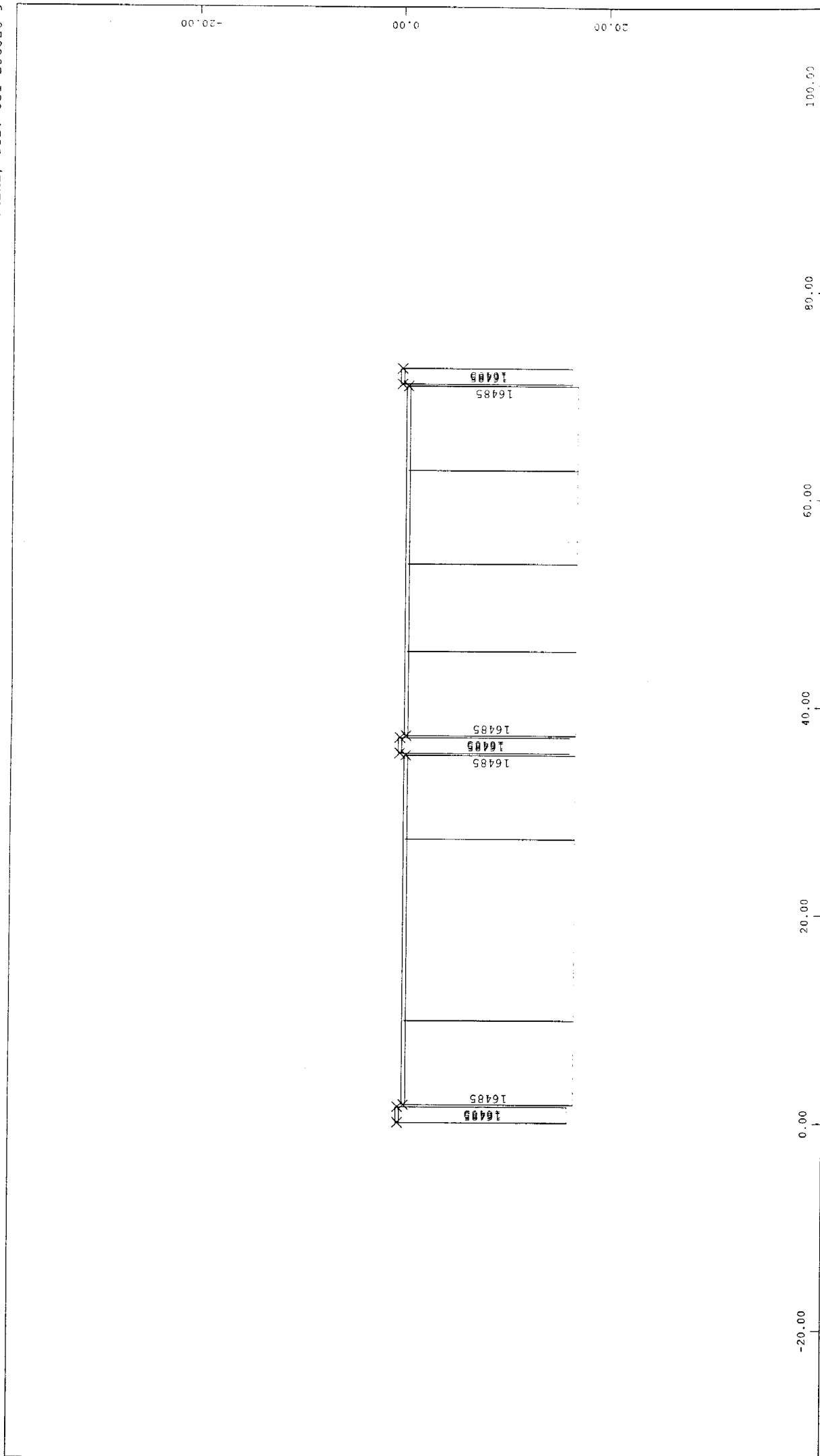


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

——— BEAM SHEAR FORCES QZ LC 2 ΦOPT. MON.+KIN.+ΘEPMOKP. 1 CM = 1000 kN

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

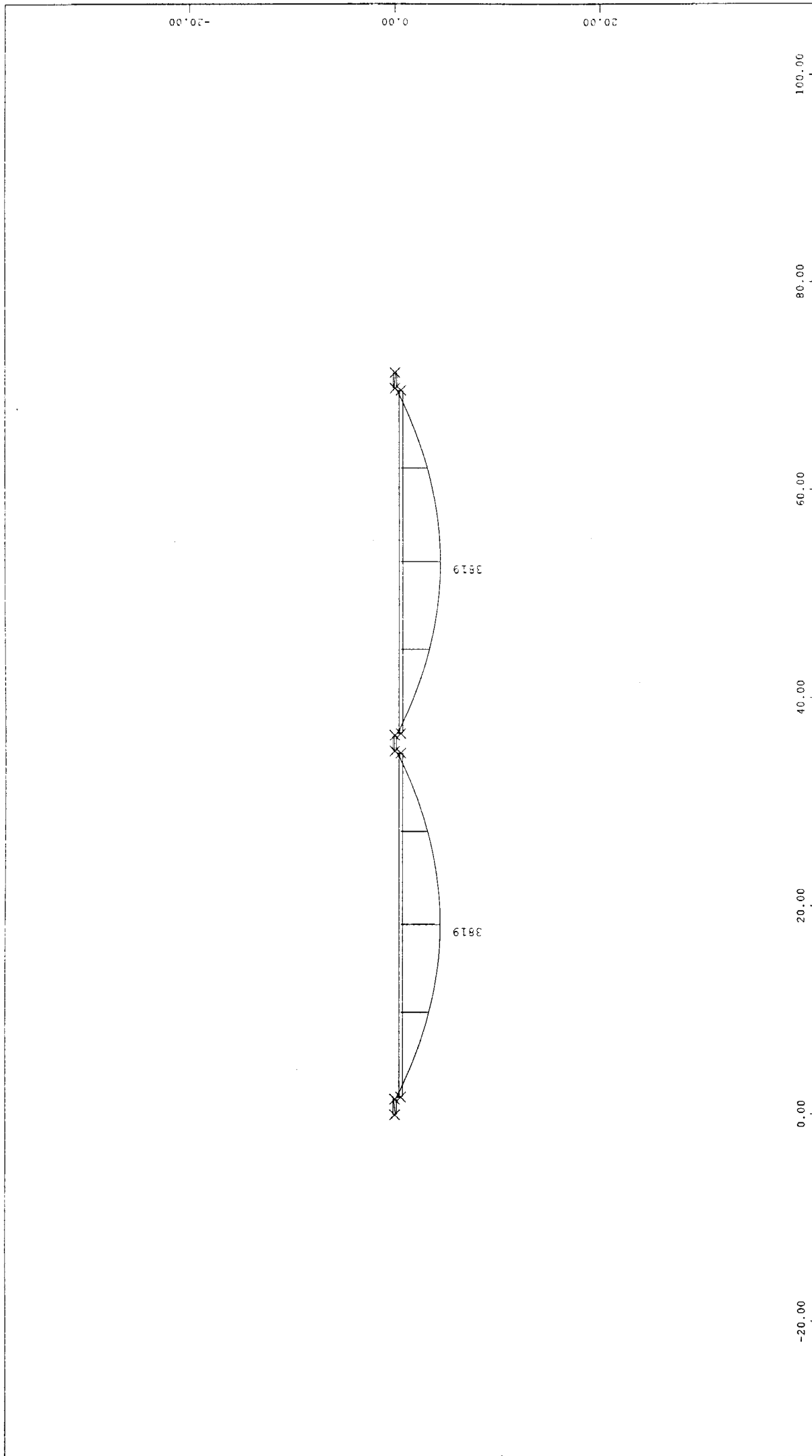
— BEAM NORMAL FORCES LC 2 OPT. MON.+KIN.+ΘEPMOKP. 1 CM = 5000 kN

M 1 : 500

$$AC_2 = \frac{1.50}{1.50 + 2L_{\text{eff}}} \quad \frac{Es}{1.2As} \frac{Ec}{Ec}$$



(31)



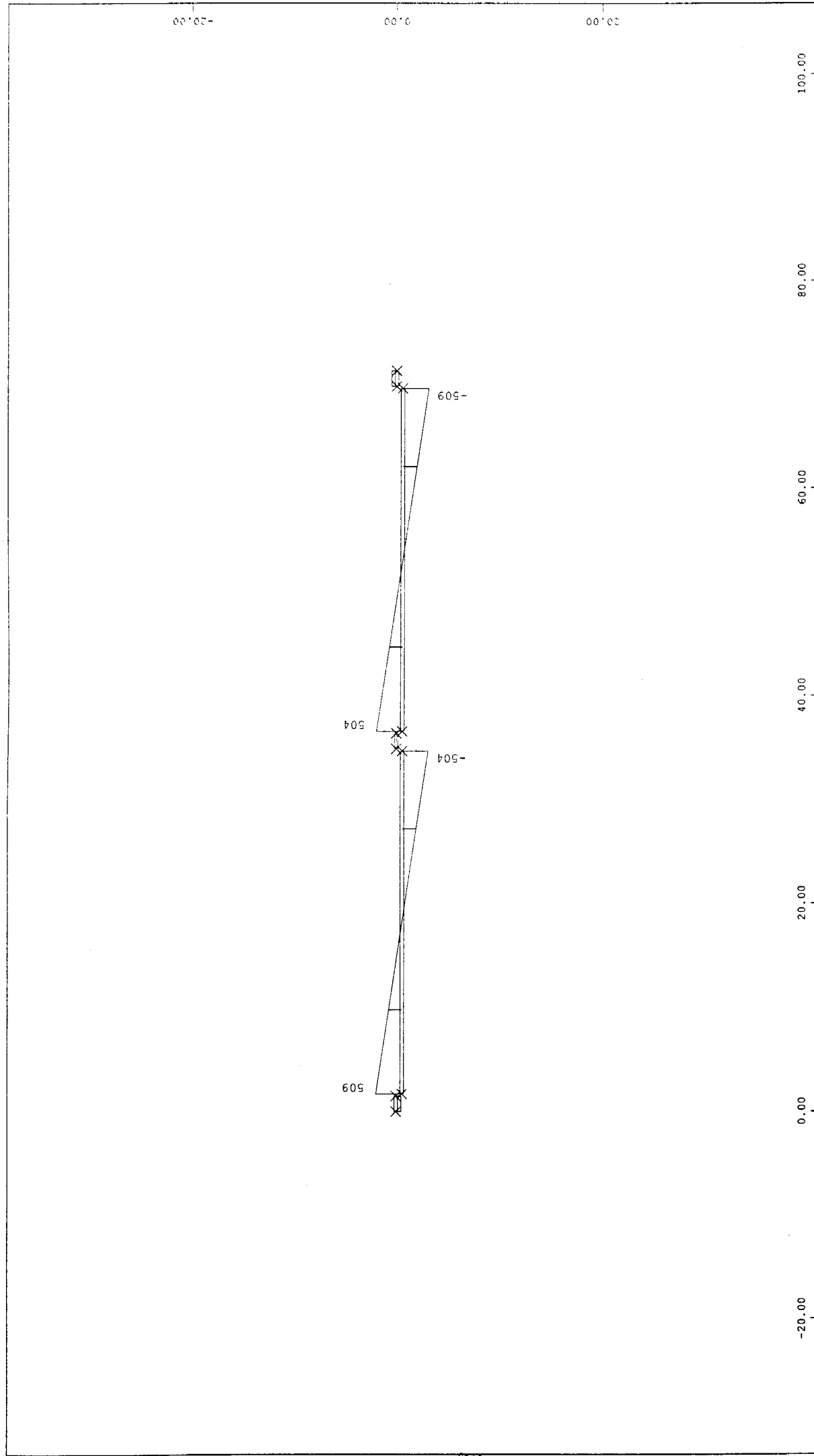
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

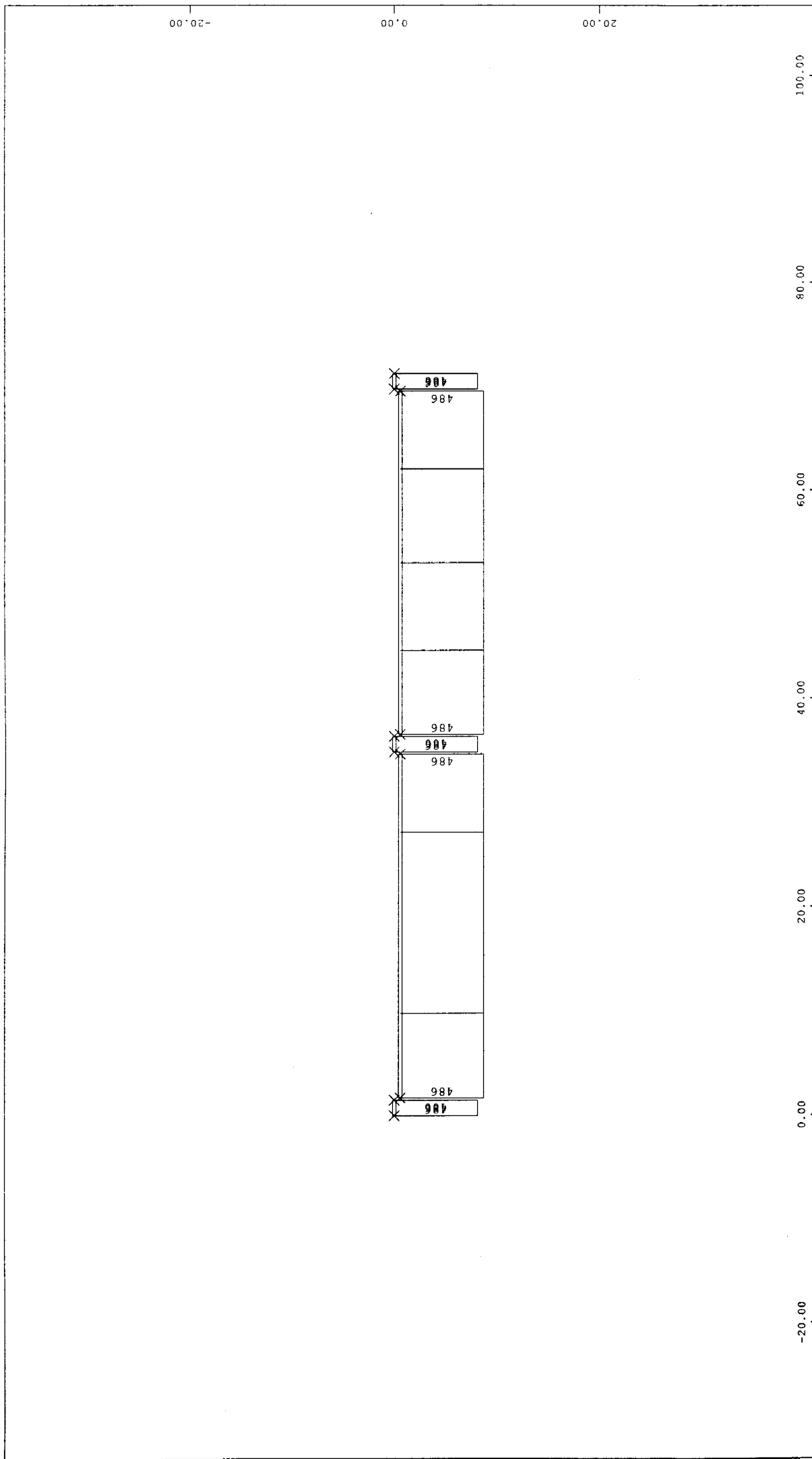
----- BEAM MOMENTS MY LC 1 ϕOPTIA MONIMA+KINHHTA 1 CM = 5000 kNm

x
z

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 BEAM SHEAR FORCES QZ LC 1 ϕOPTIA MONIMA+KINHTA 1 CM = 1000 kN
 M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM NORMAL FORCES LC 1 Φ OPTIA MONIMA+KINHTA 1 CM = 300.0 kN

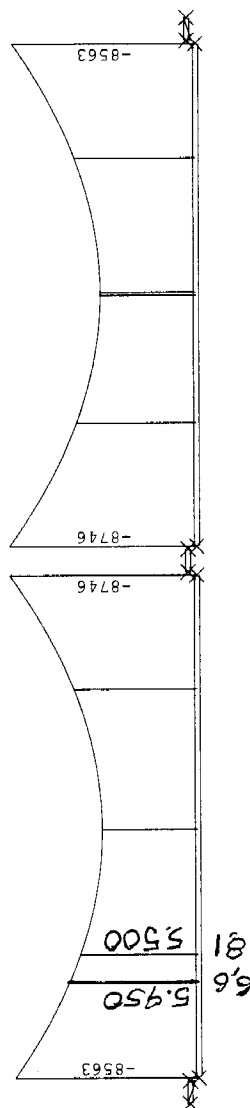
M 1 : 500

ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\begin{aligned} \Delta M(x=L/5) - 3,814(3500 - \frac{N}{5,1}) &= -1,38 \Delta N \rightarrow 5,950 - 3,814(3500 - \frac{15,249}{5,1}) = -1,38 \Delta N_1 \rightarrow \Delta N_1 = -2900 \text{ kN} \rightarrow N_1 = 15249 - 2900 = \\ &= 12.350 \text{ kN} \rightarrow x_1 = (2 \times 6,6 + 2,65) \frac{15,249}{12,350} = 19,55 \text{ m} \rightarrow L_{\text{eff},1} = 0,5(19,55 - 2,65) = 8,40 \text{ m} \rightarrow \text{ση } \Delta M(x=8,40) = 5320 \text{ kNm} \rightarrow \Delta N_2 = \\ &= (5320 - 1945)/1,38 = -2450 \text{ kN} \rightarrow N_2 = 15249 - 2450 = 12800 \text{ kN} \rightarrow x_2 = 15,85 \times 15,249 / 12800 = 18,85 \text{ m} \rightarrow L_{\text{eff},2} = 0,5(18,85 - \\ &- 2,65) = 8,10 \text{ m} \rightarrow \text{ση } \Delta M(x=8,1) = 5500 \text{ kNm} \rightarrow \Delta N_3 = (5500 - 1945)/1,38 = -2570 \text{ kN} \rightarrow N_3 = 15249 - 2570 = 12700 \text{ kN} \rightarrow \\ x_3 &= 15,85 \times 15,249 / 12700 = 19,0 \text{ m} \rightarrow L_{\text{eff},3} = 0,5(19,0 - 2,65) = 8,15 \text{ m} \end{aligned}$$

ΣΥΜΠΕΡΑΣΜΑ

Συγκριτικά με την περίπτωση της πλήρους φορτισμένης, υπό με κενά, έχουμε παρατηρείται μία μείωση του εφέ. Νώρα 21% καθής υπό μία αύξηση του L_{eff} τώρα επίσης 21%.

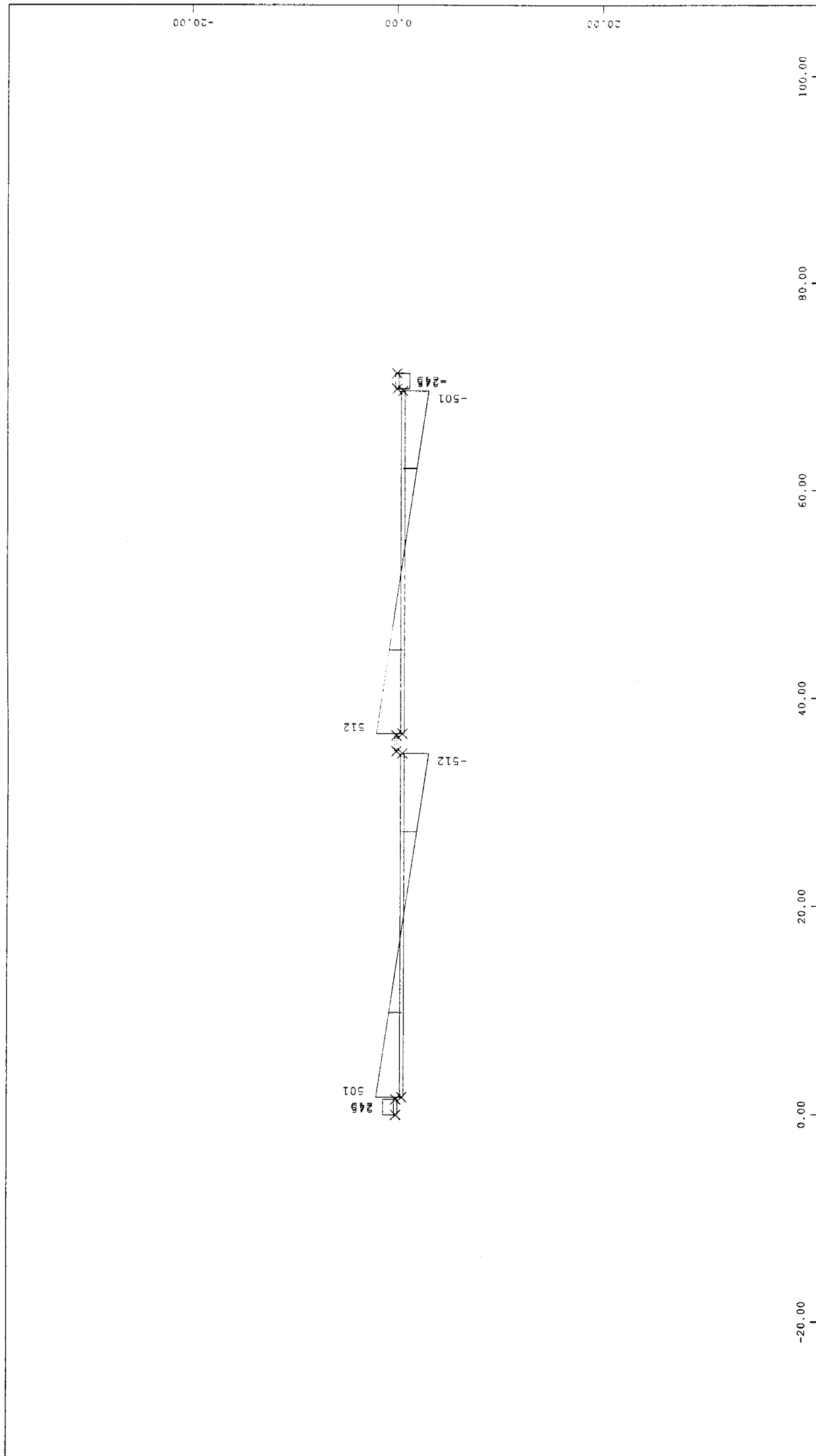


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM MOMENTS MY LC 2 OPT. MON.+KIN.+ΘΕΡΜΟΚΡ. 1 CM = 3500 kNm

M 1 : 500

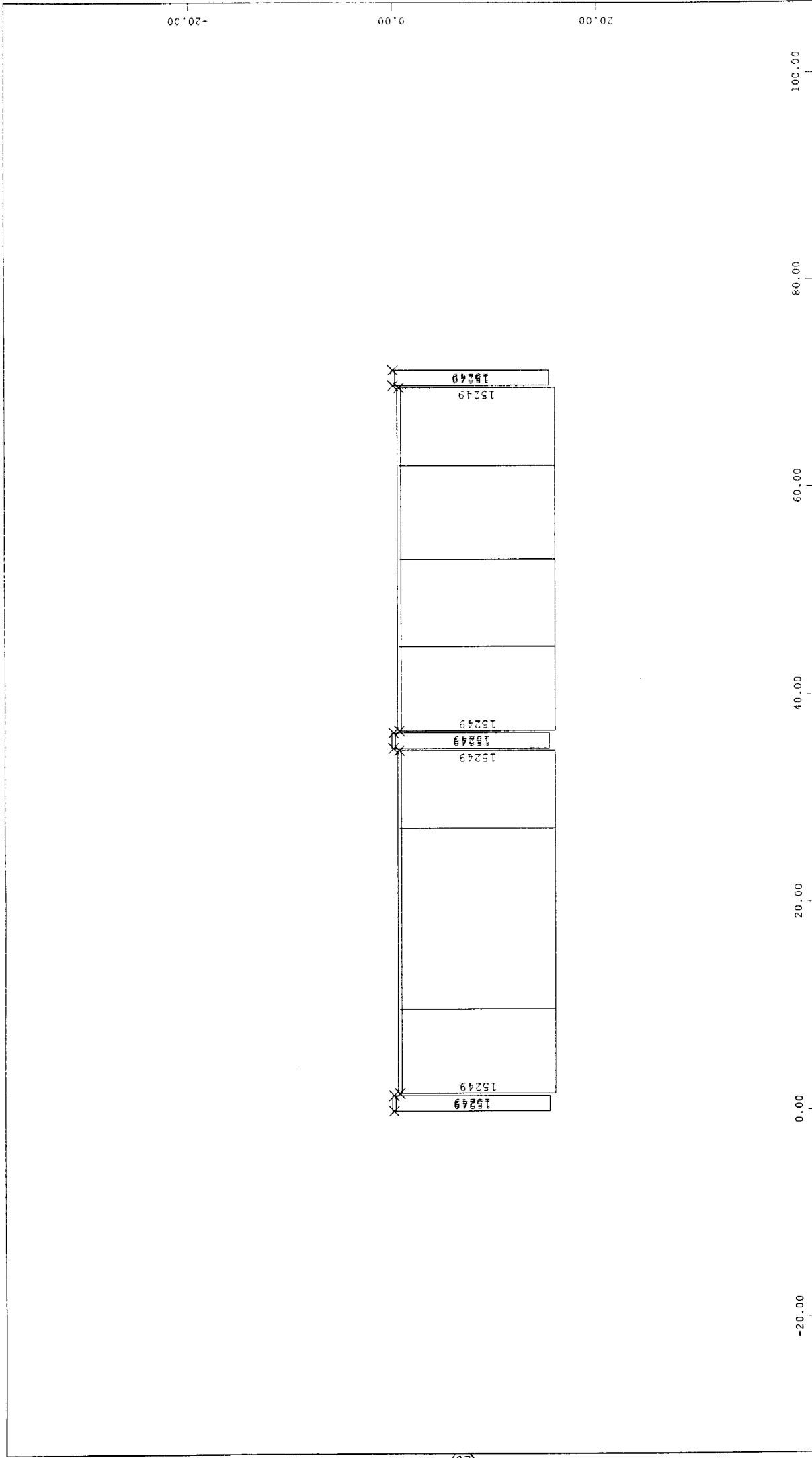


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM SHEAR FORCES QZ LC 2 OPT. MON.+KIN.+ΘEPMOKP. 1 CM = 1000 kN

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

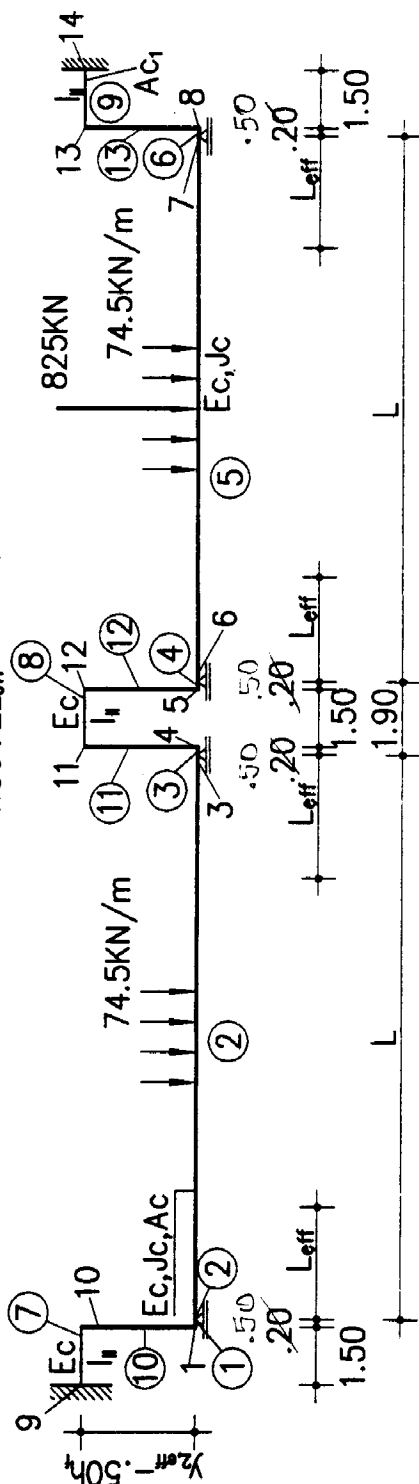
BEAM NORMAL FORCES LC 2 4OPT. MON.+KIN.+0EPMOKP. 1 CM = 5000 kN

M 1 : 500

()

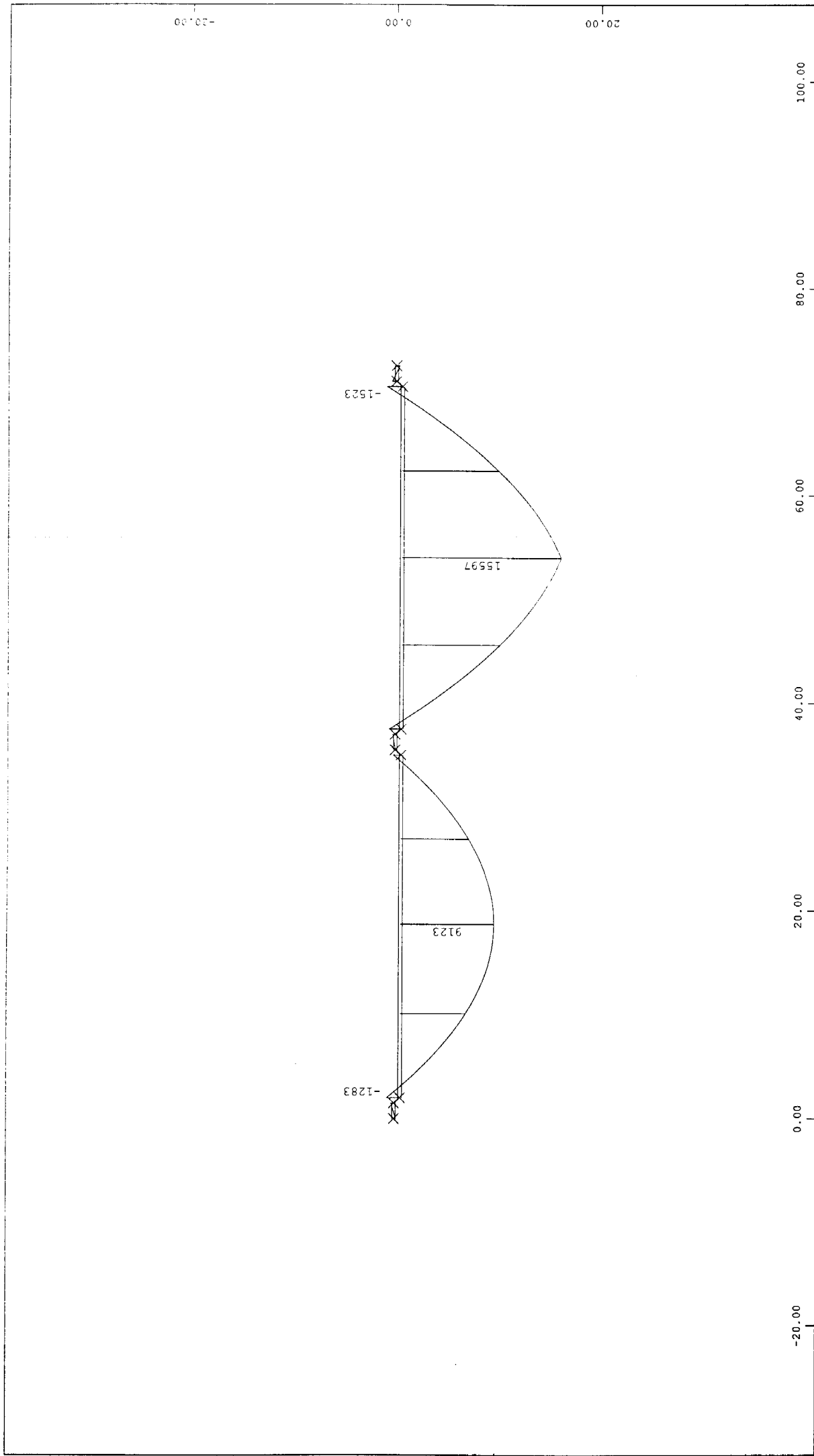
$$A_{c1} = \frac{1.50}{1.50 + L_{eff}} \frac{1.2 A_s E_s}{E_c}$$

$$A_{c2} = \frac{1.50}{1.50 + 2L_{eff}} \frac{1.2 A_s E_s}{E_c}$$

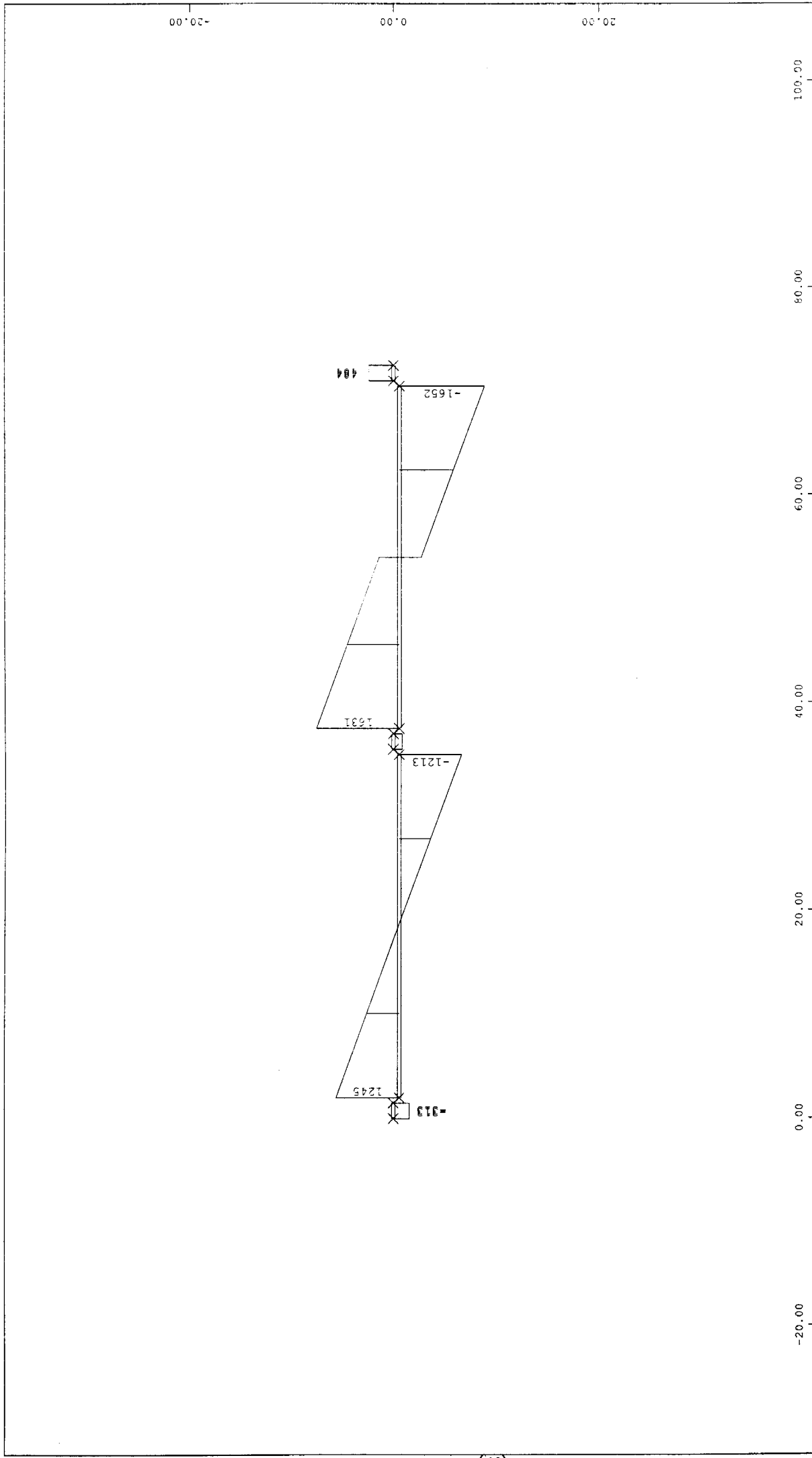


ΠΙΝΑΚΑΣ ΔΕΔΟΜΕΝΩΝ

$L = 33.0m$	$E_c = 32 \text{ GPa}$
$b = 12.0m$	$\alpha = 6.25$
$A_{c,eff} = 5.100m^2$	$g_1 = 30.7kN/m$
$J_{c,eff} = 2.784m$	$q = 43.8kN/m$
$h_b = 2.15m$	$g_1 + q = 74.5kN/m$
$h_{\pi} = 0.275m$	$Q = 825kN$
$h_{r,eff} = 0.20m$	$A_{st} = 739cm^2 (3\phi 14/75)$
$h_{(np.)} = 0.075m$	$\rho = 3.1\%$
$\chi_{2,eff} = 0.73m$	$A_{st} = 205 \frac{cm^2}{m} (3\phi 14/75) + 214 \frac{cm^2}{m} (3\phi 14/75) k.$
$\rho_b = 20.5/175 = 0.012$	$T = -50^{\circ} / -60^{\circ} / -70^{\circ} C$
$I_{II} = 3.544 \alpha \rho_b h_{r,eff}^3 / 12 = 0.1772 \rho_b = 0.0021 m^4$	$L_{eff} = L/5 = 6.6$



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
— BEAM MOMENTS MY LC 1 ϕOPTIA MONIMA+KINHTA 1 CM = 5000 kNm

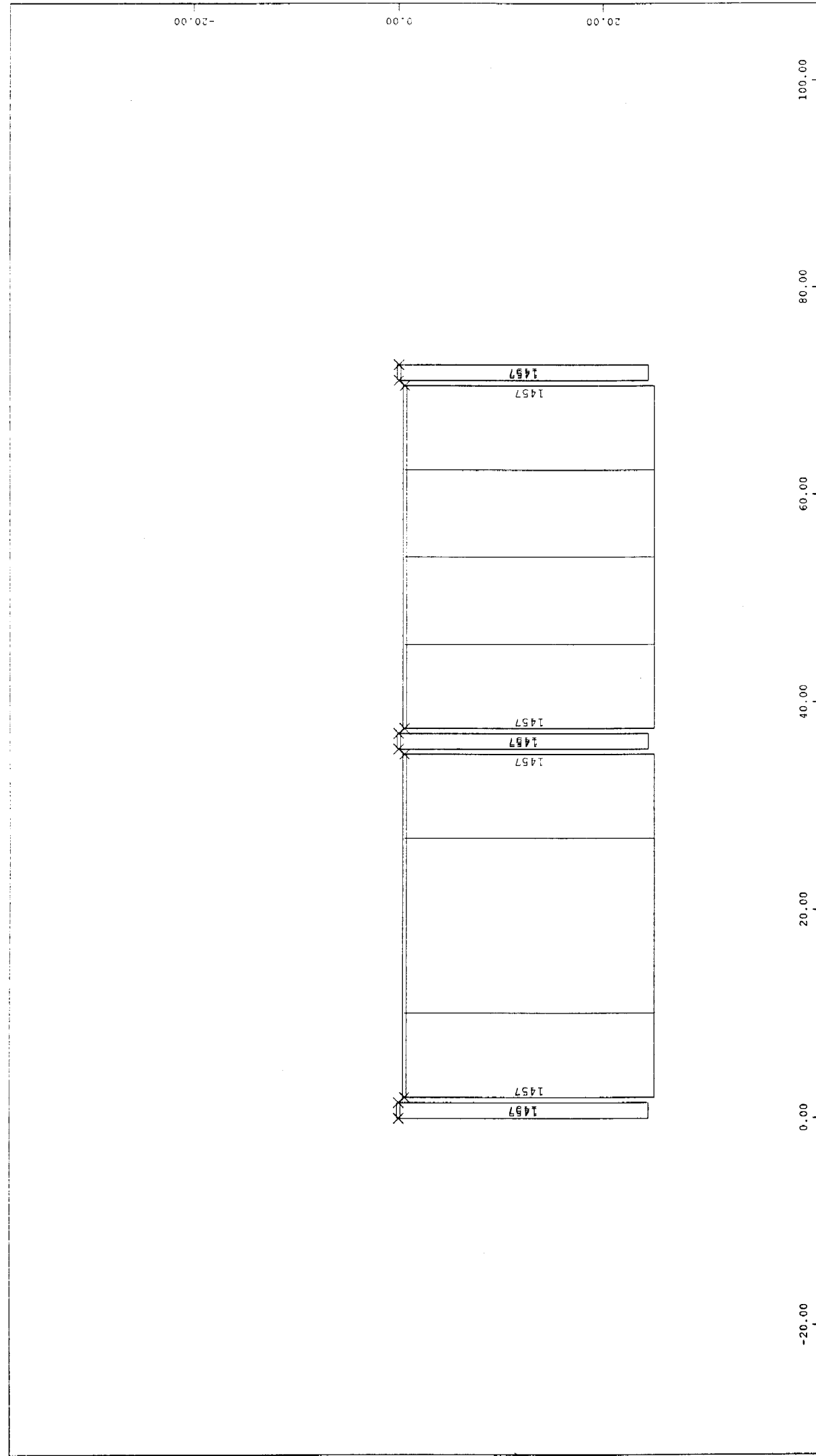


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM SHEAR FORCES QZ LC 1 OPTIA MONIMA+KINHTA 1 CM = 1000 kN

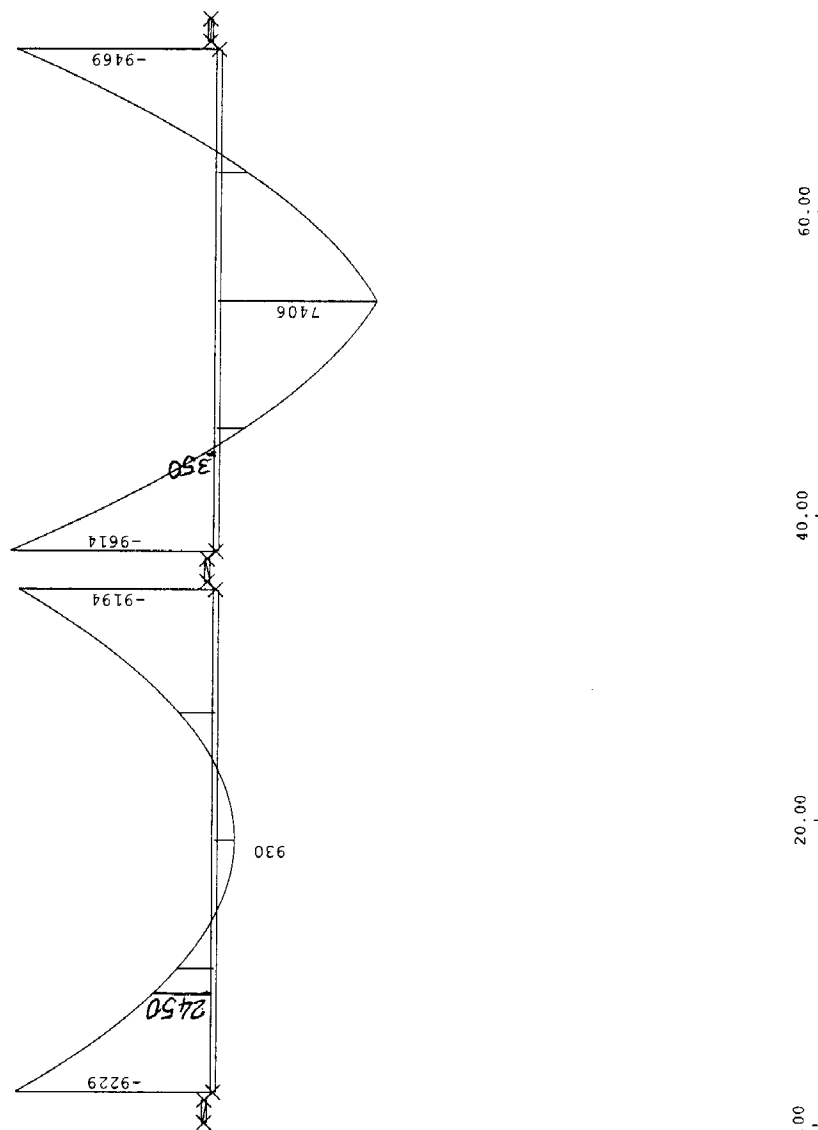
M 1 : 500



ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$v_n \Delta M (x=L_{eff}) - M_{cr} = - \left[\gamma_{2,eff} - 0,5 \gamma_{p,eff} \right] + \frac{M_{2,eff}}{A_{c,eff}} \Delta N \rightarrow 0,5 (2450 + 350) - 3814 (3500 - \frac{16240}{5,1}) = - (0,63 + \frac{3814}{0,73}) \Delta N \rightarrow \Delta N = -140 \text{ kN}$$

$$N = 16.240 - 140 = 16.100 \text{ kN} \rightarrow x = 1585 \times 16.240 / 16.100 \approx 16.00 \text{ m} \rightarrow L_{eff} = 6,65 \text{ m} \rightarrow N = 16.100 \text{ kN}$$

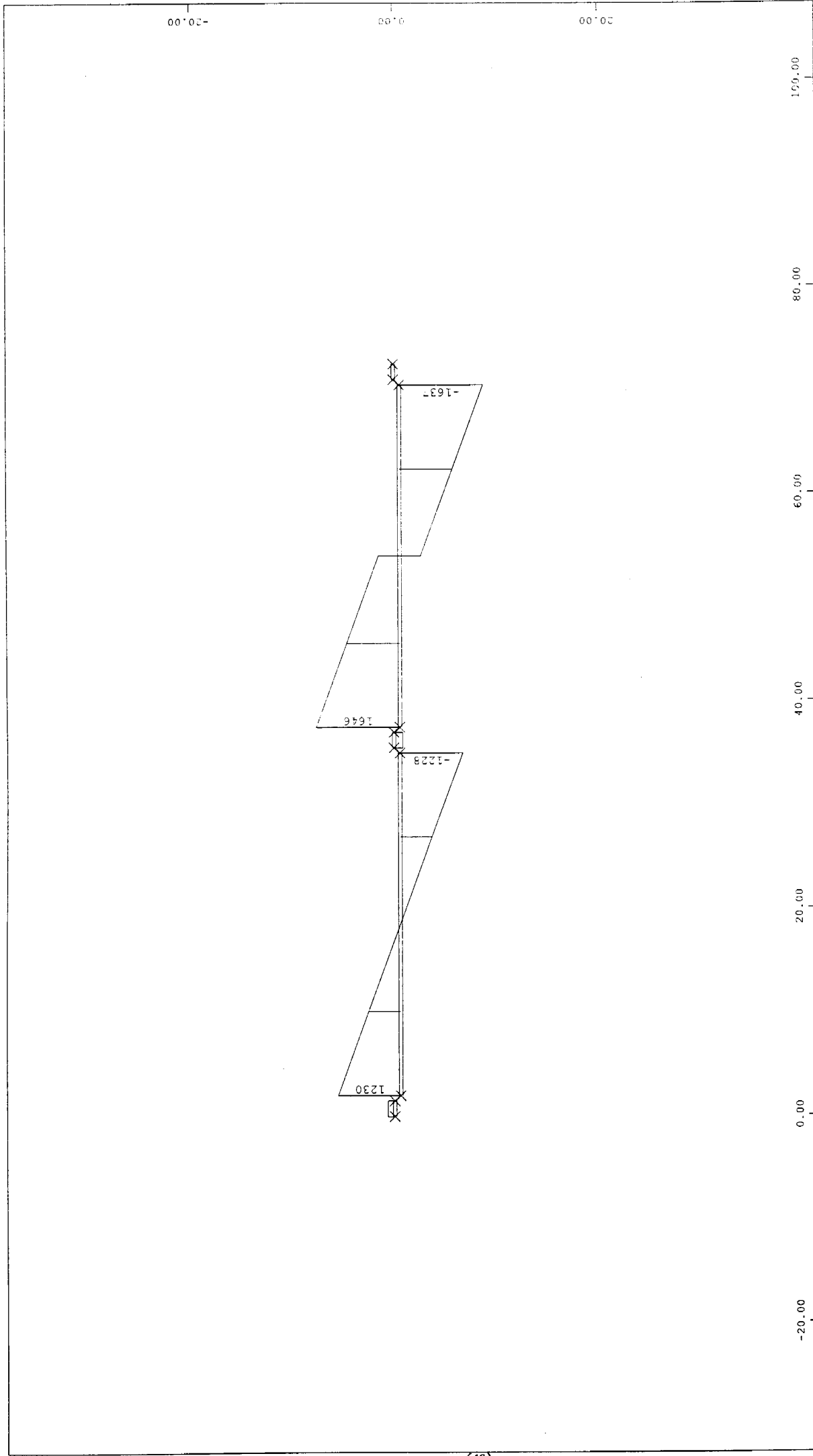


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM MOMENTS MY LC 2 ΦOPT. MON.+KIN.+ΘΕΡΜΟΚΡ. 1 CM = 3500 kNm

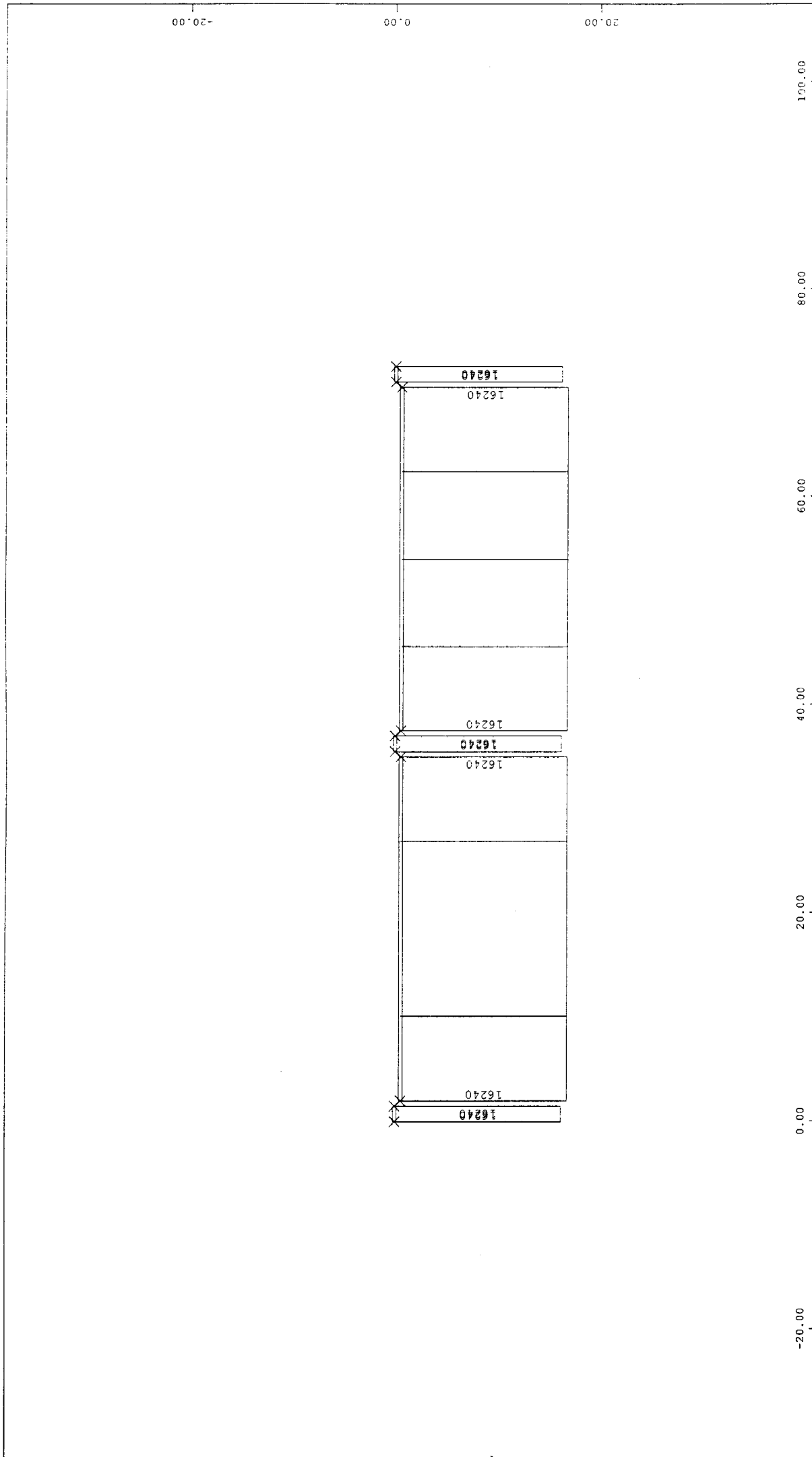
M 1 : 500



M 1 : 500

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
——— BEAM SHEAR FORCES QZ LC 2 ΦOPT. MON.+KIN.+ΦEPMOKP. 1 CM = 1000 kN

x
y
z

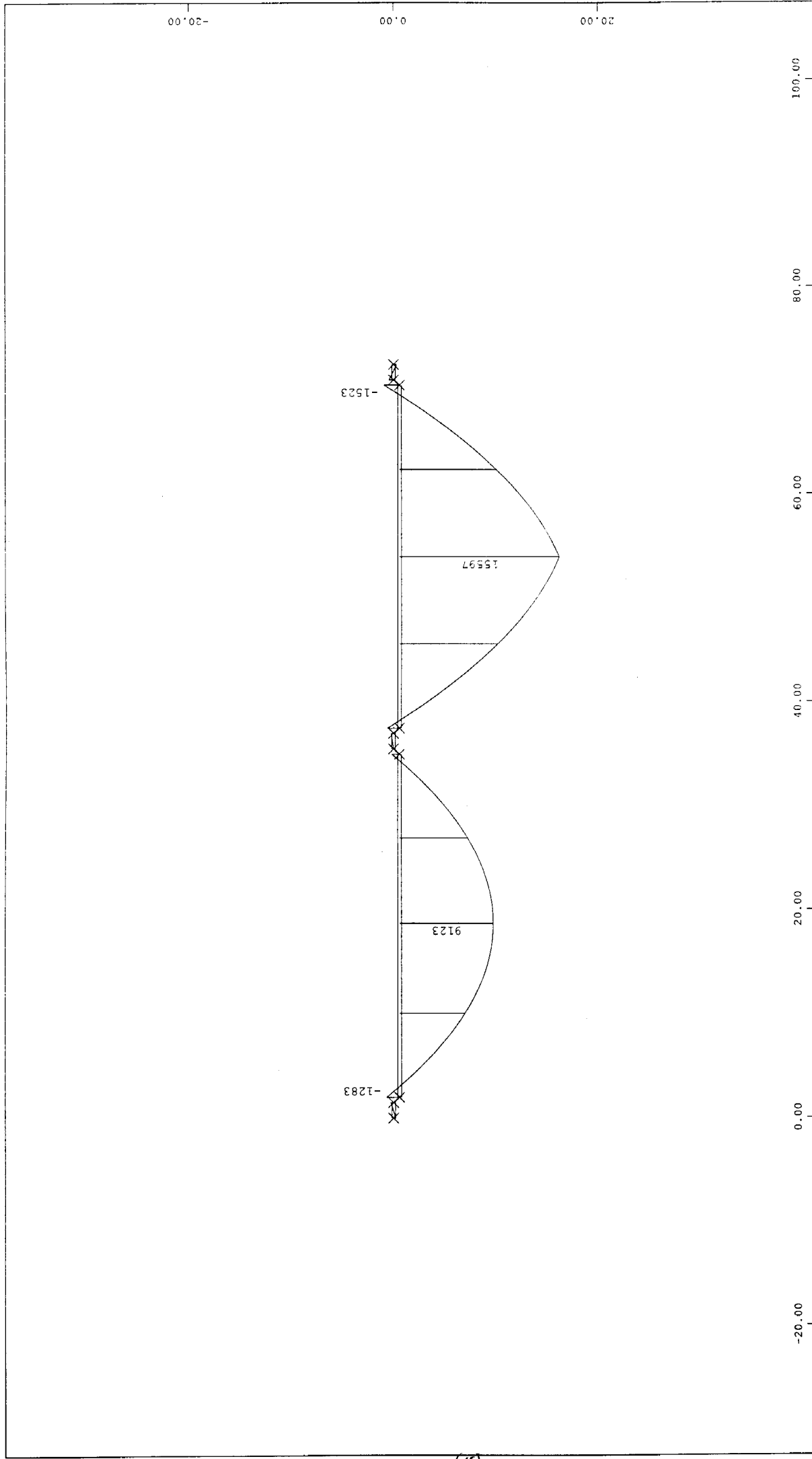


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM NORMAL FORCES LC 2 OPT. MON.+KIN.+ΘEPMOKP. 1 CM = 5000 kN

M 1 : 500

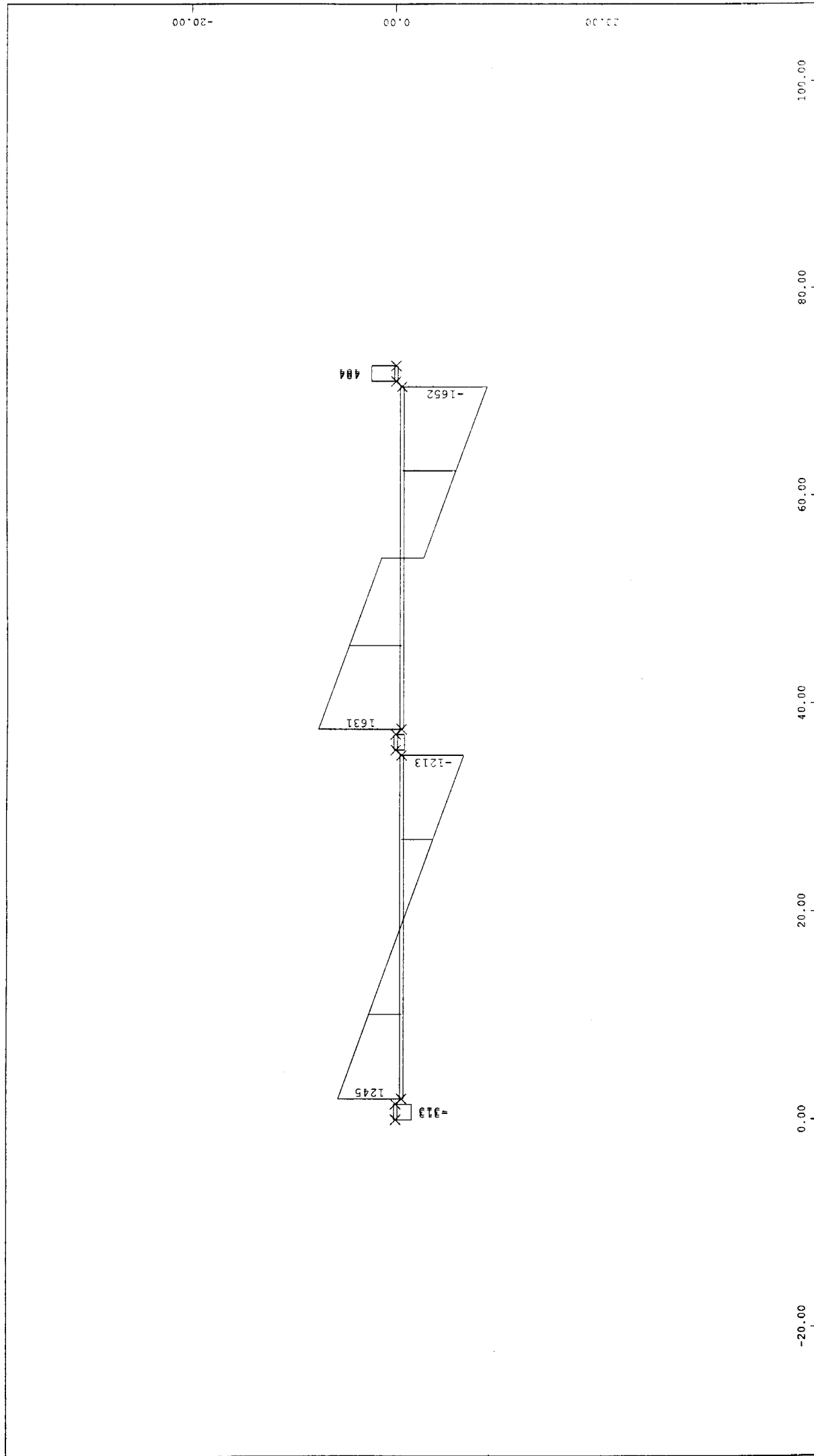


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM MOMENTS MY LC 1 ΦOPTIA MONIMA+KINHTA 1 CM = 5000 kNm

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM SHEAR FORCES QZ LC 1 OPTIA MONIMA KINIITA 1 CM 1000 kN

M 1 : 500



SECTOR OF SYSTEM, ELEMENT GROUP 0

—BEAM NORMAL FORCES LC 1 ΦOPTIA MONIMA+KINHITA 1 CM = 300.0 kN

M 1 : 500

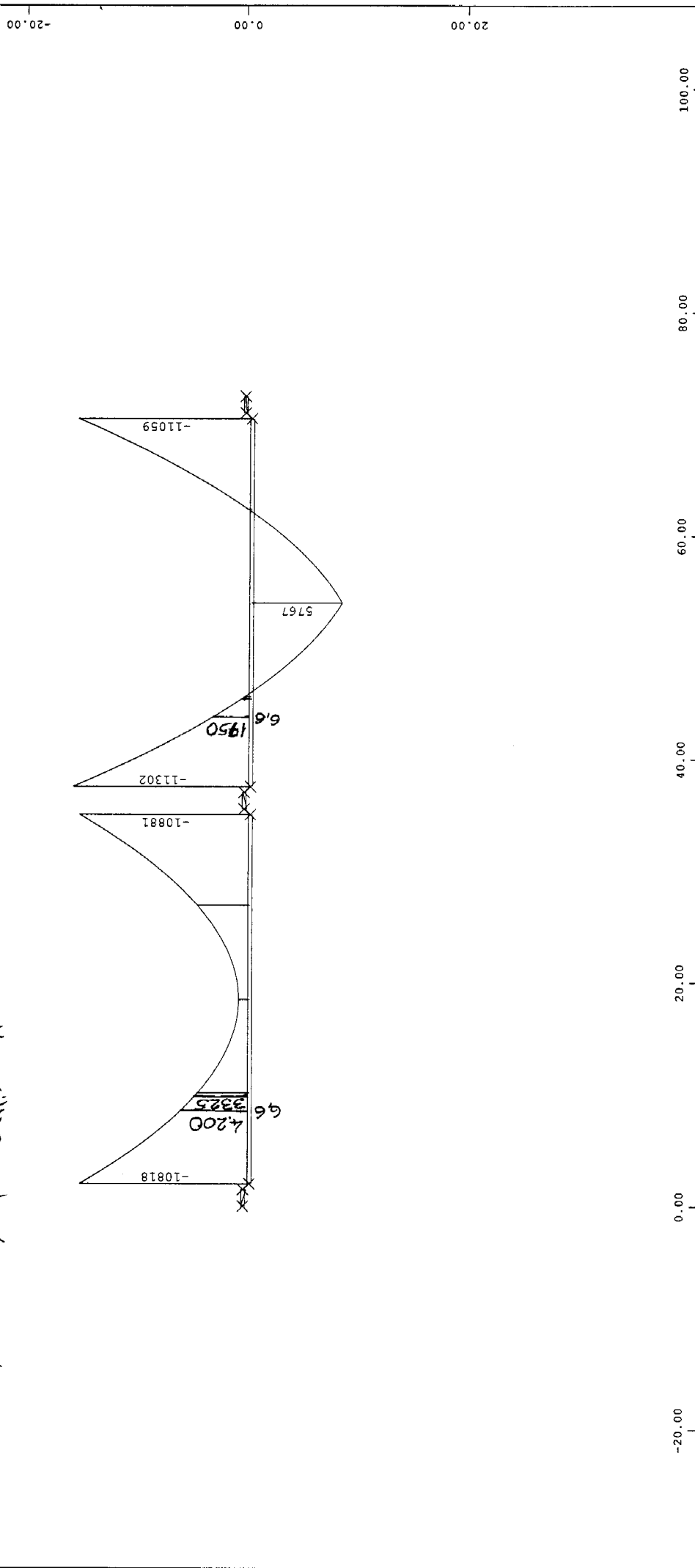
ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$M(x=L_{eff}) - M_{cr} = - \left[(x_2 - 0,5 l_{p,eff}) + \frac{W_{2,eff}}{A_{c,eff}} \right] \Delta N \rightarrow 0,5 (4,200 + 1,950) - 3,814 (3,500 - \frac{1,917}{5,1}) = -1,38 \Delta N_1 \rightarrow \Delta N_1 = -2,960 \text{ kN} \rightarrow N_1 = 19,200 - 2,960 = 16,240 \text{ kN}$$

$$\rightarrow x_1 = 14,85 \times 19,200 / 16,240 = 17,40 \text{ m} \rightarrow L_{eff,1} = 7,95 \text{ m} \rightarrow 0,5 (3,325 + 3,50) + 1,010 = -1,38 \Delta N_2 \rightarrow \Delta N_2 = -2,060 \text{ kN} \rightarrow N_2 = 19,200 - 2,060 = 17,140 \text{ kN}$$

$$\rightarrow x_2 = 14,85 \times 19,200 / 17,140 = 16,45 \text{ m} \rightarrow L_{eff,2} = 7,50 \text{ m} \rightarrow 0,5 (3,500 + 3,75) + 1,010 = -1,38 \Delta N_3 \rightarrow \Delta N_3 = -2,320 \text{ kN} \rightarrow N_3 = 16,880 \text{ kN}$$

$$x_3 = 15,85 \times 19,200 / 16,880 = 18,0 \text{ m} \rightarrow L_{eff,3} = 7,70 \text{ m} \rightarrow N = 16,800 \text{ kN}$$

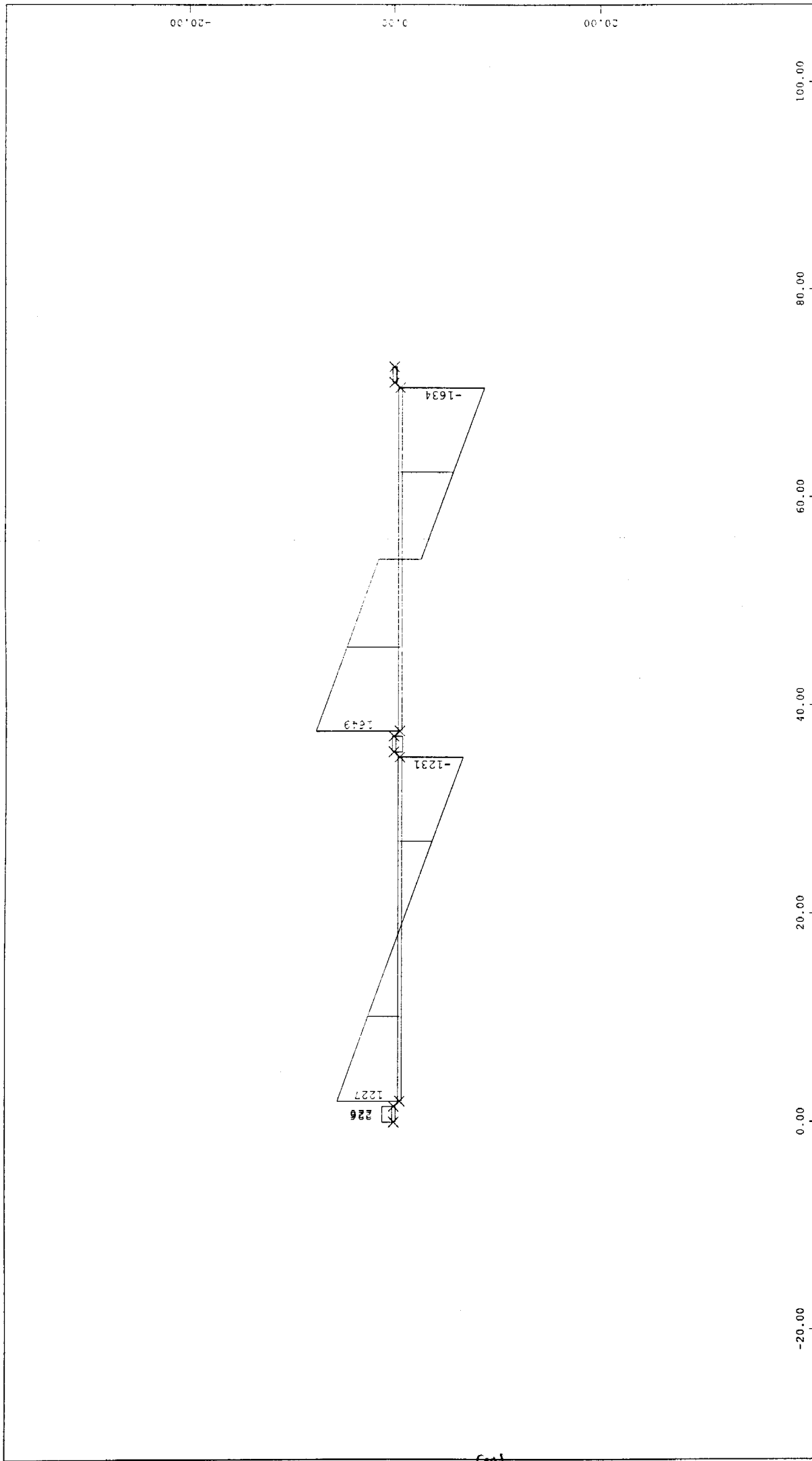


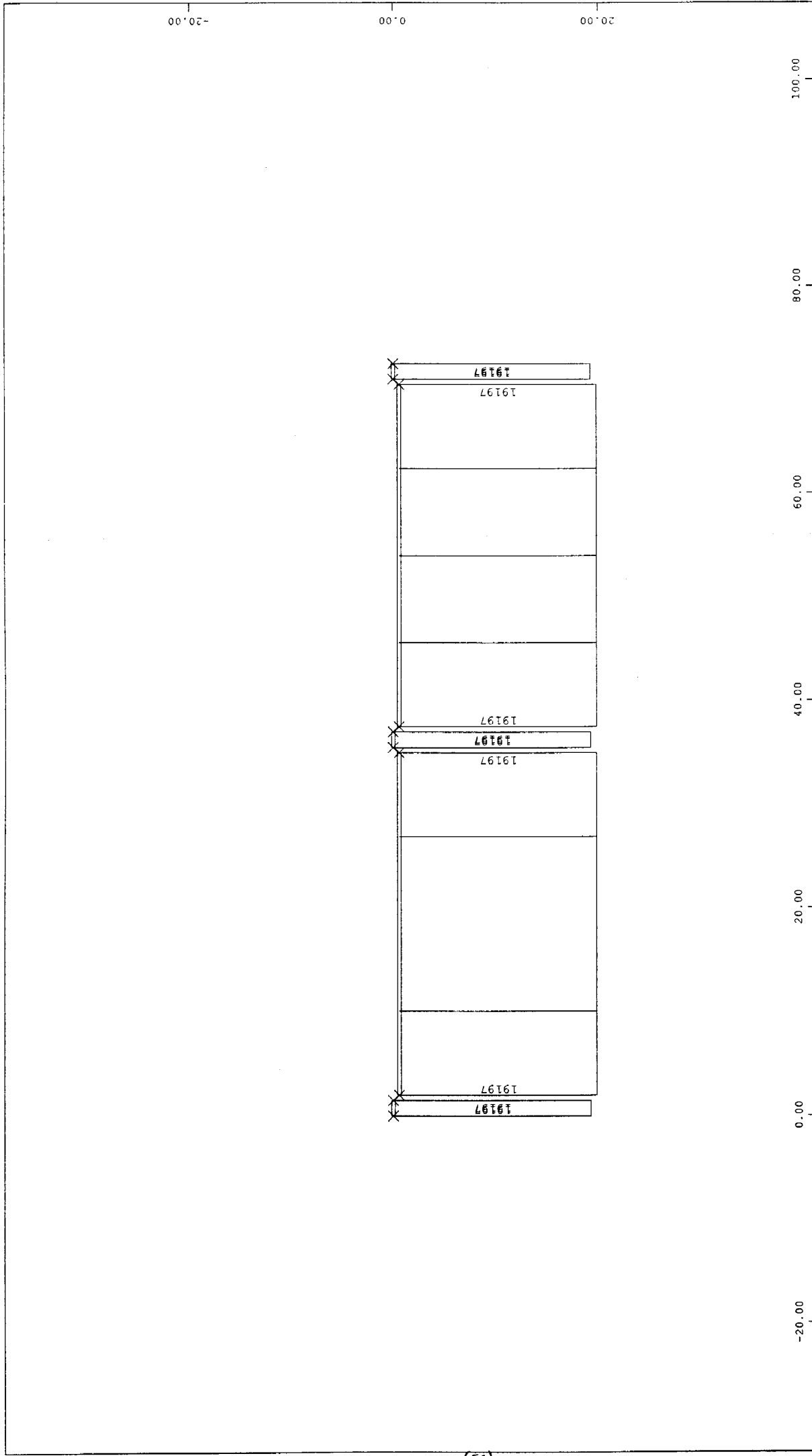
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM MOMENTS MY LC 2 OPT. MON.+KIN.+ΘΕΡΜΟΚΡ. 1 CM = 3500 kNm

M 1 : 500



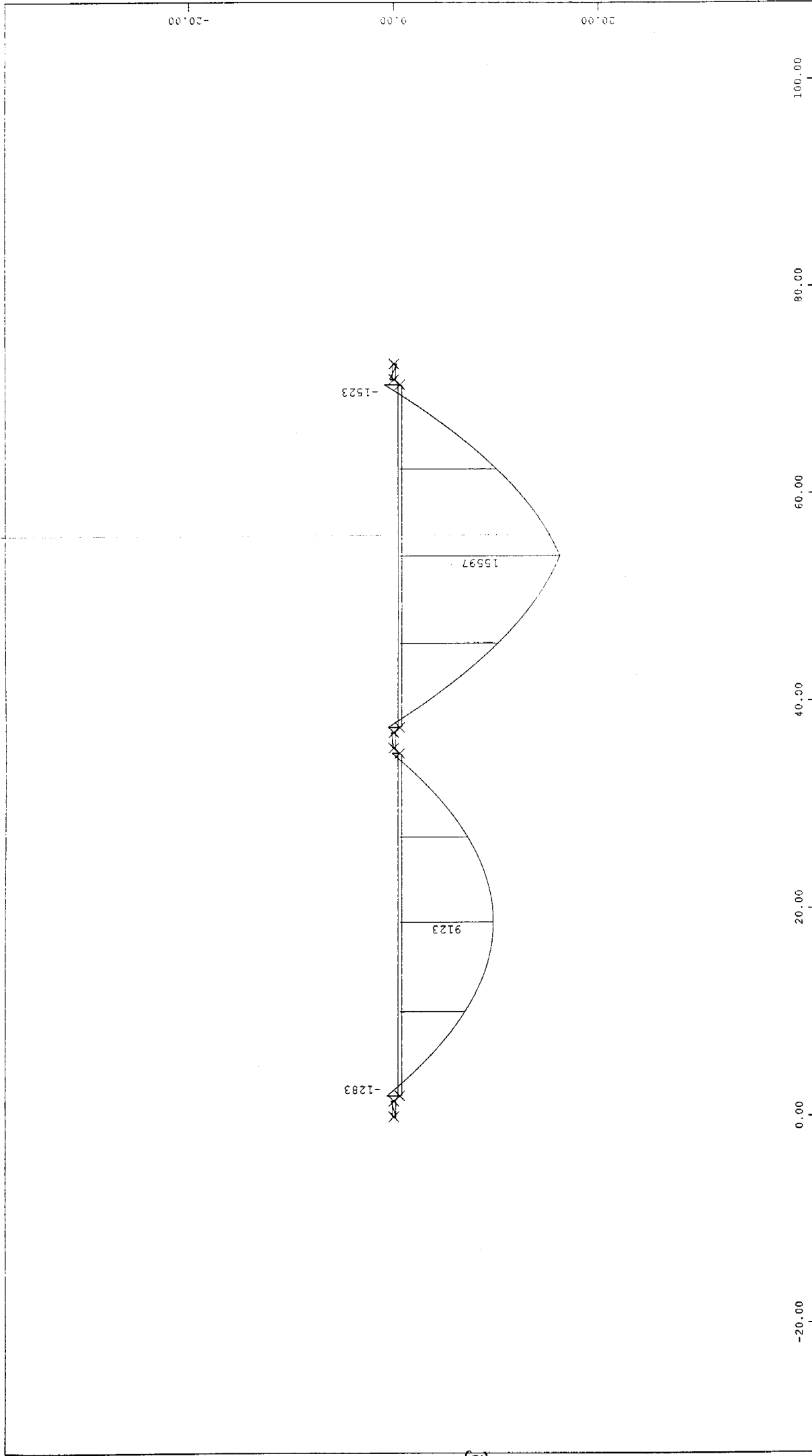


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM NORMAL FORCES LC 2 Φ OPT. MON.+KIN.+ Φ EPMOKP. 1 CM = 5000 kN

M 1 : 500

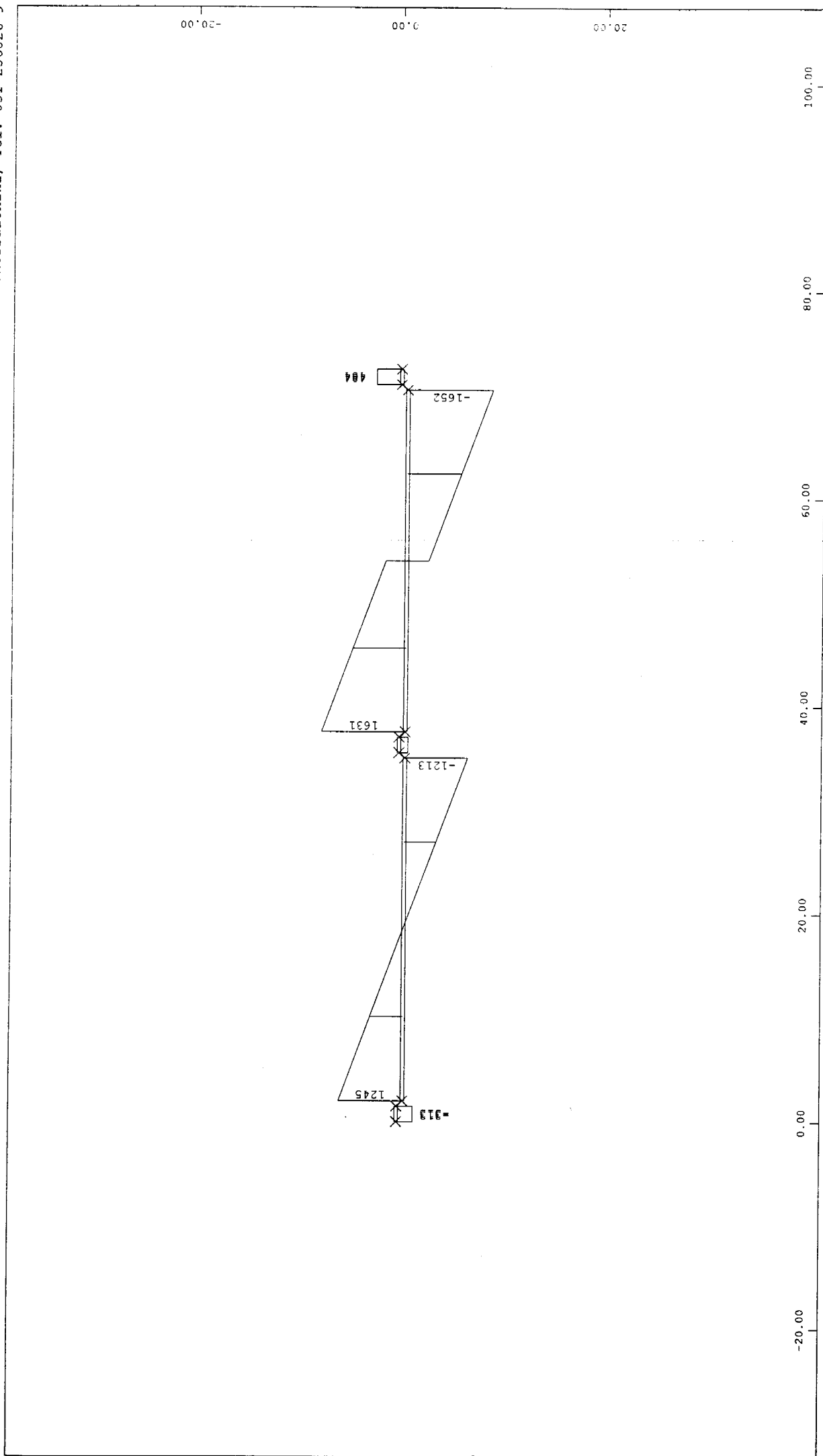


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

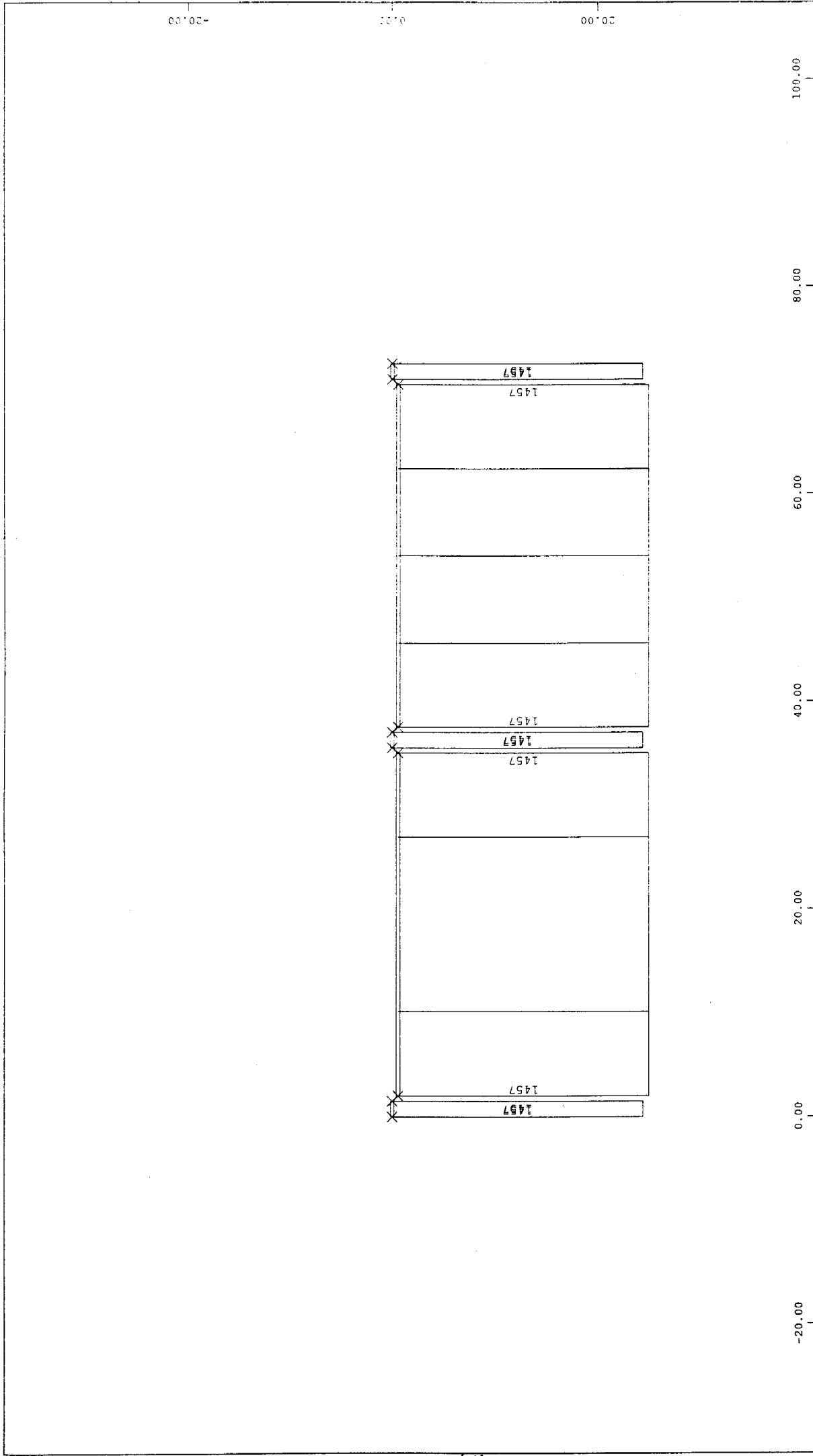
SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM MOMENTS MY LC 1 MONIMA+KINHHTA ΦOPTIA 1 CM = 5000 kNm

M 1 : 500



M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

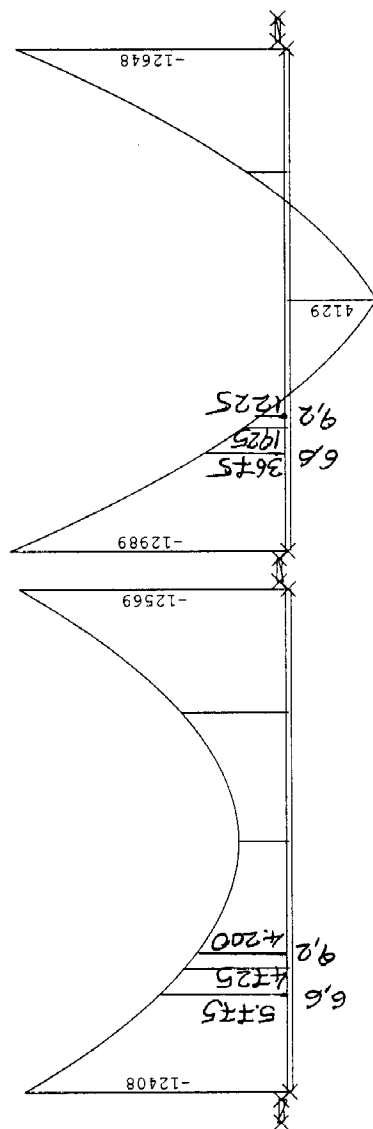
SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM NORMAL FORCES LC 1 MONIMA+KINHTA ΦOPTIA 1 CM = 300.0 kN

M 1 : 500

ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\begin{aligned} \text{on } \Delta M (x = L_{\text{eff}}) - M_{\text{cr}} &= -\left[\frac{V_{\text{eff}}}{2} - \frac{V_{\text{eff}}}{2} \right] + \frac{V_{\text{eff}}}{A_{\text{eff}}} \Delta N \sim 0,5(5775 + 3675) - 3814(3500 - \frac{22154}{5,1}) = -1,38 \Delta N_1 \rightarrow \Delta N_1 = -5750 \text{ kN} \rightarrow \\ N_1 &= 22154 - 5750 = 16400 \text{ kN} \rightarrow x_1 = 1585 \times 22154 / 16400 = 1985 \text{ m} \rightarrow L_{\text{eff},1} = 0,5(1985 - 265) = 920 \text{ m} \rightarrow 0,5(4200 + 1225) + 3220 = \\ &= -1,38 \Delta N_2 \rightarrow \Delta N_2 = -4300 \text{ kN} \rightarrow N_2 = 17850 \text{ kN} \rightarrow x_2 = 1585 \times 22154 / 17850 = 1825 \text{ m} \rightarrow L_{\text{eff},2} = 0,5(4726 + 1925) + \\ &+ 3220 = -1,38 \Delta N_3 \rightarrow \Delta N_3 = -4740 \text{ kN} \rightarrow N_3 = 17400 \text{ kN} \rightarrow x_3 = 15,85 \times 22154 / 17400 = 2020 \text{ m} \rightarrow L_{\text{eff},3} = 0,5(875 + 75) \rightarrow \\ &\rightarrow N = 17350 \text{ kN} \end{aligned}$$

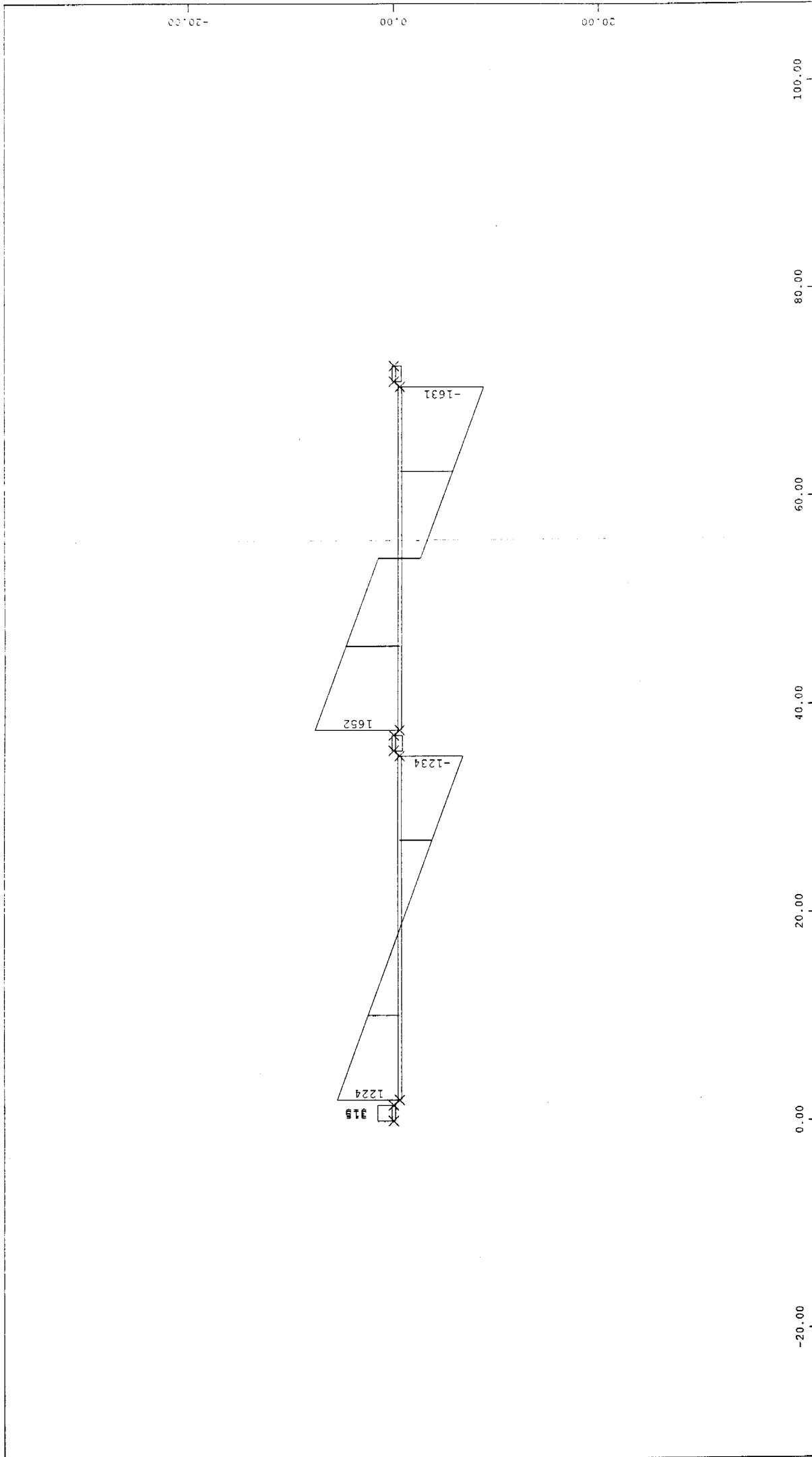


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM MOMENTS MY IC 2 OPT. MON.+KIN.+ΘΕΡΜΟΚΡ. 1 CM = 3500 kNm

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

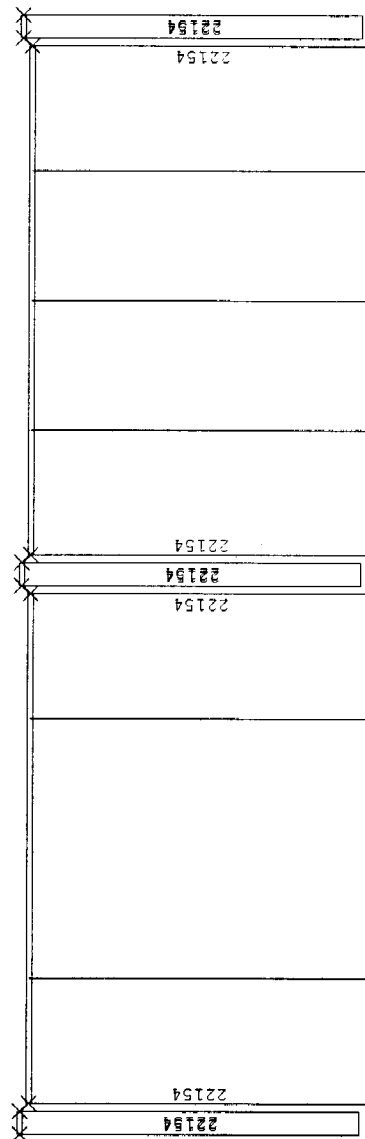
SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM SHEAR FORCES QZ LC 2 ΦOPT. MON.+KIN.+ΘEPMOKP. 1 CM = 1000 kN

M 1 : 500

ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$v \Delta M (x = L_{eff}) - M_{cr} = - \left[\gamma_2 - 0.5 h_{p,eff} \right] + \frac{W_{2,eff}}{A_{eff}} \Delta N \rightarrow 0.5 ($$

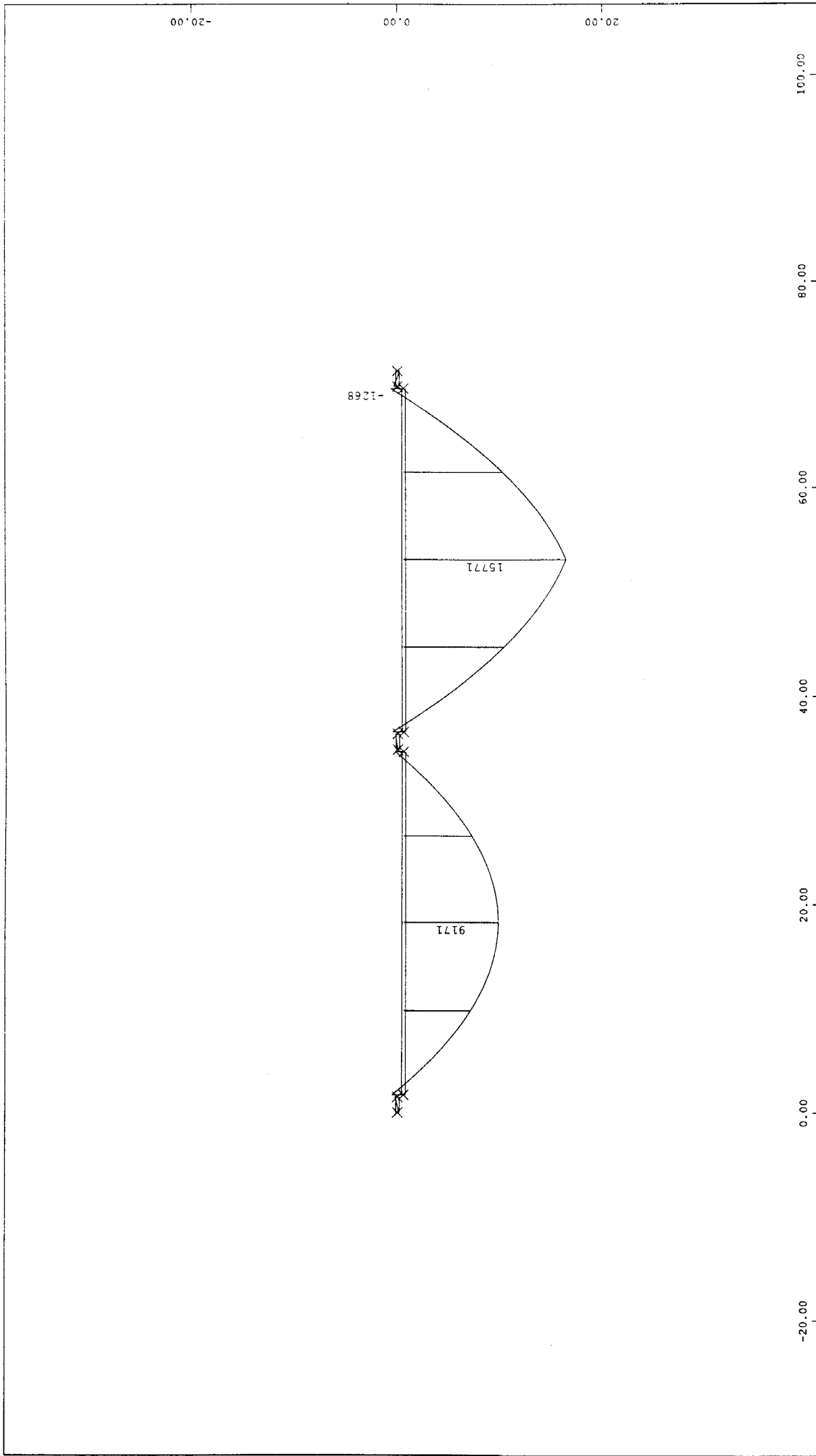


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

-----BEAM NORMAL FORCES LC 2 OPT. MON.+KIN.+ΘΕΡΜΟΚΡ. 1 CM = 5000 kN

M 1 : 500



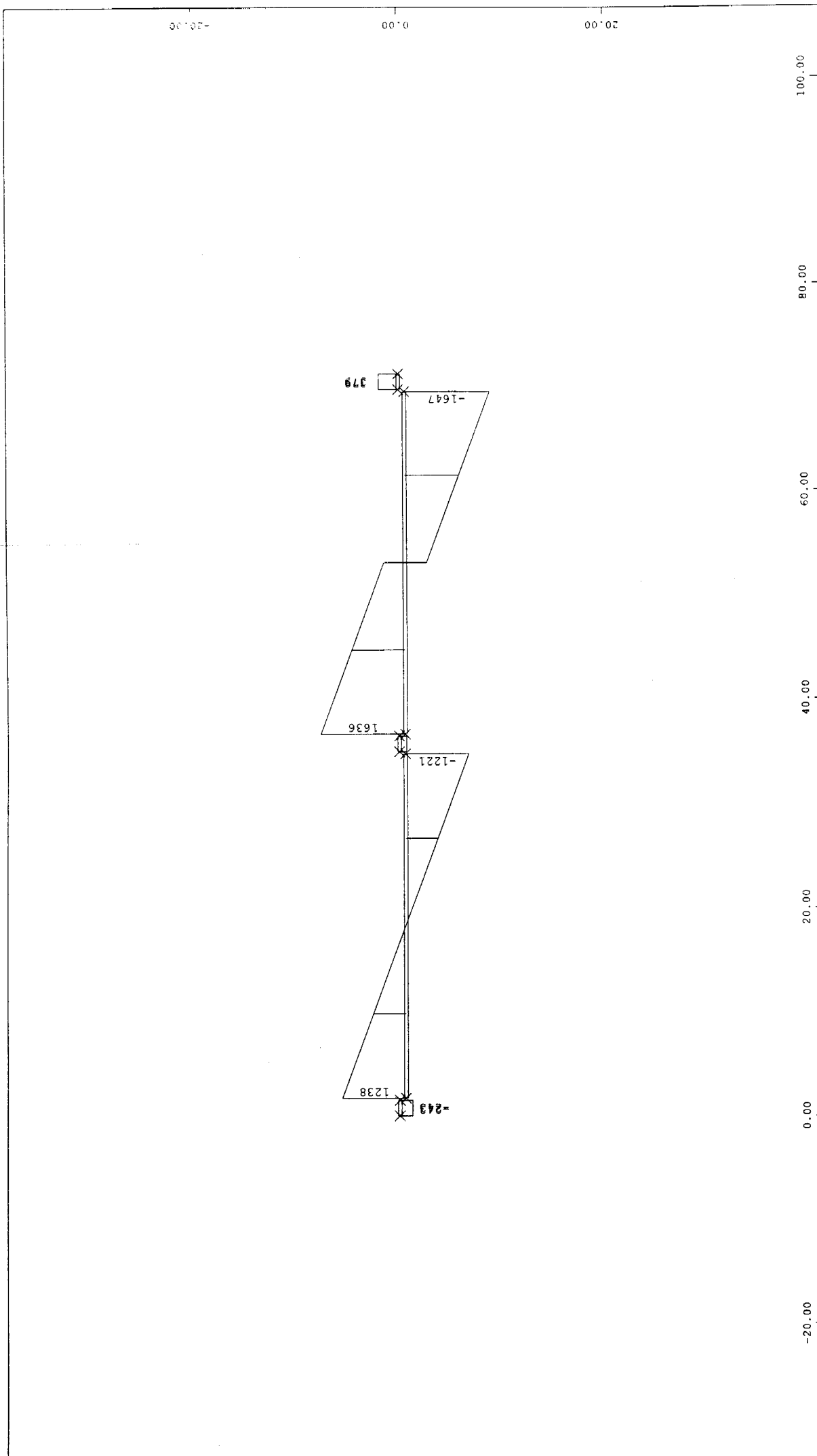
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM MOMENTS MY LC 1 LOAD CASE 1 1 CM = 5000 kNm

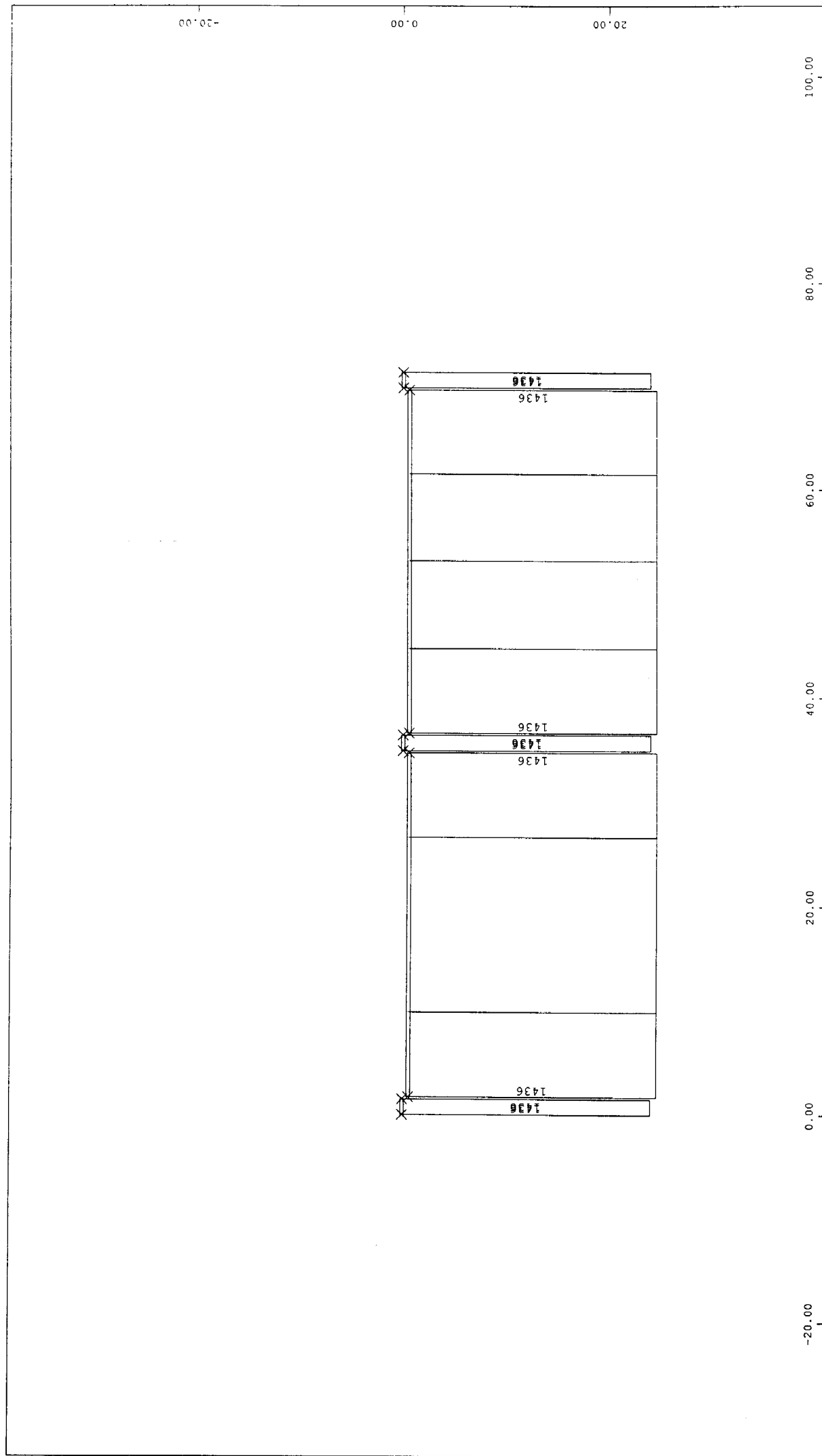
M 1 : 500

z



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
——— BEAM SHEAR FORCES QZ LC 1 LOAD CASE 1 1 CM = 1000 kN

M 1 : 500

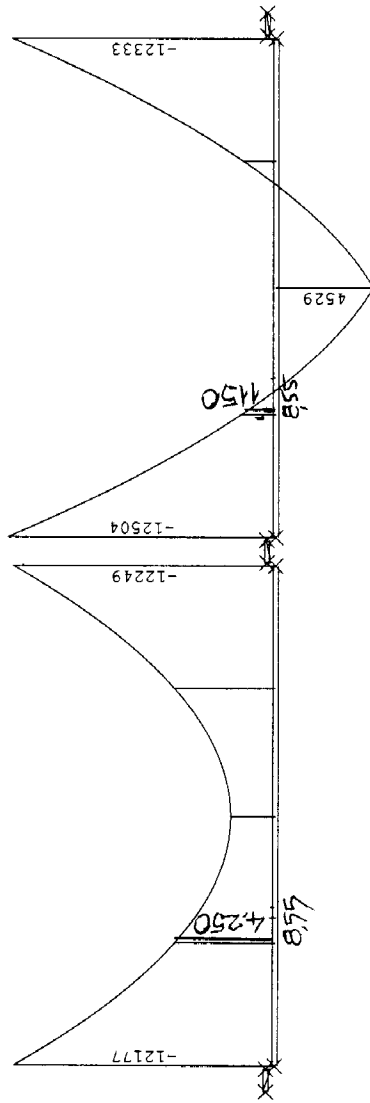


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM NORMAL FORCES LC 1 LOAD CASE 1 1 CM = 300.0 kN

M 1 : 500



(19)

$$v_n \Delta M(x=8.55) \approx 0.5(4.250 + 11.50) = 2.700 \text{ kNm}$$

$$d_n \Delta M \approx \frac{2.784}{0.73} \left(3500 - \frac{21.450}{5.1} \right) = -2.640 \text{ "}$$

$$2.700 + 2.690 = 5390 = -1.38 \Delta N_1 \rightarrow \Delta N_1 = -3910 \text{ kN} \rightarrow N_1 = 21450 - 3910 = 17.540 \text{ kN} \rightarrow x_1 = \frac{21450}{17.540} = 22.75 \text{ m}$$

$$l_{eff,1} = 0.5(22.75 - 2.65) = 10.60 \text{ m} \rightarrow 0.5(3325 - 525) + 2690 = 4090 = -1.38 \Delta N_2 \rightarrow \Delta N_2 = -2960 \text{ kN} \rightarrow N_2 = 21450 - 2960 = 18.490 \text{ kN}$$

$$x_2 = 19.75 \times 21450 / 18.490 = 21.60 \text{ m} \rightarrow l_{eff,2} = 10.0 \text{ m} \rightarrow 0.5(3500 - 200) + 2690 = 4340 = -1.38 \Delta N_3 \rightarrow \Delta N_3 = -3140 \text{ kN}$$

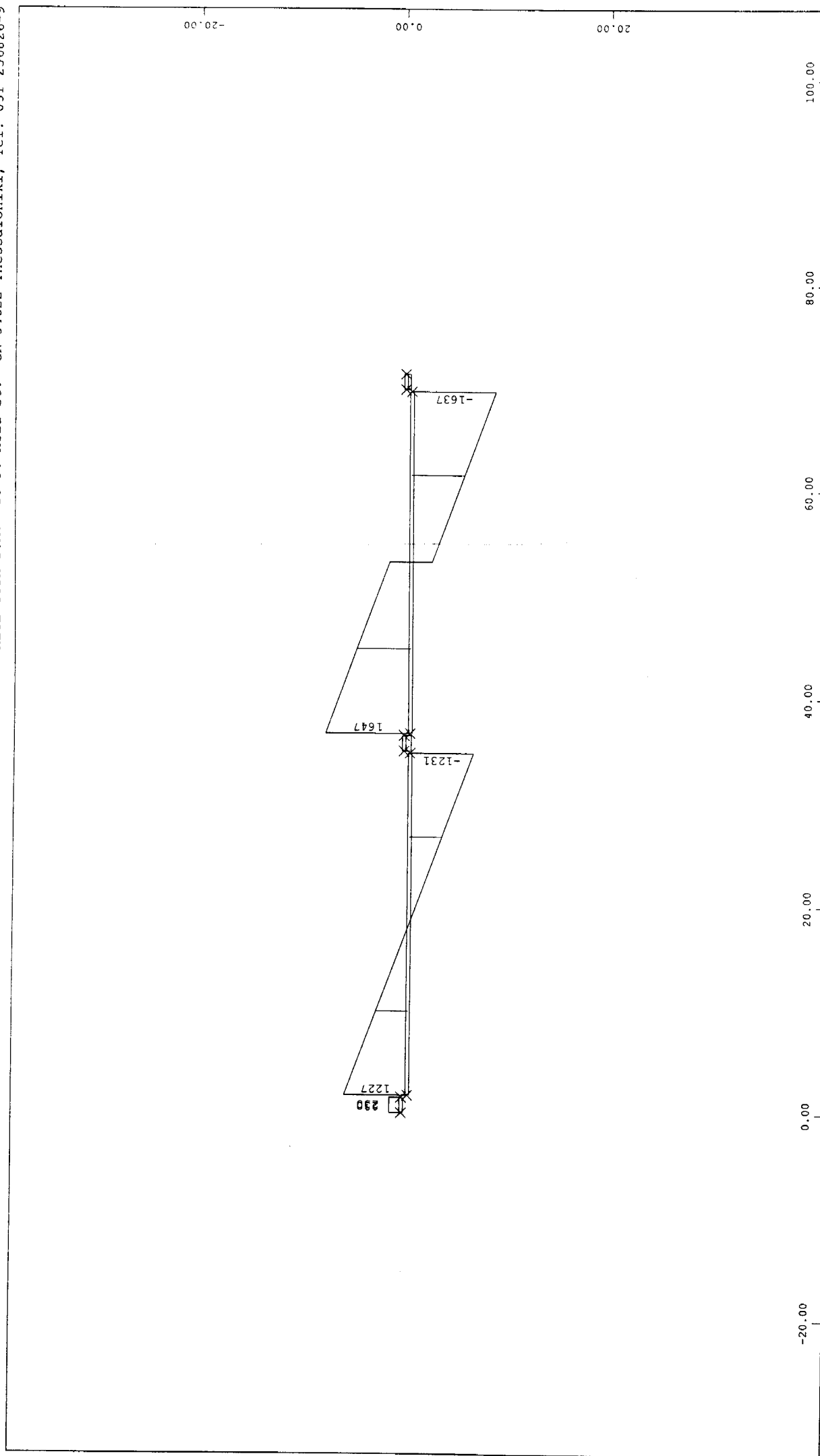
$$N_3 = 21450 - 3140 = 18.300 \text{ kN} \rightarrow x_3 = 23.10 \text{ m} \rightarrow l_{eff,3} = 10.25 \text{ m}$$

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

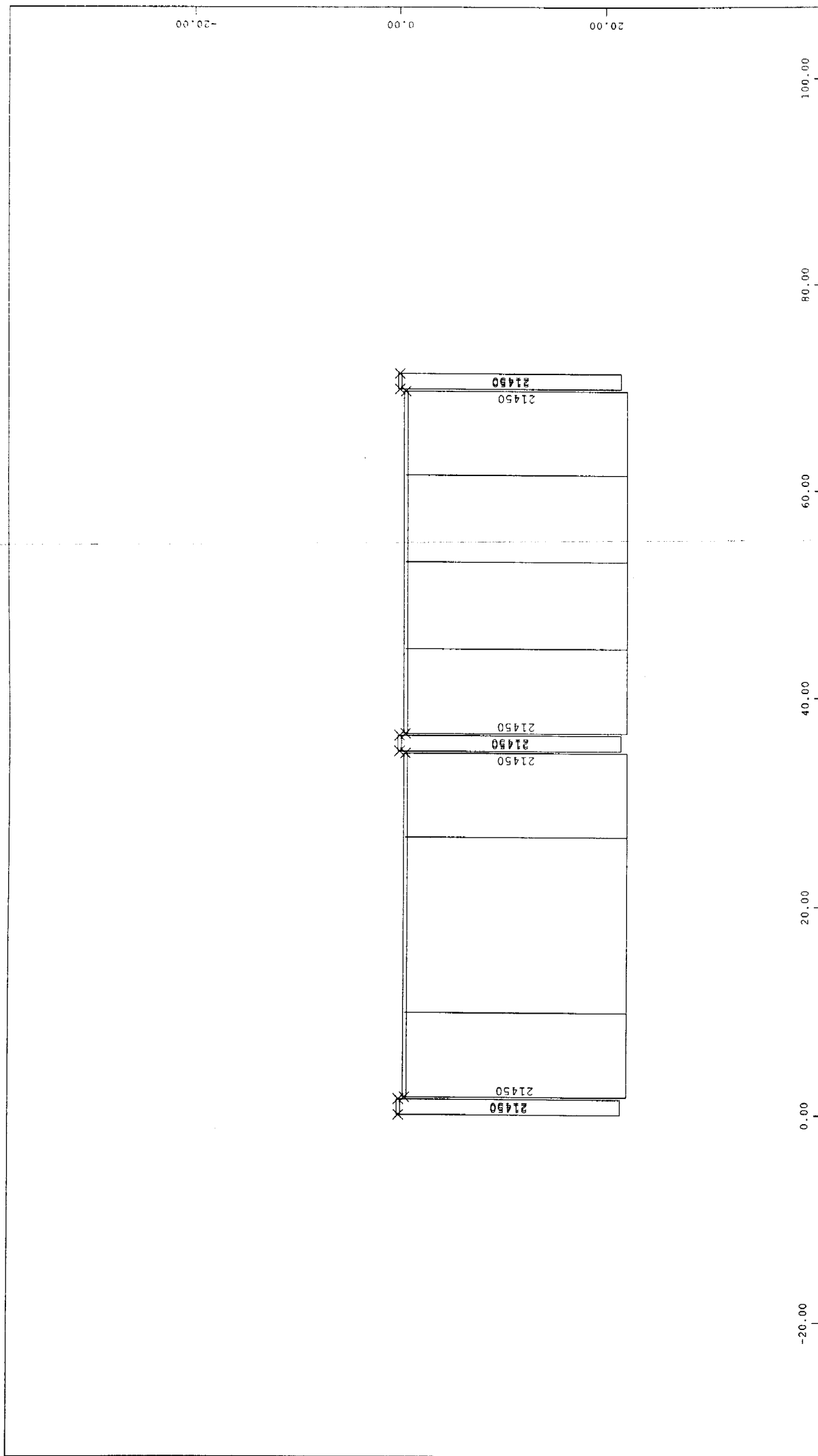
— BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 ——— BEAM SHEAR FORCES QZ LC 2 LOAD CASE 2 1 CM = 1000 kN

M 1 : 500

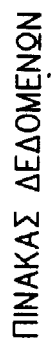


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0

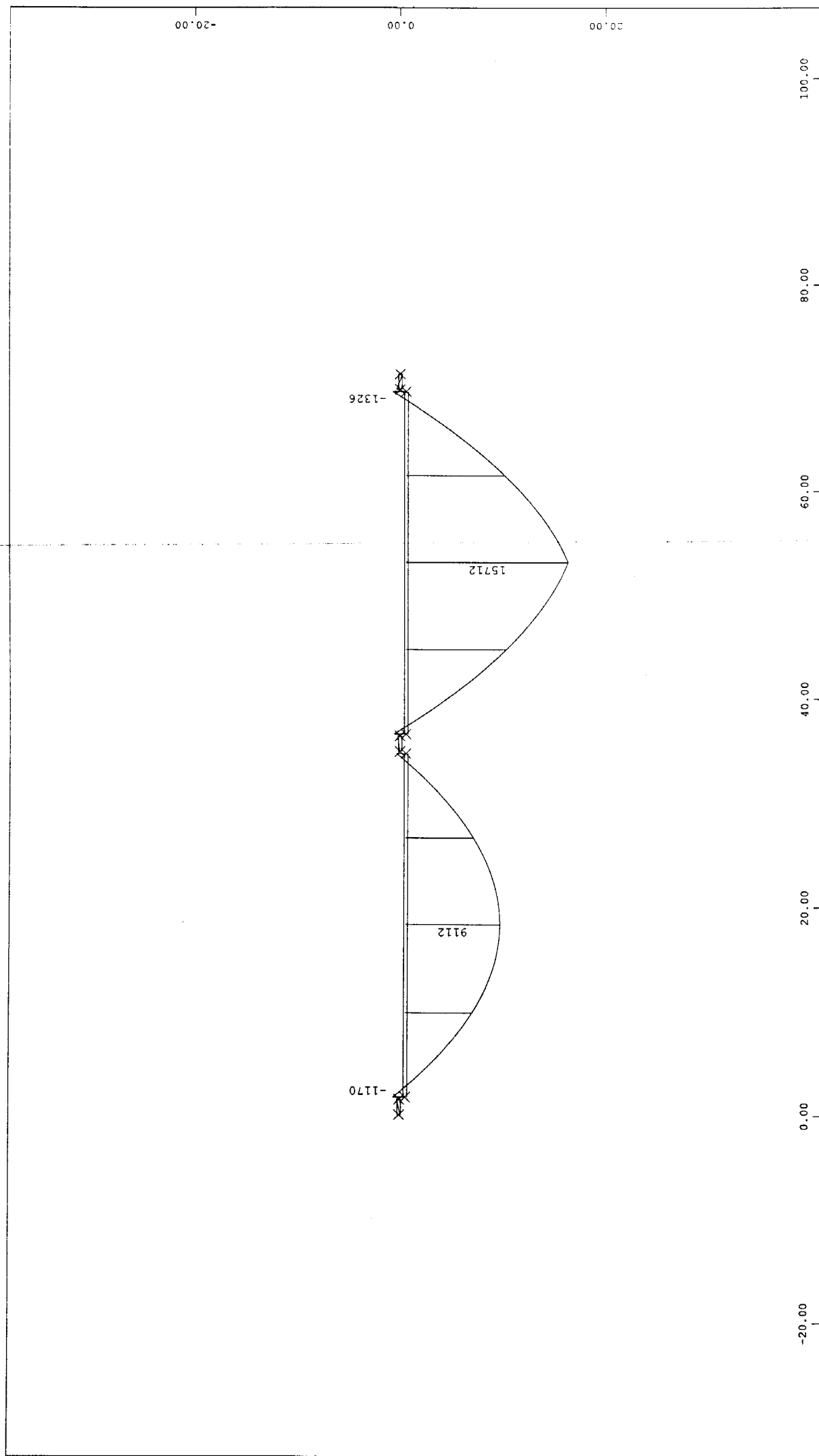
BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

M 1 : 500

$$AC_2 = \frac{1.50}{1.50 + 2L_{\text{eff}}} \quad 1.2As \frac{Es}{Ec}$$



(64)

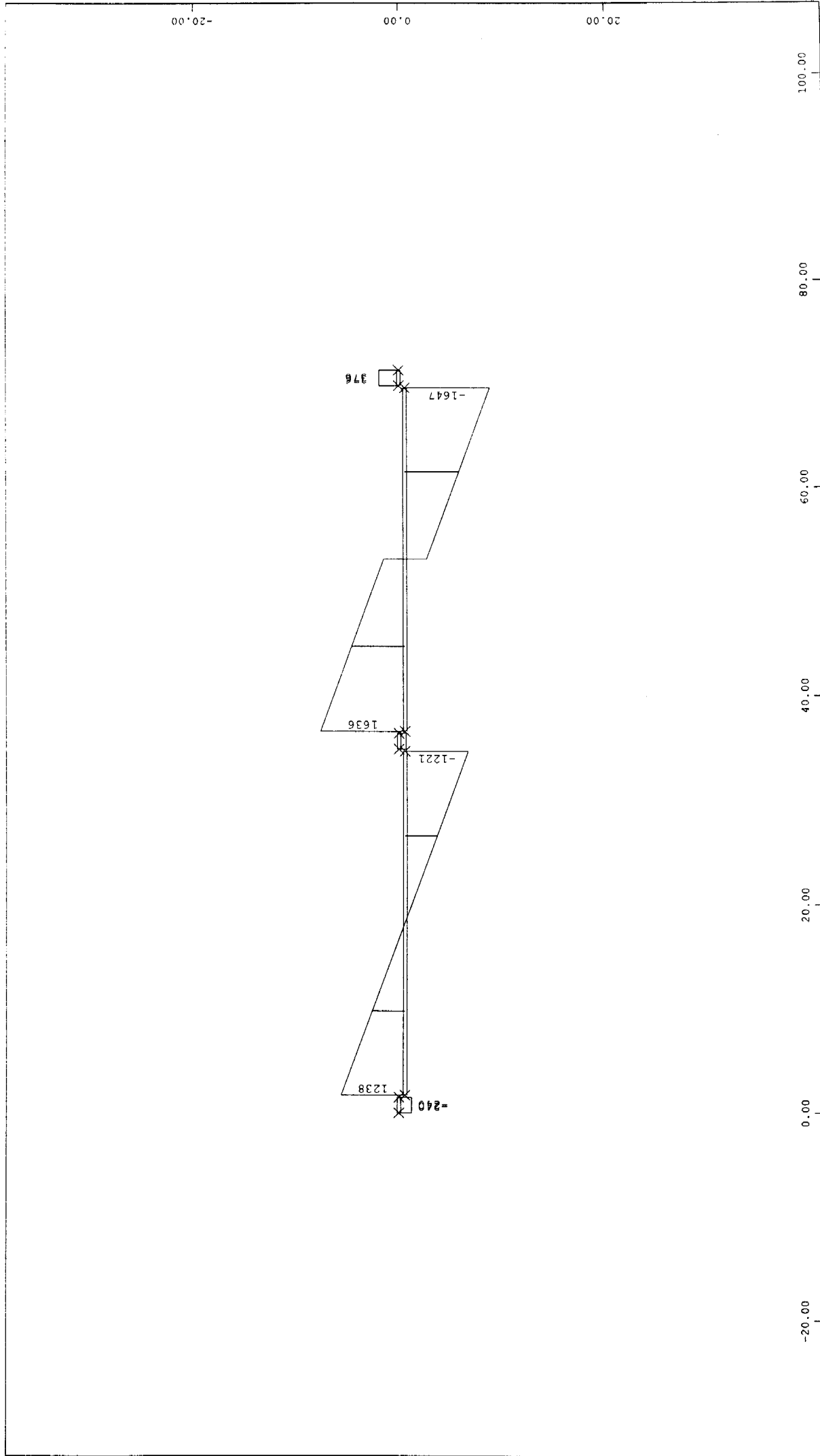


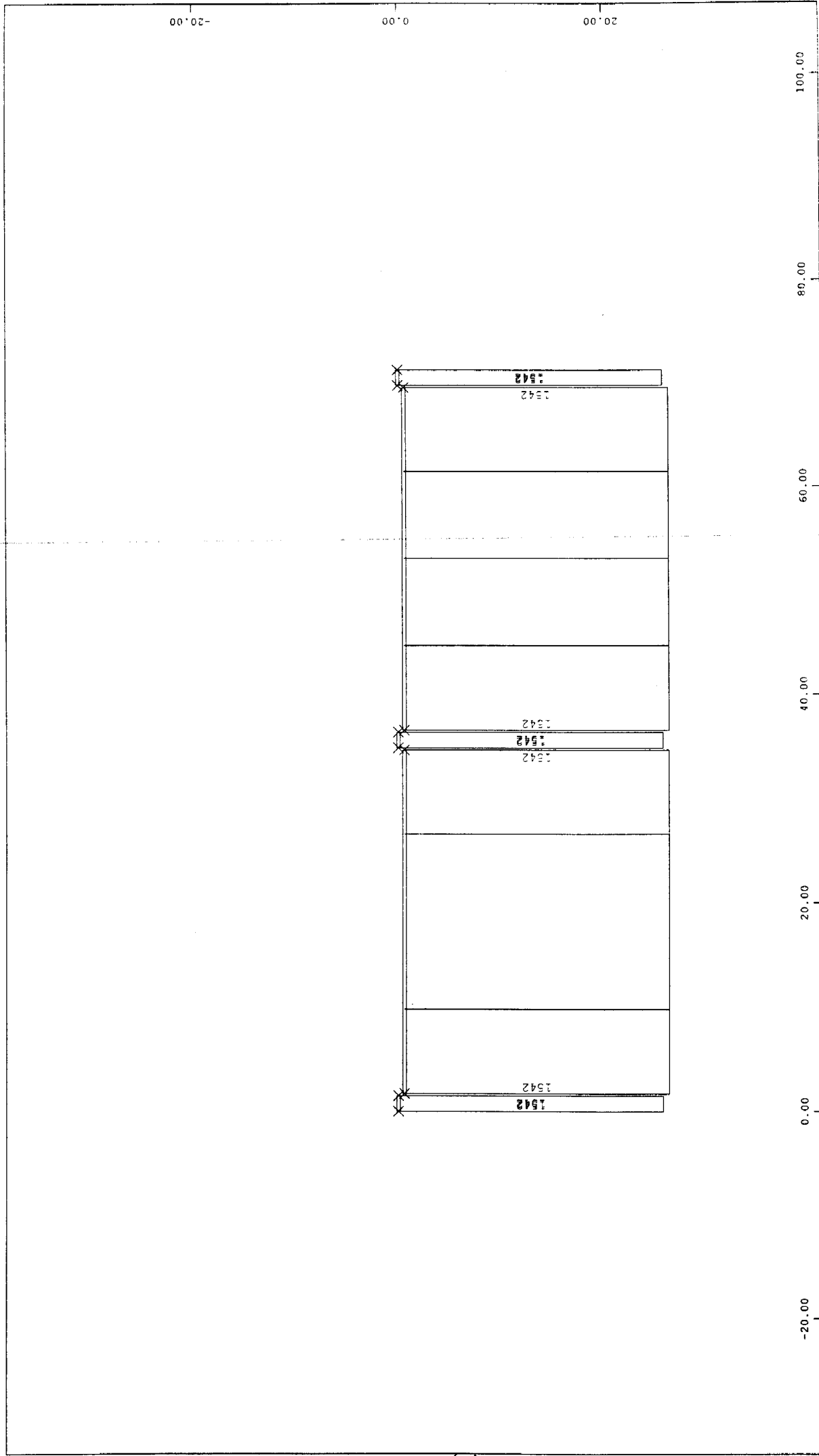
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

----- BEAM MOMENTS MY IC 1 LOAD CASE 1 1 CM = 5000 kNm

M 1 : 500





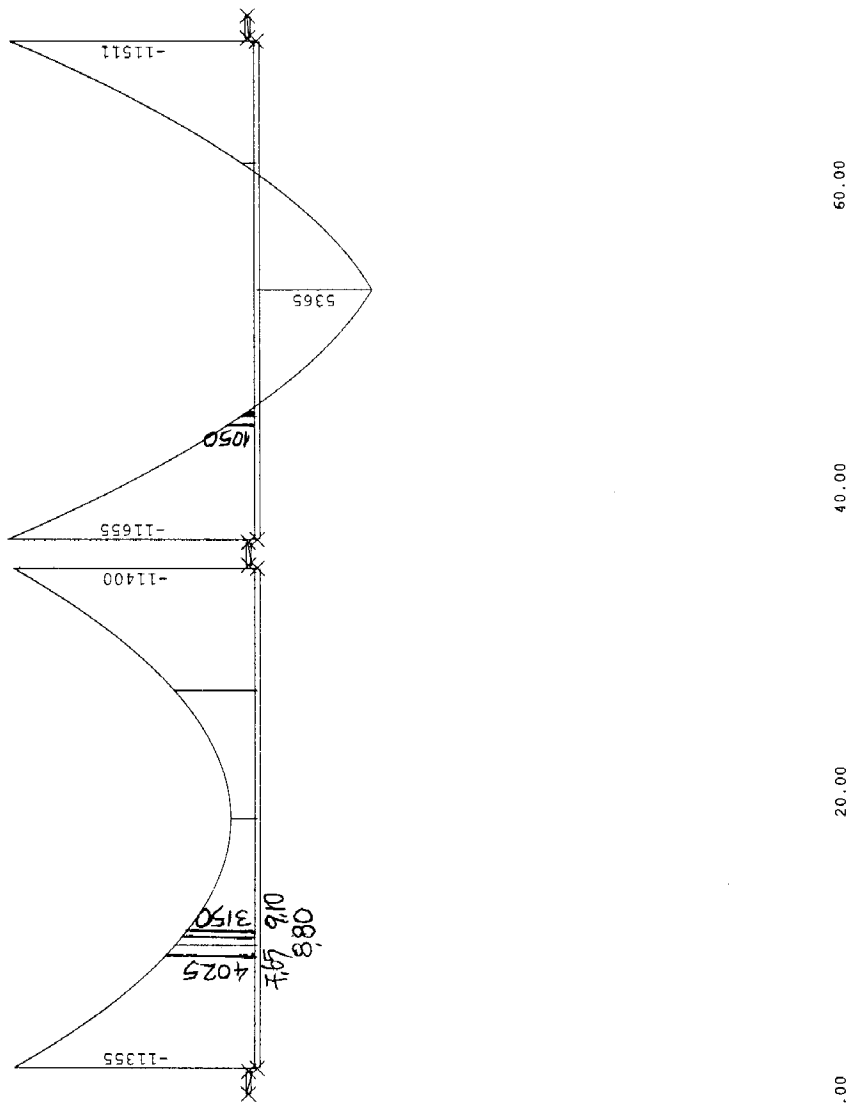
M 1 : 500

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
——— BEAM NORMAL FORCES LC 1 LOAD CASE 1 1 CM = 300.0 kN

x
y
z

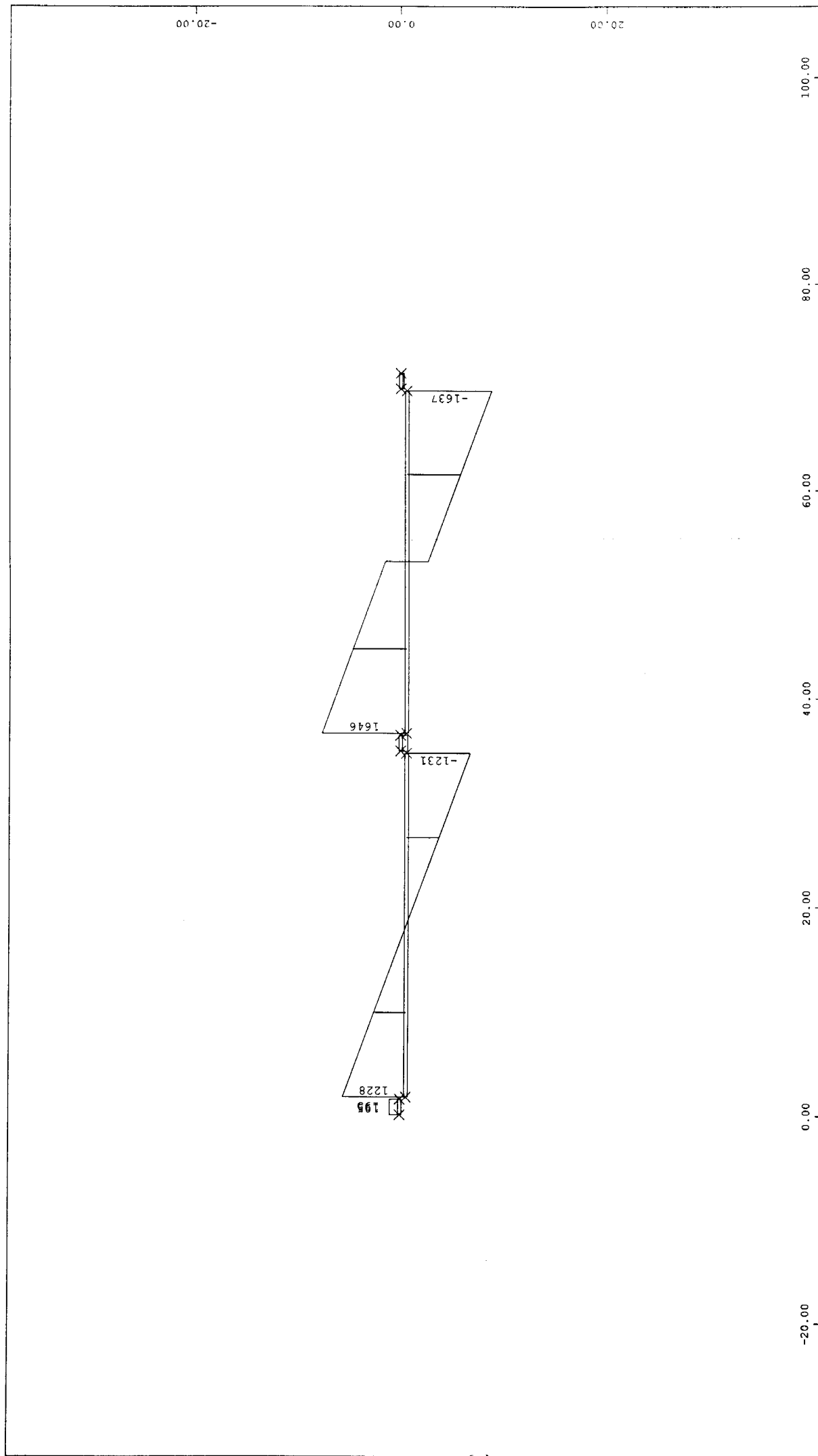
ΘΑ ΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\begin{aligned} \text{UN } \Delta M (x=7,65) &= 3814 \left(3500 - \frac{19962}{51} \right) = -1,38 \Delta N_1 \rightarrow 0,5(4025+1050)+1580 = -1,38 \Delta N_1 \rightarrow \Delta N_1 = -2,980 \text{ kN} \rightarrow N_1 = 19962 - 2980 = \\ &= 16980 \text{ kN} \rightarrow x_1 = \frac{19962 \cdot 1795}{16980} = 21,10 \text{ m} \rightarrow L_{\text{eff},1} = (21,1 - 2,65)/2 = 9,10 \text{ m} \rightarrow \Delta M (x=9,10) = 0,5 \times (3150 + \varnothing) = 1575 \text{ kNm} \\ 1575 + 1580 &= -1,38 \Delta N_2 \rightarrow \Delta N_2 = -2286 \text{ kN} \rightarrow N_2 = 19962 - 2286 = 17,680 \text{ kN} \rightarrow x_2 = \frac{1795 \times \frac{19962}{17680}}{17680} = 20,25 \text{ m} \rightarrow L_{\text{eff},2} = 8,80 \text{ m} \\ \Delta M (x=8,80) &= 0,5(3325 + 125) = 1750 \text{ kN} \rightarrow 1750 + 1580 = -1,38 \Delta N_3 \rightarrow \Delta N_3 = -2412 \text{ kN} \rightarrow N_3 = 19962 - 2412 = 17550 \text{ kN} \\ x_3 &= 1795 \times 19962 / 17550 = 20,40 \text{ m} \rightarrow L_{\text{eff},3} = 8,85 \text{ m} \end{aligned}$$



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500

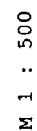


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM SHEAR FORCES QZ LC 2 LOAD CASE 2 1 CM = 1000 KN

M 1 : 500

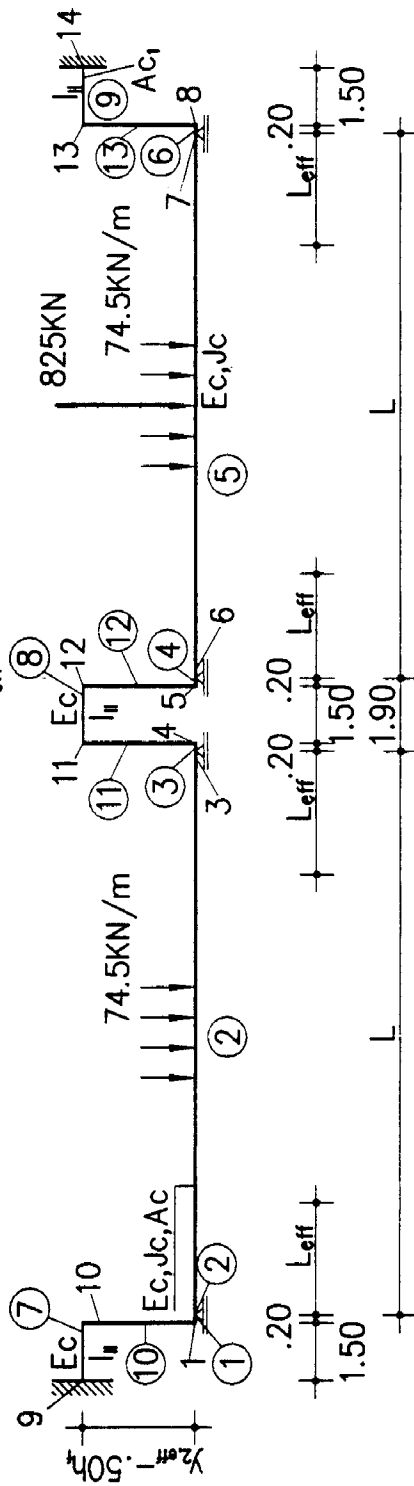


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
-----BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

2

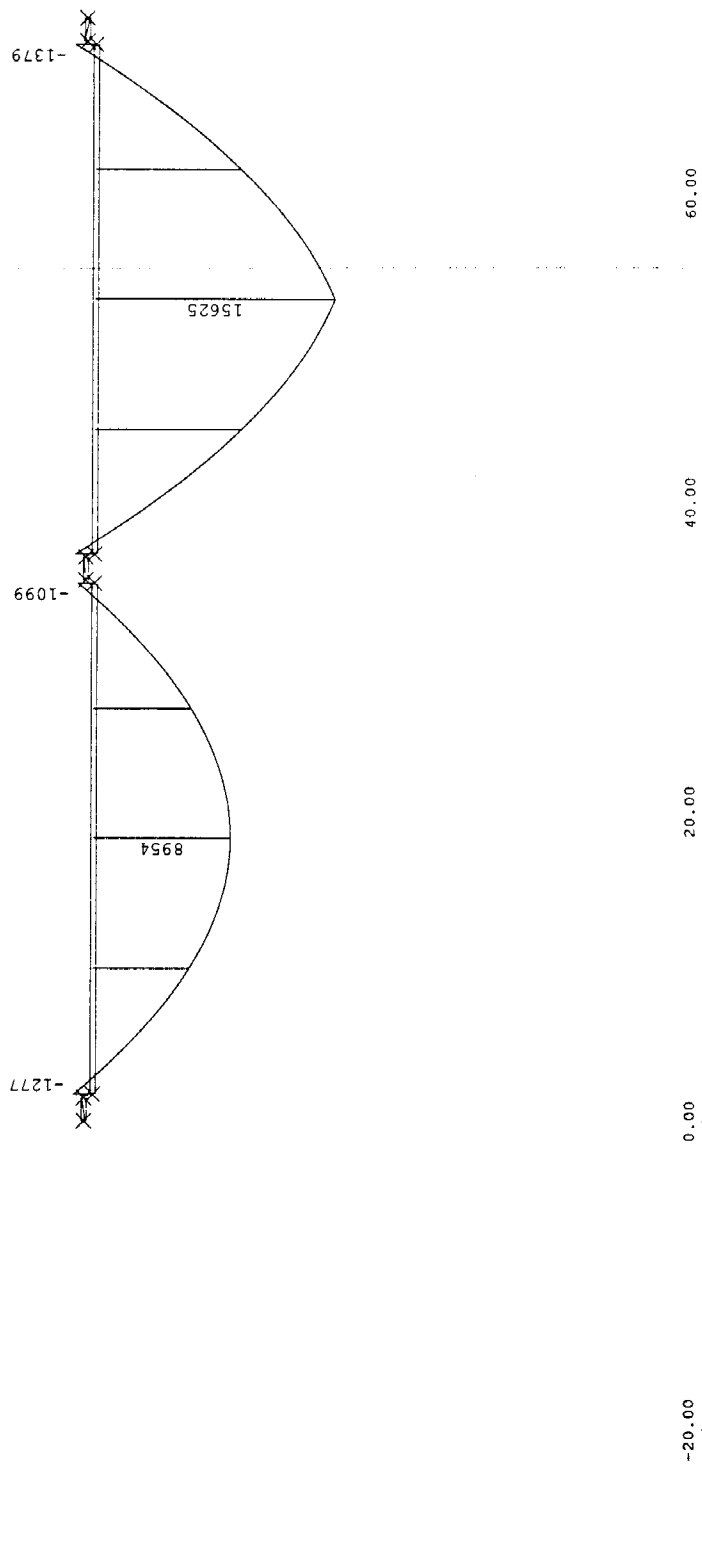
$$A_{C1} = \frac{1.50}{1.50 + L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$

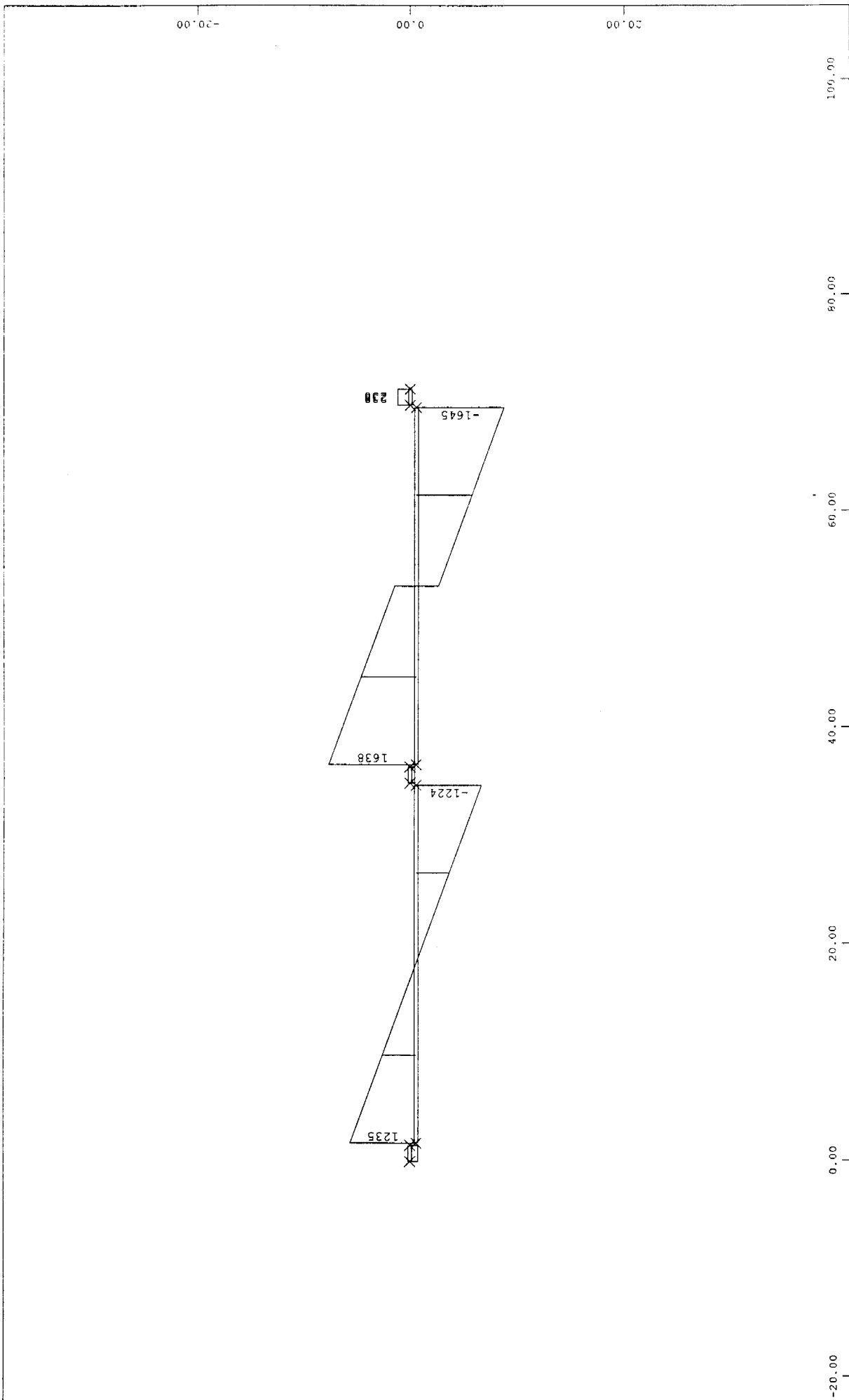
$$A_{C2} = \frac{1.50}{1.50 + 2L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$

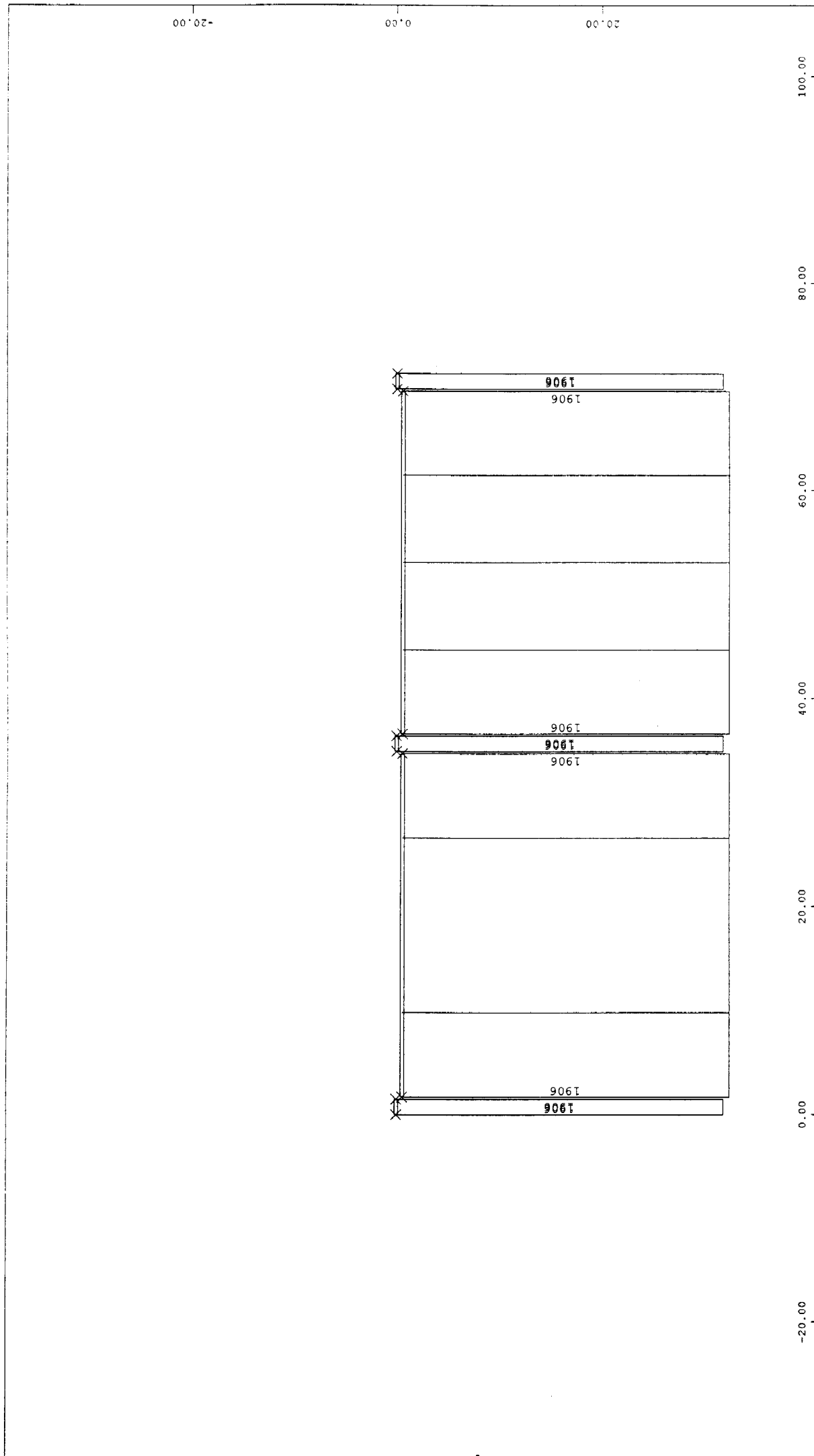


ΠΙΝΑΚΑΣ ΔΕΔΟΜΕΝΩΝ

$L = 33.0m$	$E_c = 32 \text{ GPa}$
$b = 12.0m$	$\alpha = 6.25$
$A_{c,eff} = 5.100m^2$	$g_1 = 30.7kN/m$
$J_{c,eff} = 2.784m$	$q = 43.8kN/m$
$h_b = 2.15m$	$g_1 + q = 74.5kN/m$
$h_{ft} = 0.275m$	$Q = 825kN$
$h_{r,eff} = 0.20m$	$A_{st} = 1280cm^2 (4\phi 16/15)$
$h_{(np.)} = 0.075m$	$\rho = 5.3\%$
$y_{2,eff} = 0.73m$	$A_{st} = 13.7 \frac{cm^2}{m} (\phi 16/150)$
	$T = -60/-70^\circ C$
	$L_{eff} = L/4 = 8.25$
	$\rho_b = 0.0076 (\phi 16/150)$
	$I_{II} = 3.544 \alpha \rho_b^3 h_{r,eff}^3 / 12 = 0.1772 \rho_b = 0.00135 m^4$







INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM NORMAL FORCES LC 1 LOAD CASE 1 1 CM = 300.0 kN

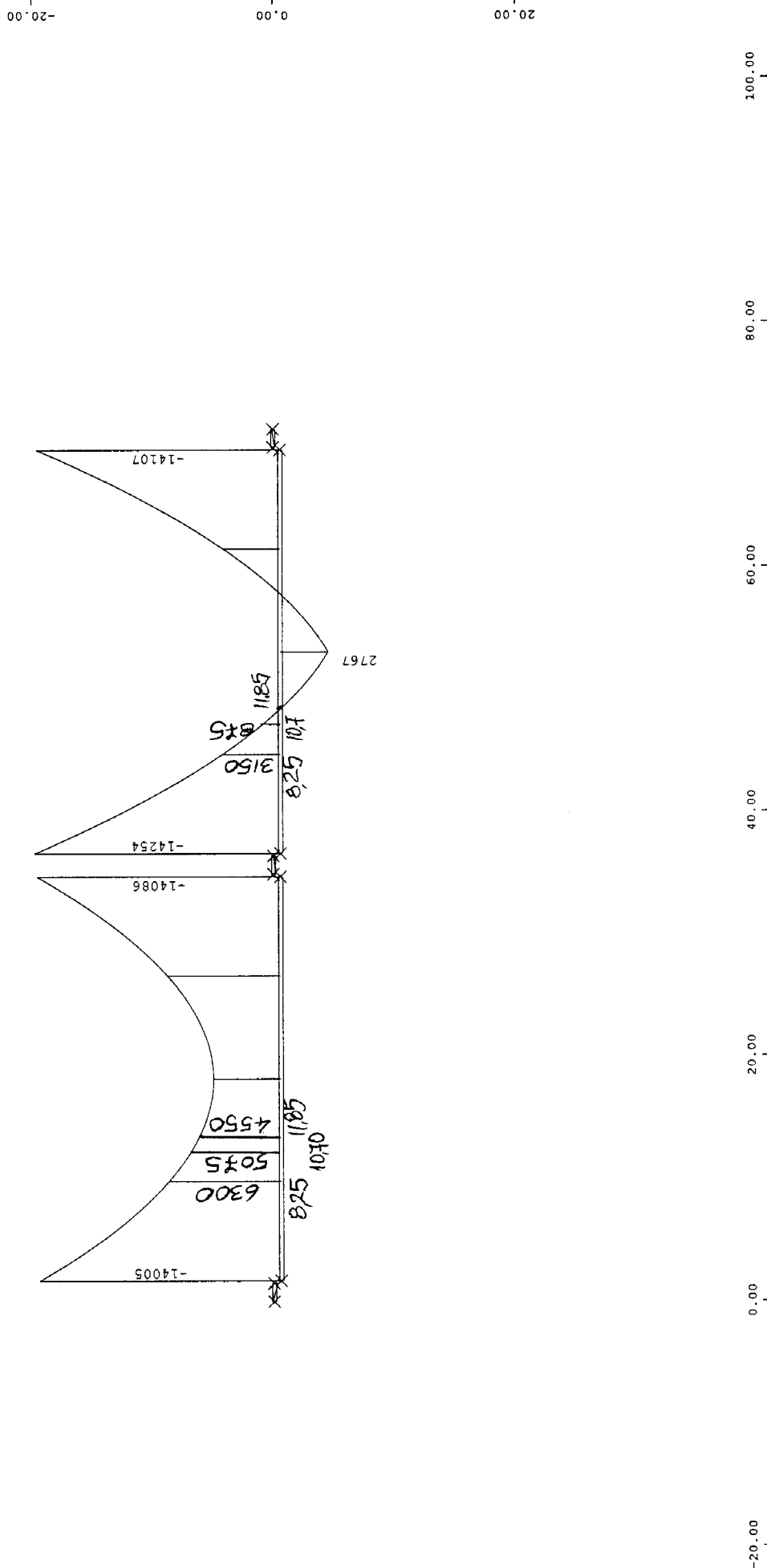
M 1 : 500

ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$0,5(6300 + 3150) + 3814(3500 - \frac{24.535}{5,1}) = -1,38 \Delta N_1 \rightarrow \Delta N_1 = -4050 \text{ kN} \rightarrow N_1 = 24535 - 4050 = 17490 \text{ kN} \rightarrow X_1 = (8 \times 825 + 245) \times 60^\circ$$

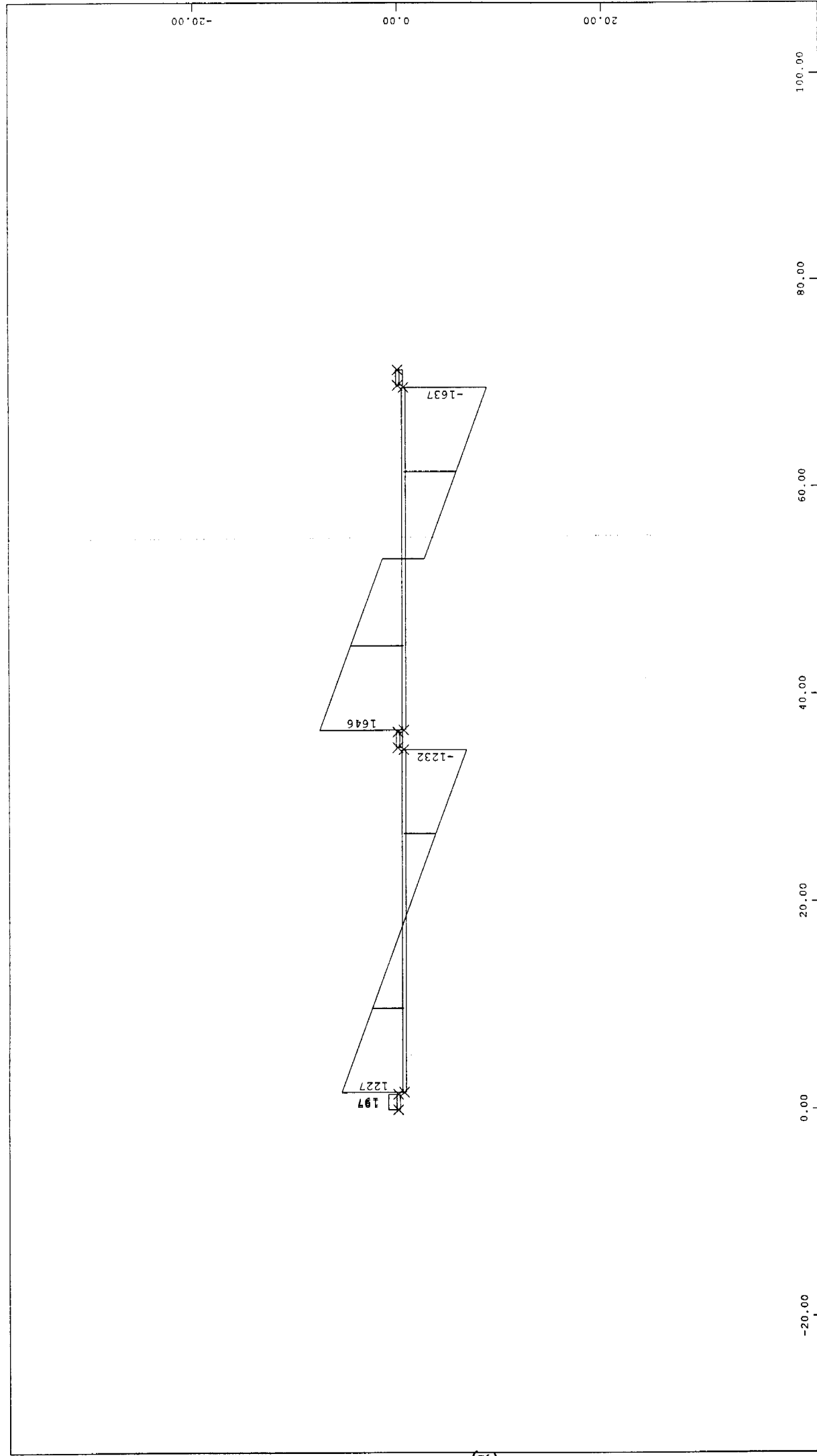
$$\times 24.535 / 17.490 = 25,95 \text{ m} \rightarrow L_{\text{eff}1} = 11,85 \text{ m} \rightarrow 0,5(4550 + \phi) + 5000 = -1,38 \Delta N_2 \rightarrow \Delta N_2 = -5240 \text{ kN} \rightarrow N_2 = 19.260 \text{ kN} \rightarrow X_2 = 19,5 \times 24.535 /$$

$$19.260 = 22,90 \text{ m} \rightarrow L_{\text{eff}2} = 10,70 \text{ m} \rightarrow 0,5(5075 + 875) + 5000 = -1,38 \Delta N_3 \rightarrow \Delta N_3 = -5480 \text{ kN} \rightarrow N_3 = 18.750 \text{ kN} \rightarrow L_{\text{eff}3} = 11,0 \text{ m}$$



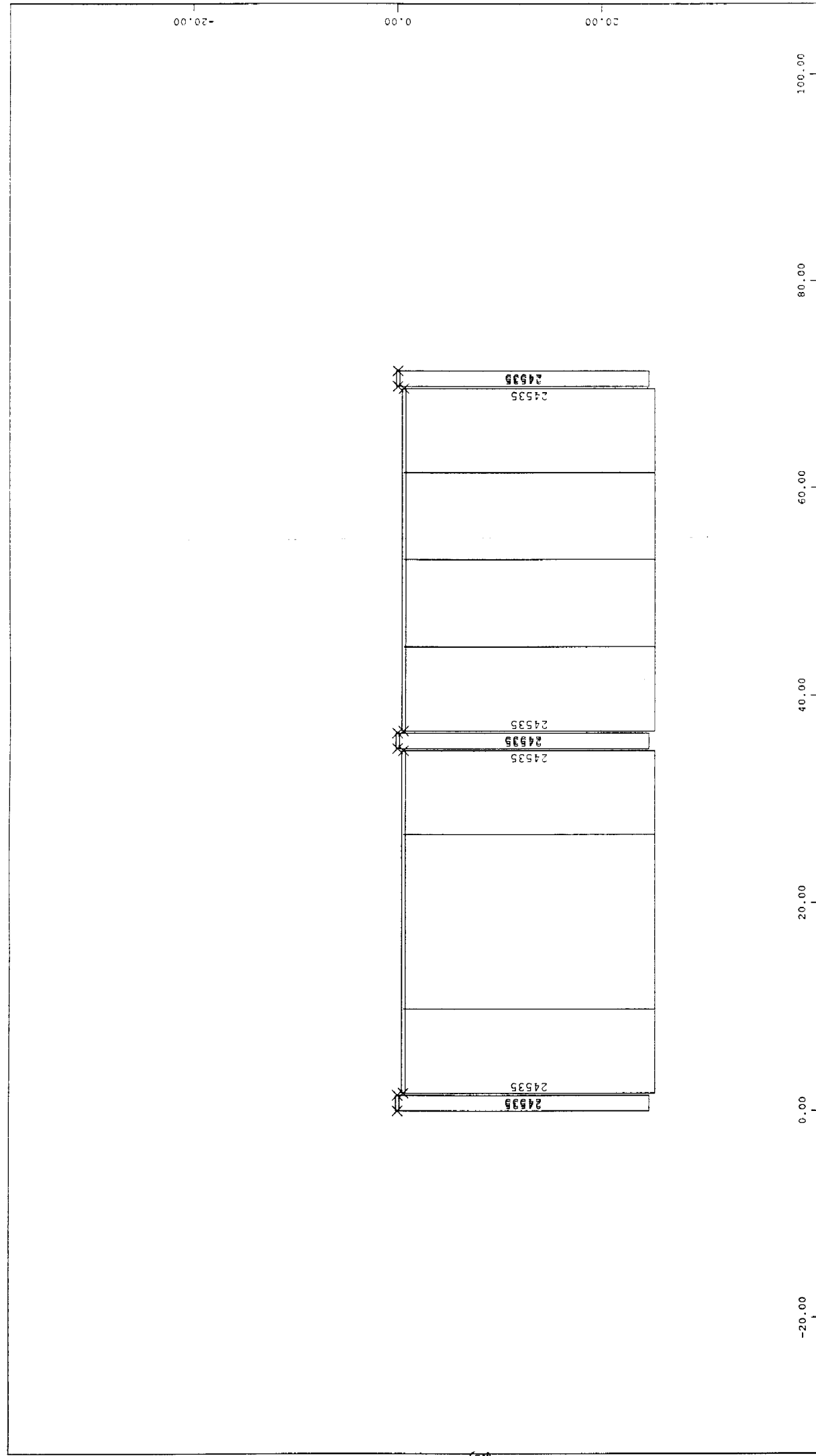
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

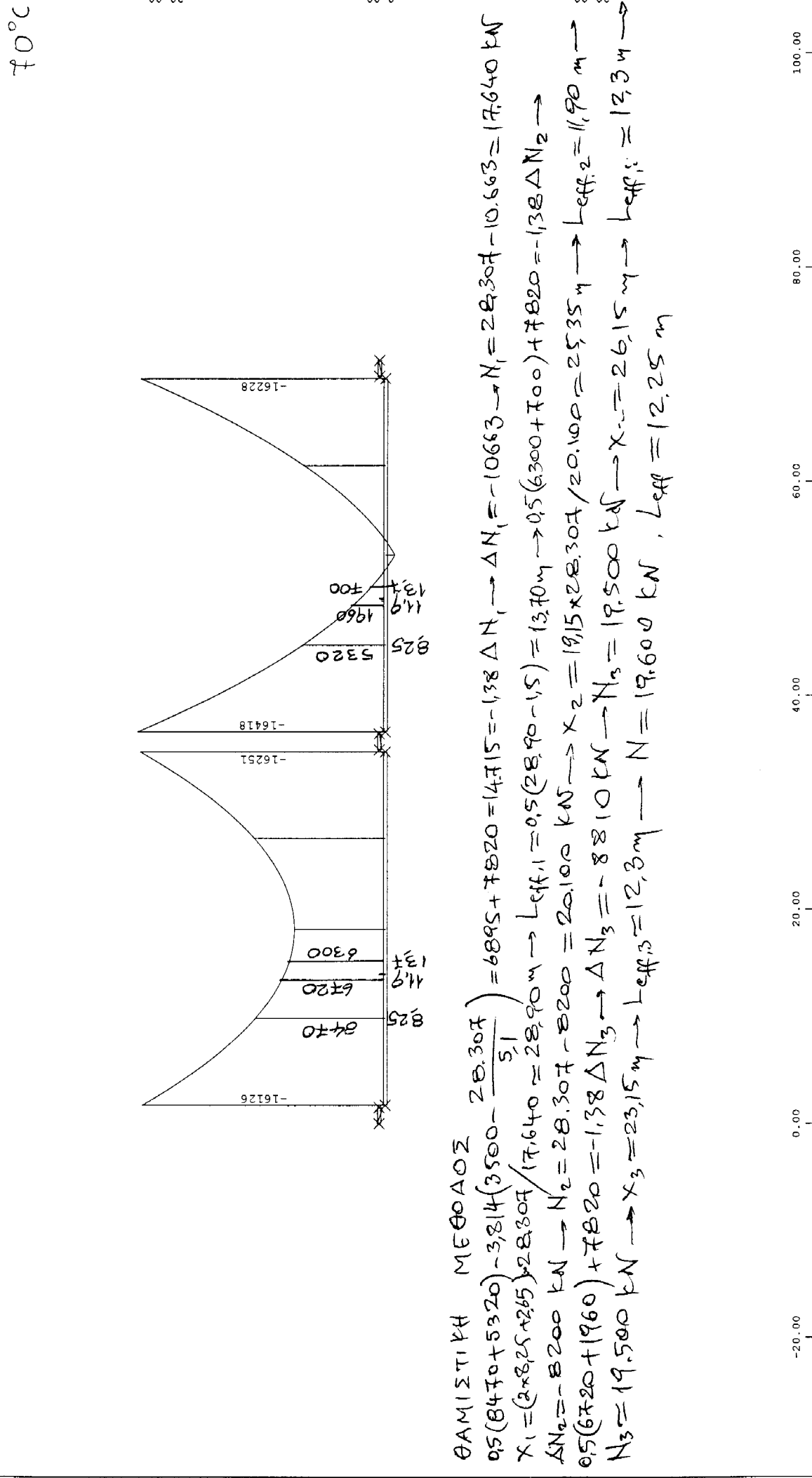
M 1 : 500



M 1 : 500

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
-----BEAM SHEAR FORCES QZ LC 2 LOAD CASE 2 1 CM = 1000 kN





ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\Delta M_{12} = 16.00402 \quad \Delta N_1 = 28.307$$

$$= 6895 + 7820 = 14715 \rightarrow \Delta N_1 = -10663 \rightarrow N_1 = 28307 - 10663 = 17640 \text{ kN}$$

$$x_1 = (2 \times 25 + 265) / 17,640 = 28,90 \rightarrow L_{eff,1} = 0,5(28,90 - 1,5) = 13,70m \rightarrow 0,5(6300 + 700) + 7820 = -138 \Delta N_2 \rightarrow$$

$$AN_2 = -8200 \text{ kN} \rightarrow N_2 = 28.307 - 8200 = 20.100 \text{ kN} \rightarrow X_2 = 1915 \times 28.307 / 20.100 = 25.35 \text{ m} \rightarrow L_{\text{eff}2} = 11.90 \text{ m}$$

$$N_3 = 19,500 \text{ kN} \rightarrow X_3 = 2615 \text{ mm} \rightarrow \text{len.} = 133 \text{ m}$$

$173 = 17.300 \text{ kN} \rightarrow x_3 = 23,15 \text{ m} \rightarrow L_{\text{eff},3} = 12,3 \text{ m} \rightarrow N = 19.600 \text{ kN}, L_{\text{eff}} = 12,25 \text{ m}$

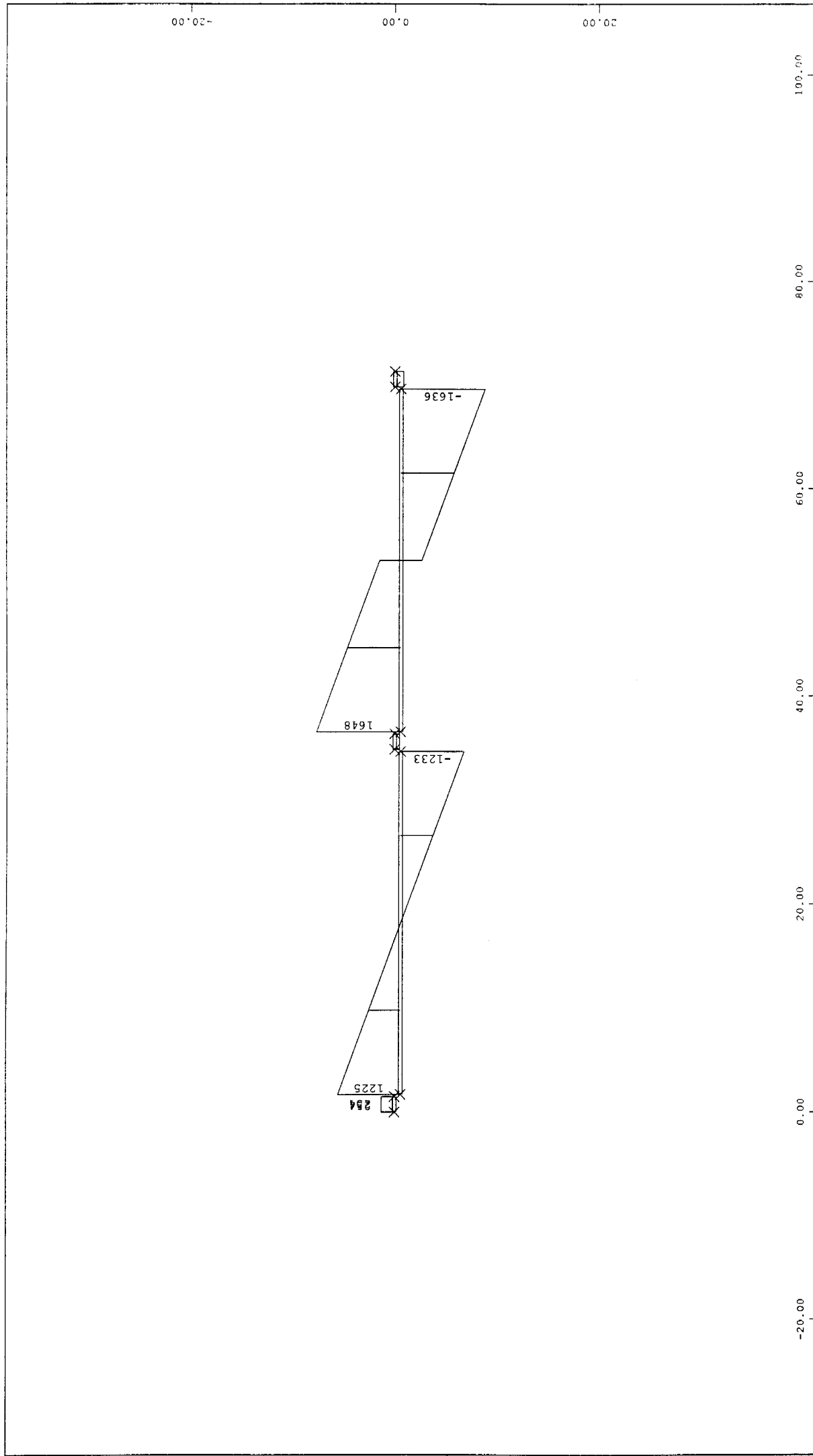
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

SECTION OF STUDENT/ ELEMENT GROUP 0

BEAM MOMENTS MY	LC 2	LOAD CASE 2	1 CM = 3500 kNm
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M 1 : 500

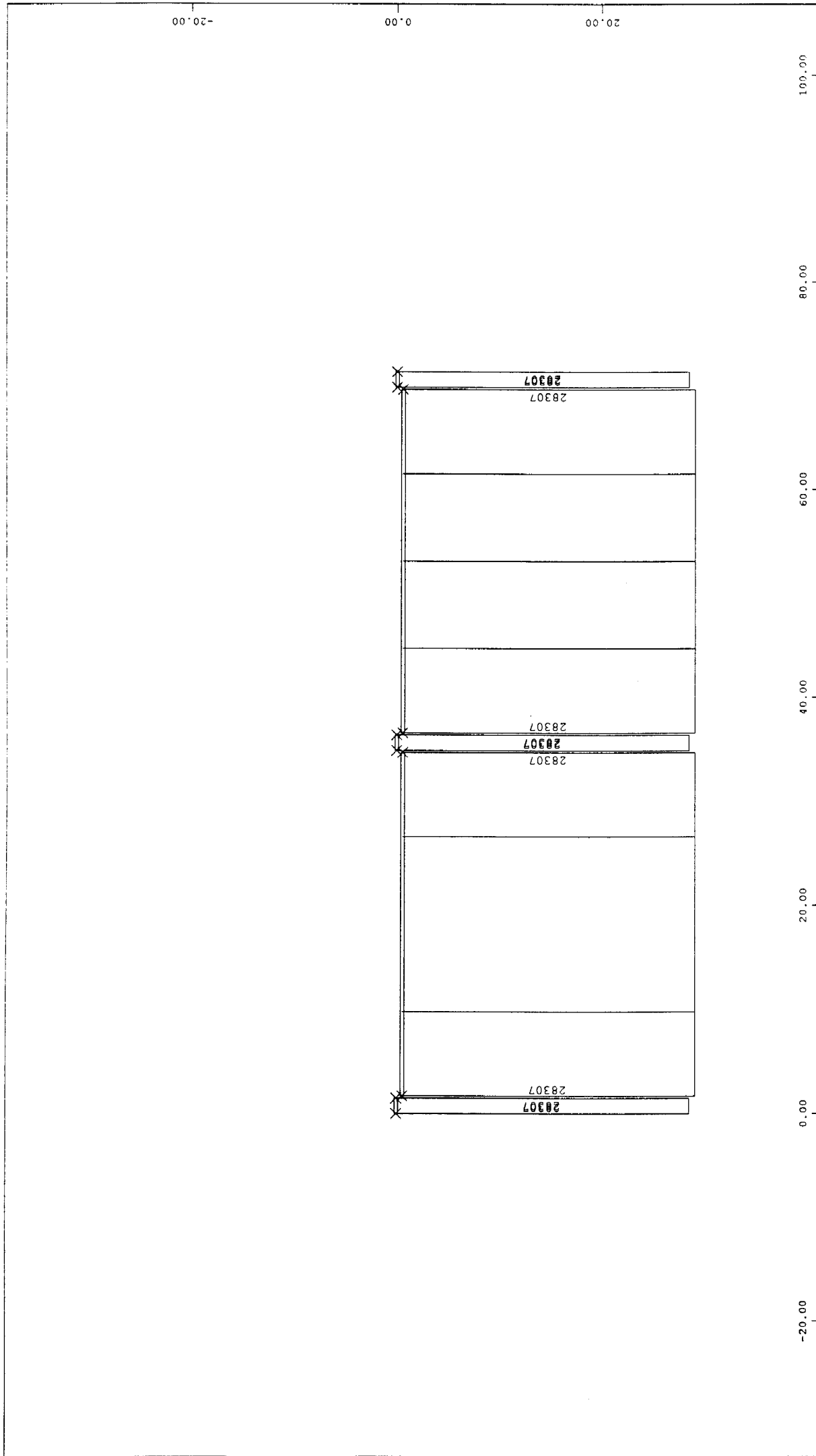


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

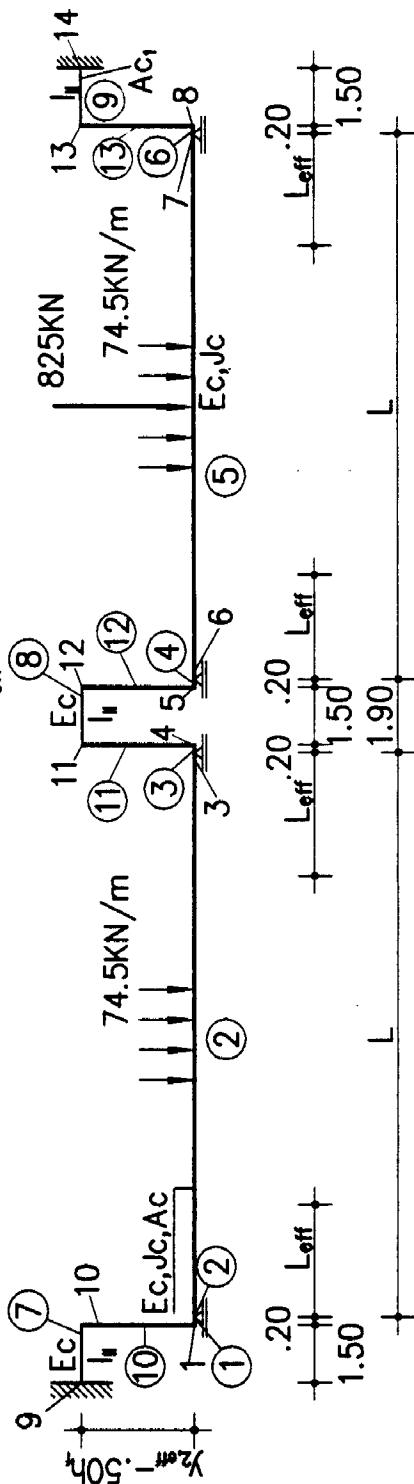
—— BEAM SHEAR FORCES QZ LC 2 LOAD CASE 2 1 CM = 1000 kN

M 1 : 500



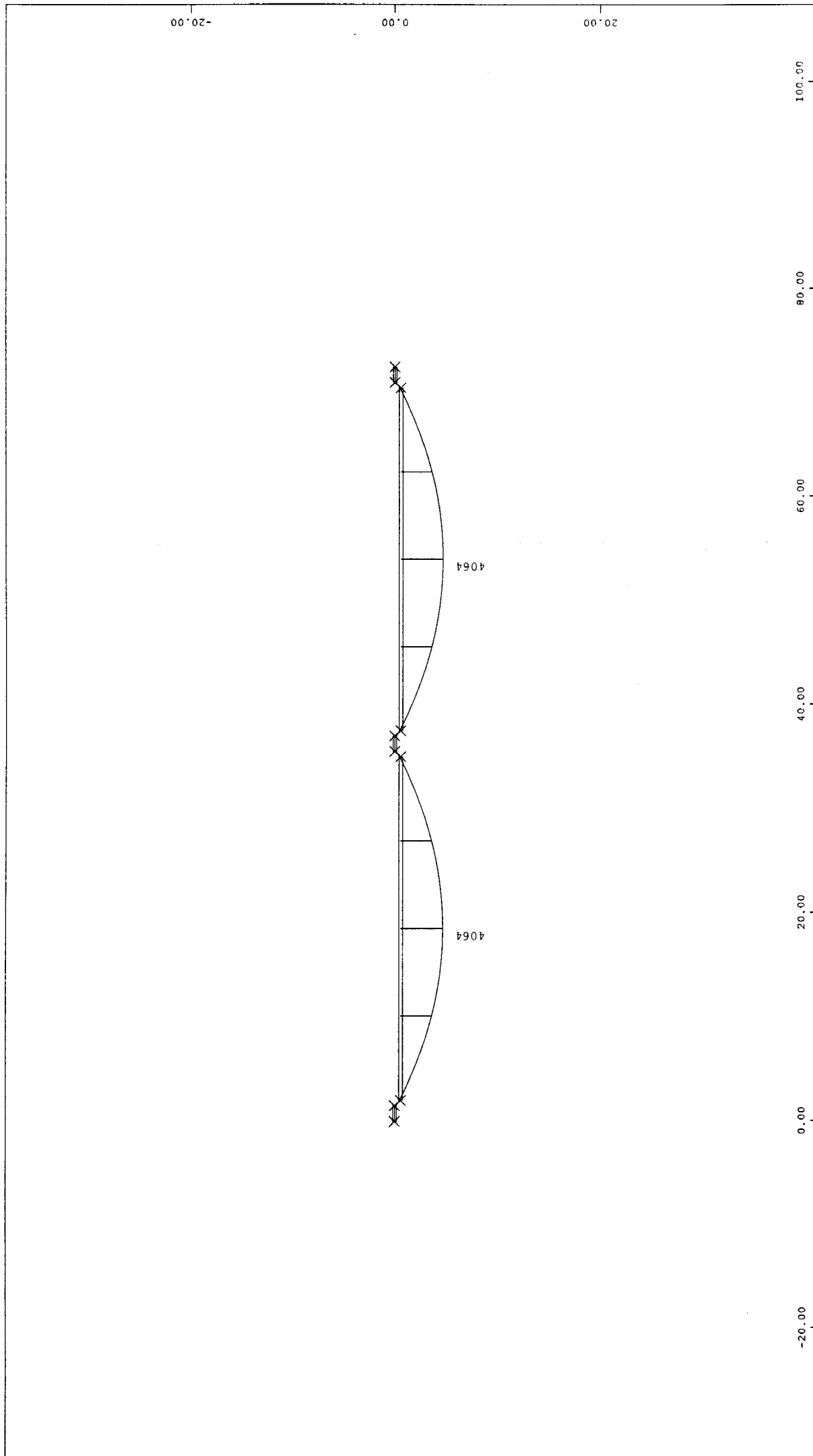
$$A_{c1} = \frac{1.50}{1.50 + L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$

$$A_{c2} = \frac{1.50}{1.50 + 2L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$



ΠΙΝΑΚΑΣ ΔΕΔΟΜΕΝΩΝ

$L = 33.0\text{m}$	$E_c = 32\text{ GPa}$
$b = 12.0\text{m}$	$\alpha = 6.25$
$A_{c,eff} = 5.100\text{m}^2$	$g_1 = 30.7\text{KN/m}$
$J_{c,eff} = 2.784\text{m}$	$q = \varnothing\text{ KN/m}$
$h_b = 2.15\text{m}$	$g_1 + q = 30.7\text{KN/m}$
$h_{it} = 0.275\text{m}$	$Q = \varnothing\text{ KN}$
$h_{t,eff} = 0.20\text{m}$	$A_{st} = 3\text{FF}(3\varnothing 10/75)$
$h_{(np.)} = 0.075\text{m}$	$\rho = 0.016$
$y_{2,eff} = 0.73\text{m}$	$A_{sb} =$
	$T = 50^\circ\text{C}$
	$L_{eff} = L/3 \approx 11\text{m}$
	$I_{II} = 3.544 \alpha \rho b h_{t,eff}^3 / 12 = 0.1772 \rho \sim \varnothing$



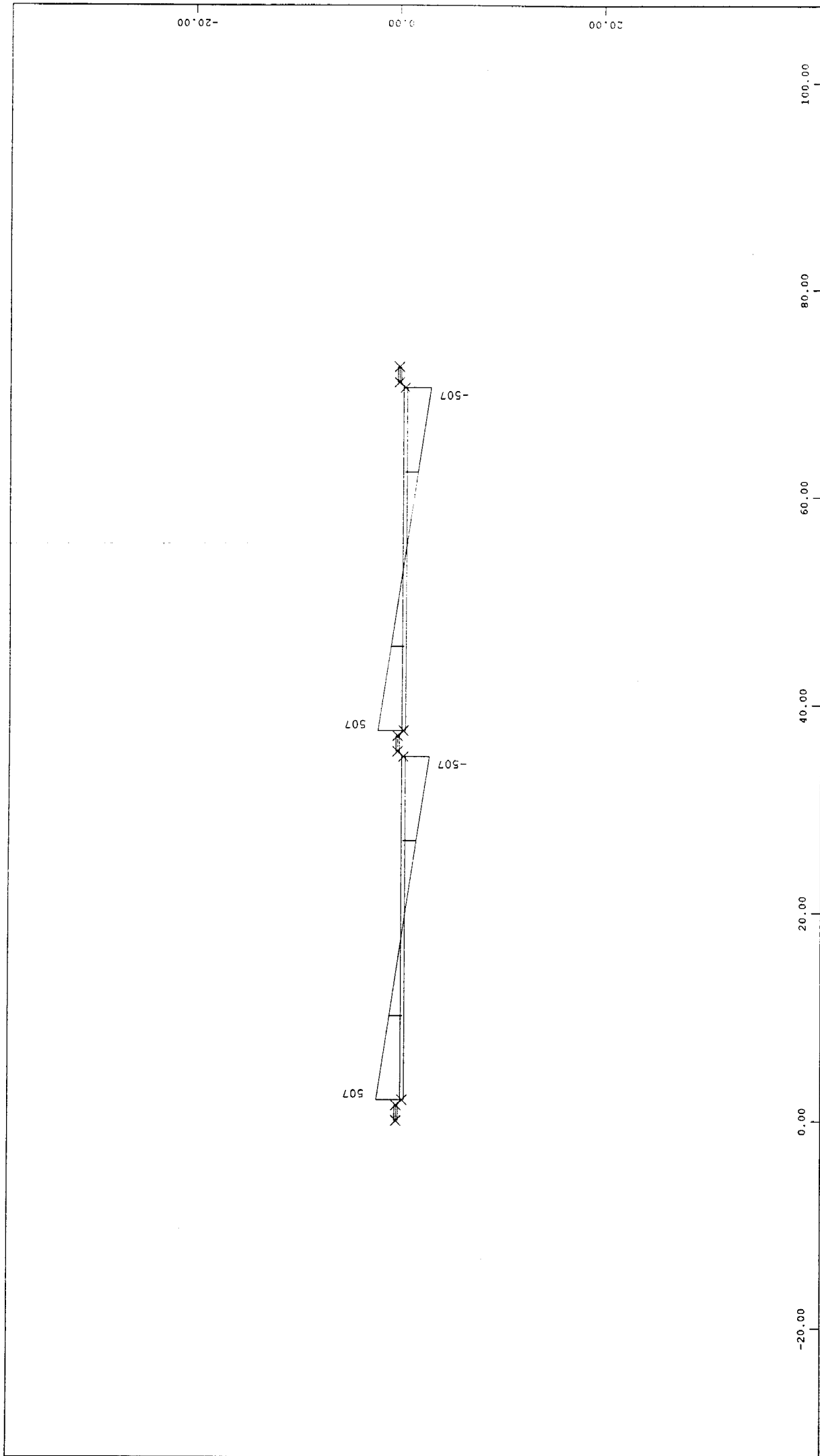
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM MOMENTS MY LC 1 LOAD CASE 1 1 CM = 5000 kNm

x
y
z

M 1 : 500

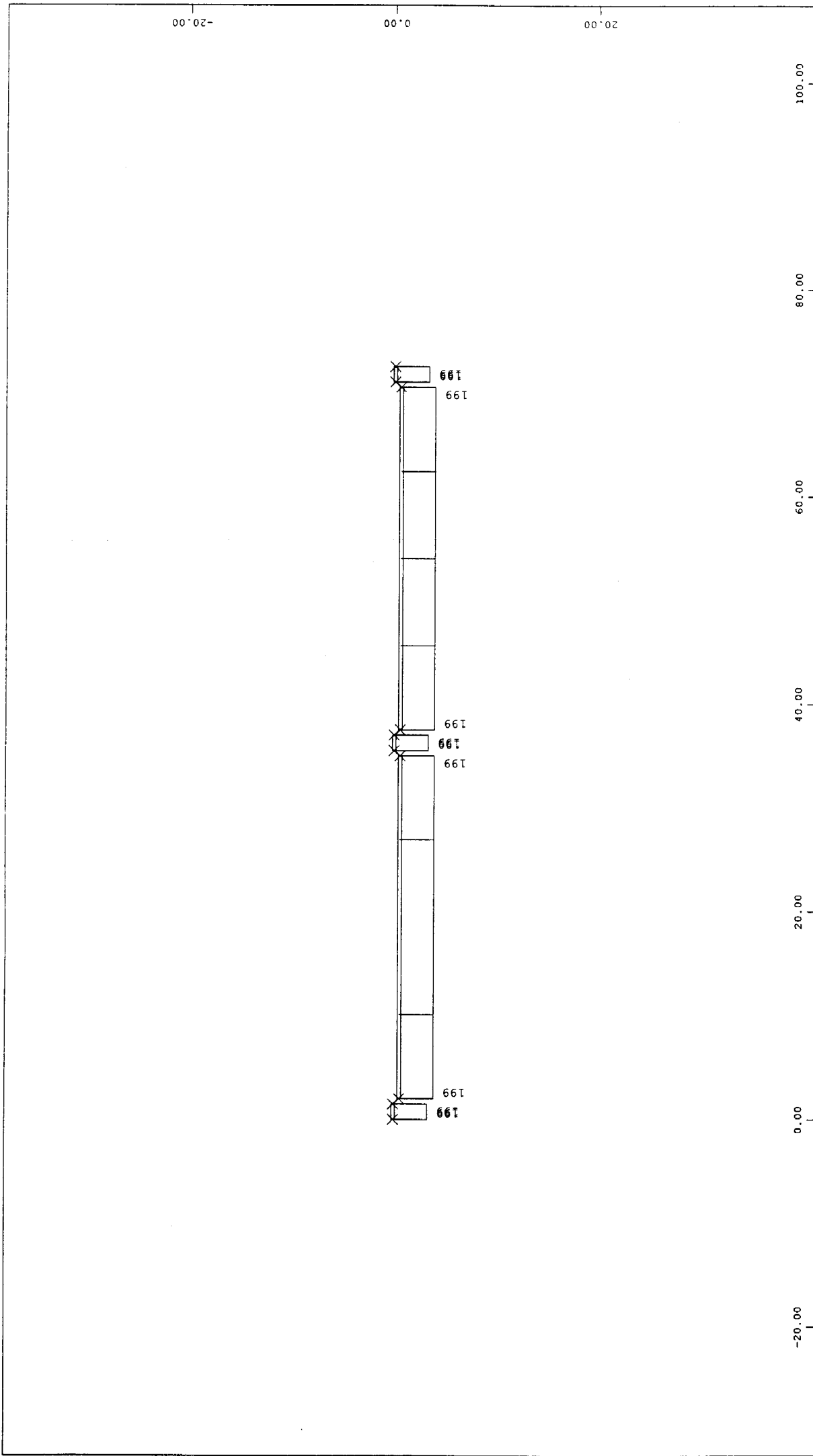


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

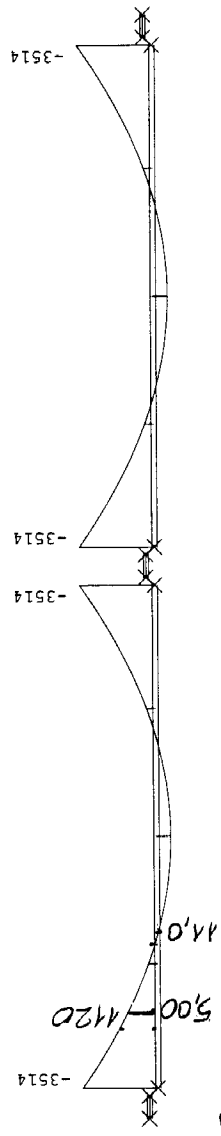
SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM SHEAR FORCES QZ LC 1 LOAD CASE 1 1 CM = 1000 kN

M 1 : 500



M 1 : 500

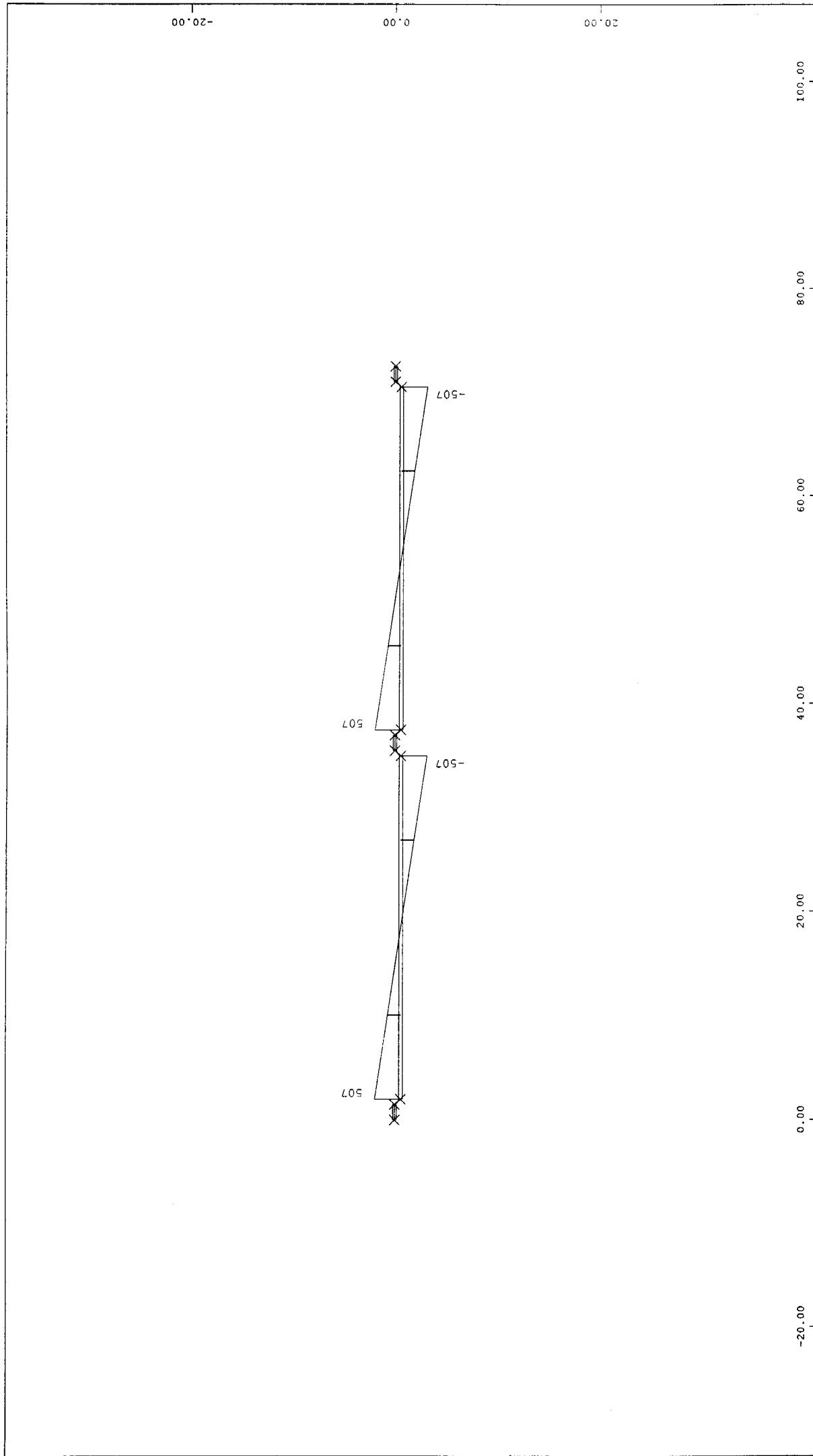


ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\begin{aligned}
 \text{or } \Delta M(x=L_{\text{eff}}) - M_{\text{cr}} &= -\left(\frac{1}{2} V_{2,\text{eff}} - 0,5 h_{f,\text{eff}} + \frac{V_{2,\text{eff}}}{A_{c,\text{eff}}}\right) \Delta N \rightarrow 0 - 3,814 \left(3500 - \frac{6059}{5,1}\right) = -1,38 \Delta N_1 \rightarrow \Delta N_1 = 6390 \text{ kN} \\
 N_1 &= 6059 + 6390 = 12449 \text{ kN} \rightarrow x_1 = (2 \times 11,0 + 2,65) \times 6059 / 12449 = 11,45 \text{ m} \rightarrow L_{\text{eff}} = 4,97 \text{ m} \rightarrow 1120 - 8820 = -1,38 \Delta N_2 \rightarrow \\
 \Delta N_2 &= 5580 \text{ kN} \rightarrow N_2 = 11640 \text{ kN} \rightarrow x_2 = 24,65 \times 6059 / 11640 = 12,25 \text{ m} \rightarrow L_{\text{eff},2} = 5,35 \text{ m} \rightarrow 1050 - 8820 = -1,38 \Delta N_3 \rightarrow \\
 \Delta N_3 &= 5630 \text{ kN} \rightarrow N_3 = 5630 + 6059 = 11690 \text{ kN} \rightarrow x_3 = 12,20 \text{ m} \rightarrow L_{\text{eff}} = 5,30 \text{ m} \rightarrow N = 11700 \text{ kN}
 \end{aligned}$$

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500

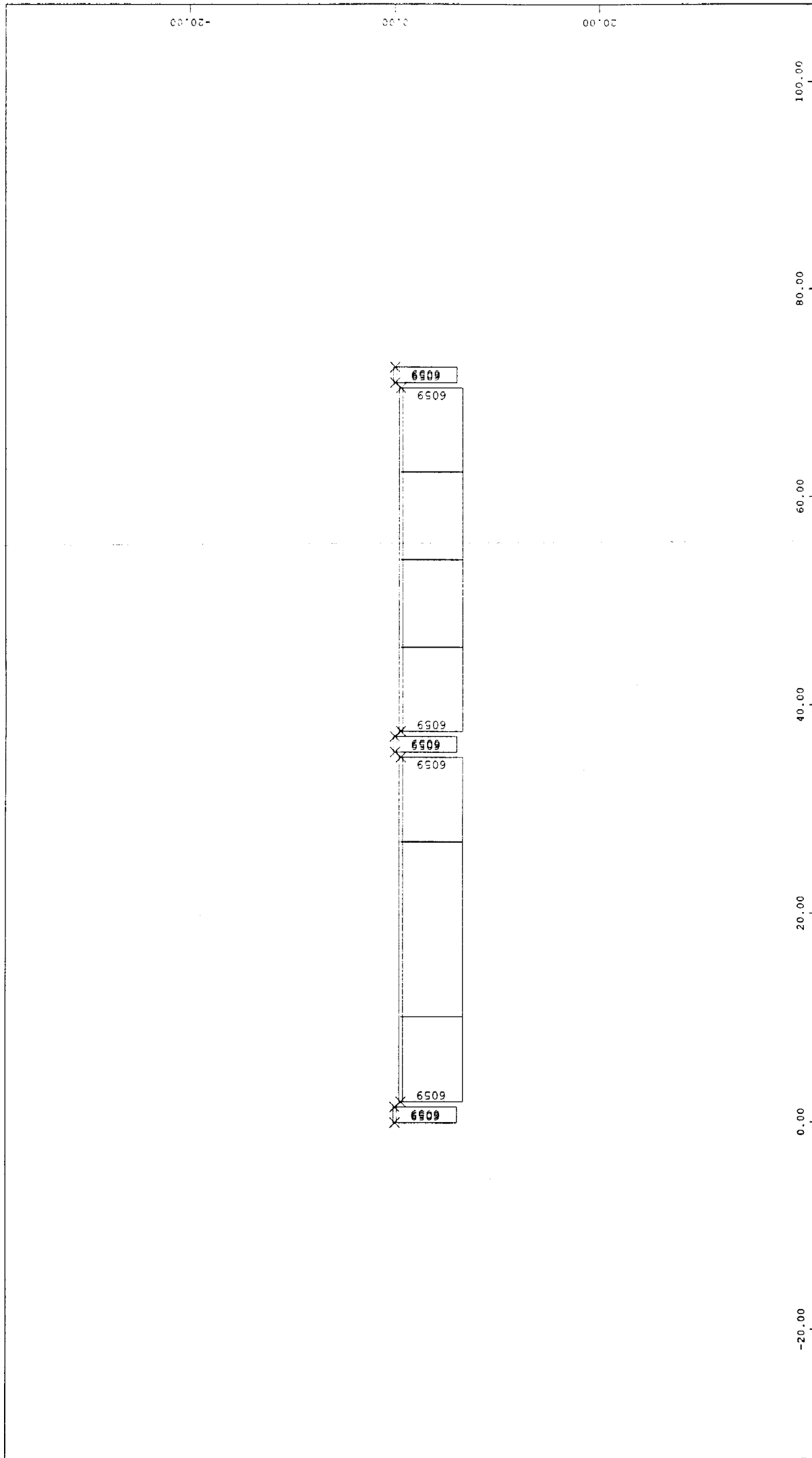


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM SHEAR FORCES QZ LC 2 LOAD CASE 2 1 CM = 1000 kN

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

Y x
Z

M 1 : 500

$$AC_2 = \frac{1.50}{1.50 + 2L_{\text{eff}}} \quad \frac{1.2As}{Es} \frac{Ec}{Ec}$$



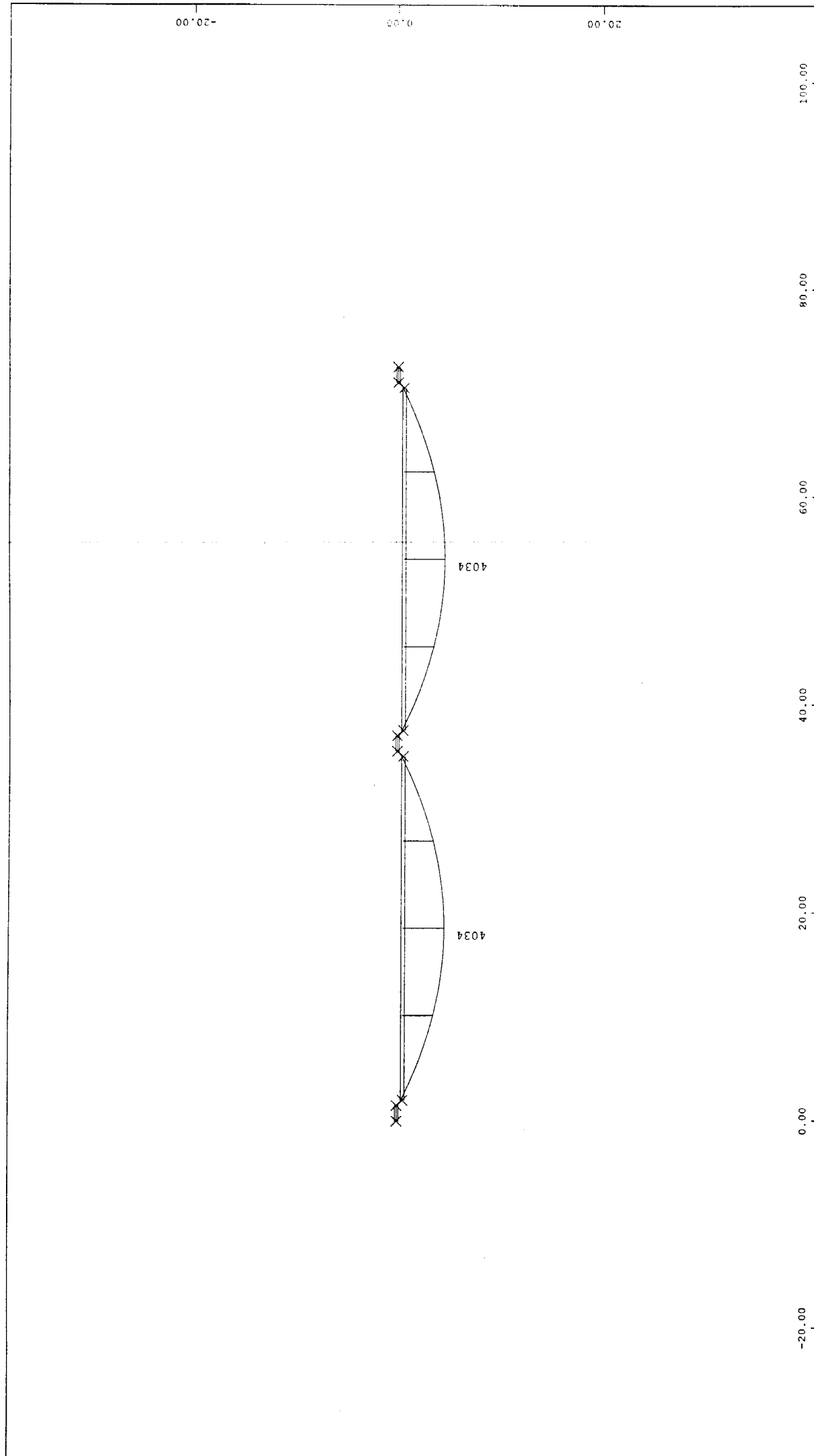
(88)

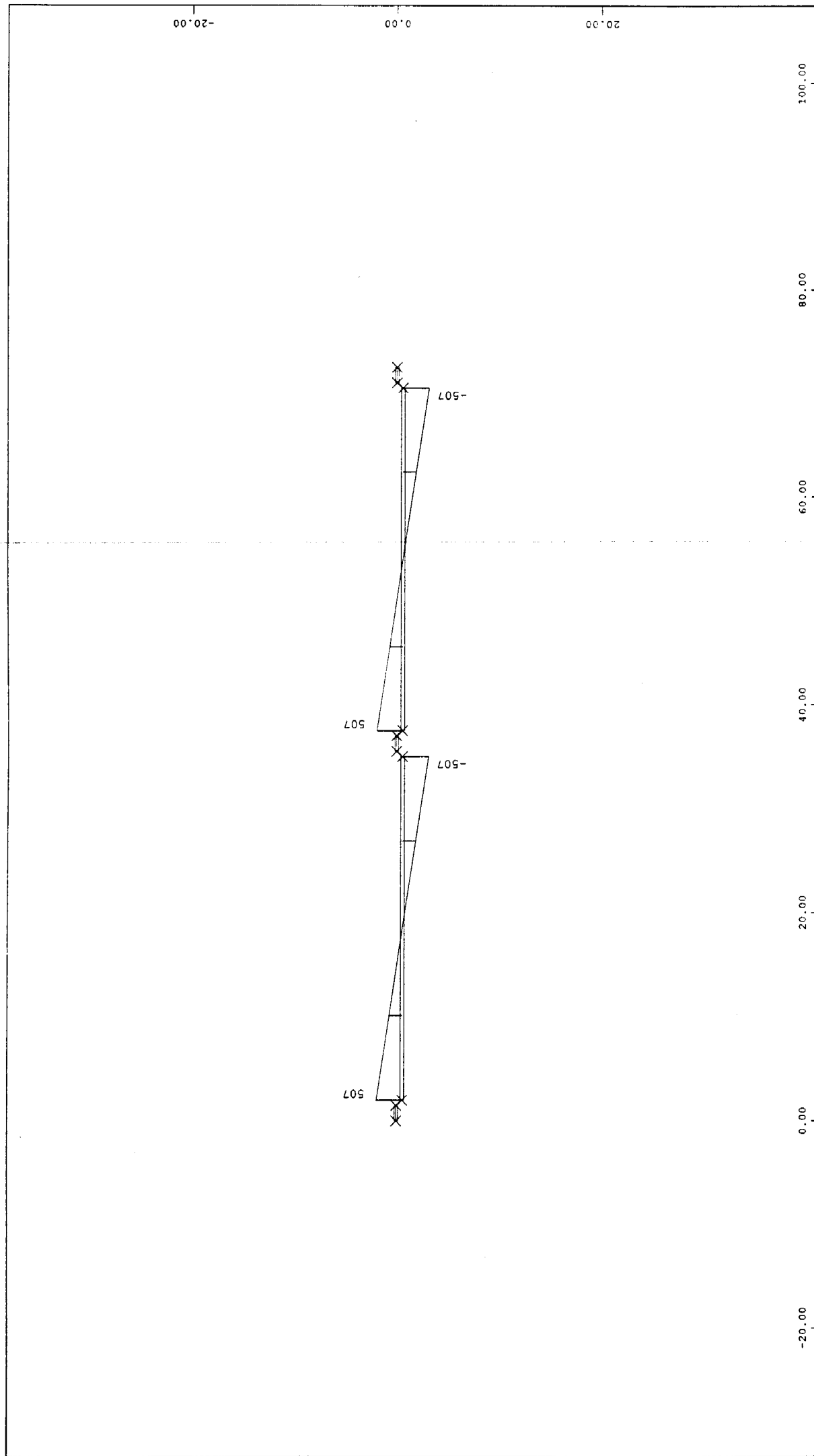
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM MOMENTS MY LC 1 LOAD CASE 1 1 CM = 5000 kNm

Y — x
z





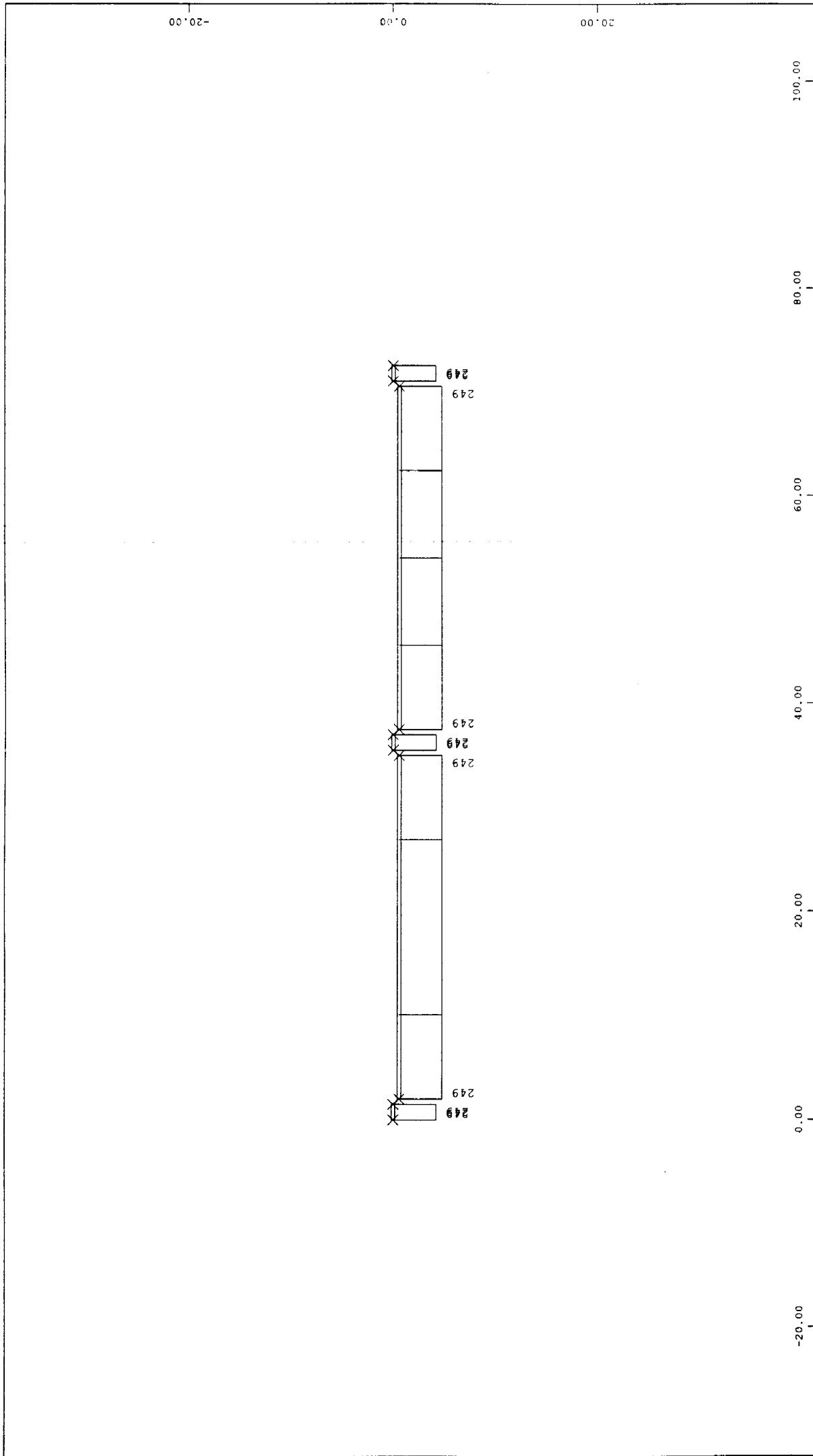
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM SHEAR FORCES QZ LC 1 LOAD CASE 1 1 CM = 1000 kN

x
y
z

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

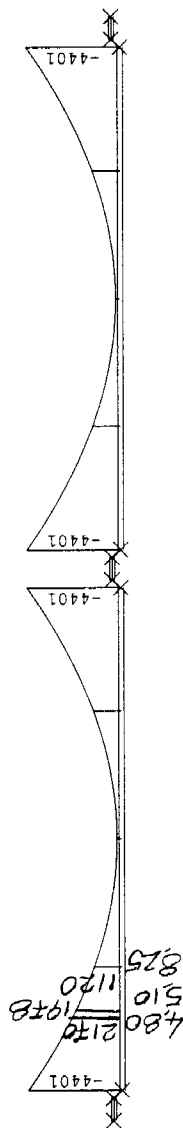
SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM NORMAL FORCES LC 1 LOAD CASE 1 1 CM = 300.0 kN

M 1 : 500

ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\begin{aligned} \text{2η } \Delta M(x=L_{\text{eff}}) - M_{\text{cr}} &= - \left[(x/2 - 0.5 h_{\text{eff}}) + \frac{W_{2,\text{eff}}}{A_{\text{c,eff}}} \right] \Delta N \rightarrow 1120 - 3814 (3500 - \frac{7588}{5.1}) = -138 \Delta N_1 \rightarrow \Delta N_1 = 4750 \text{ kN} \\ N_1 &= 7588 + 4750 = 12338 \text{ kN} \rightarrow x_1 = (2 \times 825 + 265) \times 7588 / 12338 = 1105 \text{ m} \rightarrow L_{\text{eff},1} = (1105 - 265) / 2 = 420 \text{ m} \rightarrow 2180 - 7675 = \\ &= -138 \Delta N_2 \rightarrow \Delta N_2 = 3990 \text{ kN} \rightarrow N_2 = 11580 \text{ kN} \rightarrow x_2 = 1915 \times 7588 / 11580 = 1165 \text{ m} \rightarrow L_{\text{eff},2} = 510 \text{ m} \rightarrow 1978 - \\ &- 7675 = -138 \Delta N_3 \rightarrow \Delta N_3 = 4130 \text{ kN} \rightarrow N_3 = 11720 \text{ kN} \rightarrow x_3 = 1165 \text{ m} \rightarrow L_{\text{eff},3} = 510 \text{ m} \rightarrow N = 11700 \text{ kN} \end{aligned}$$

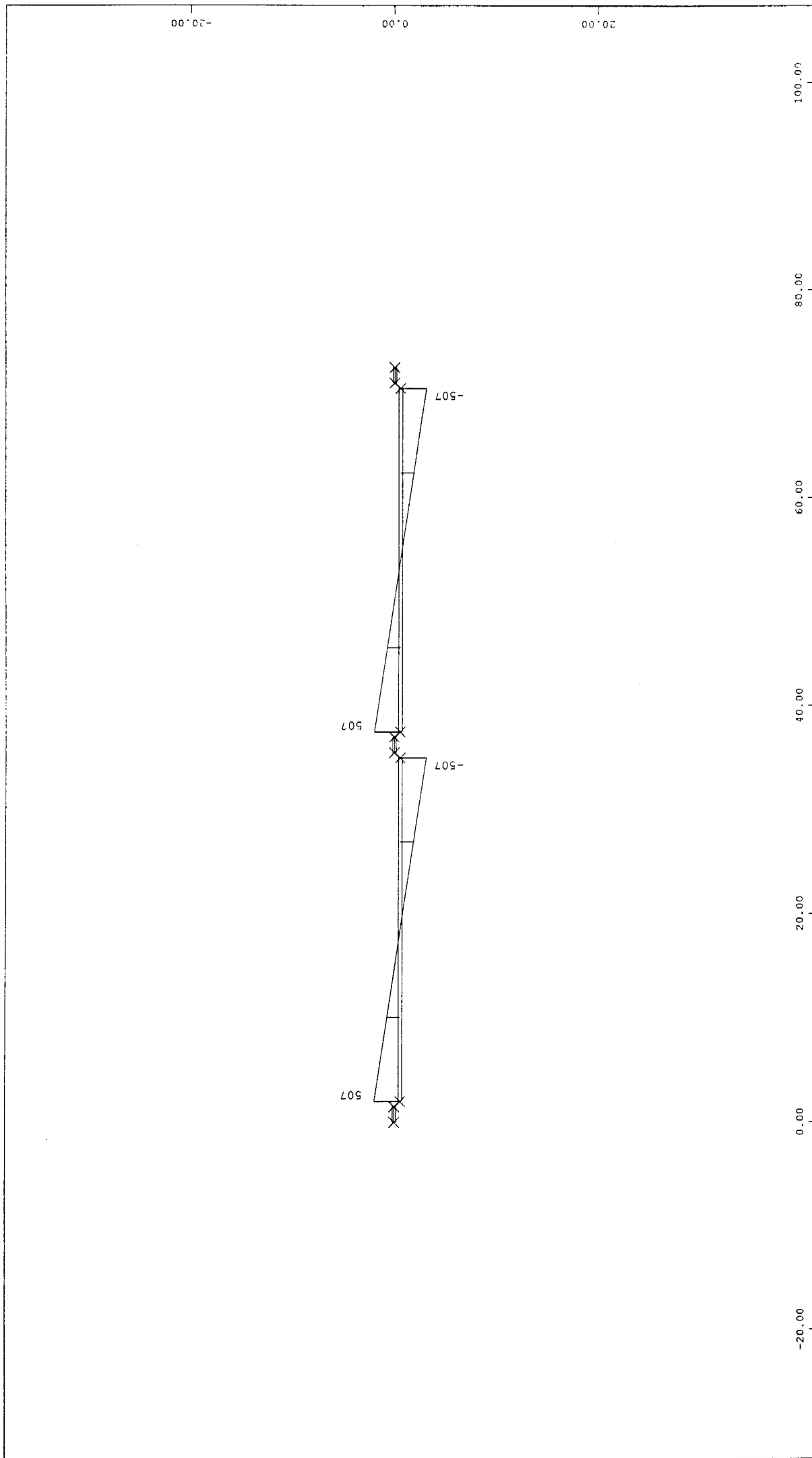


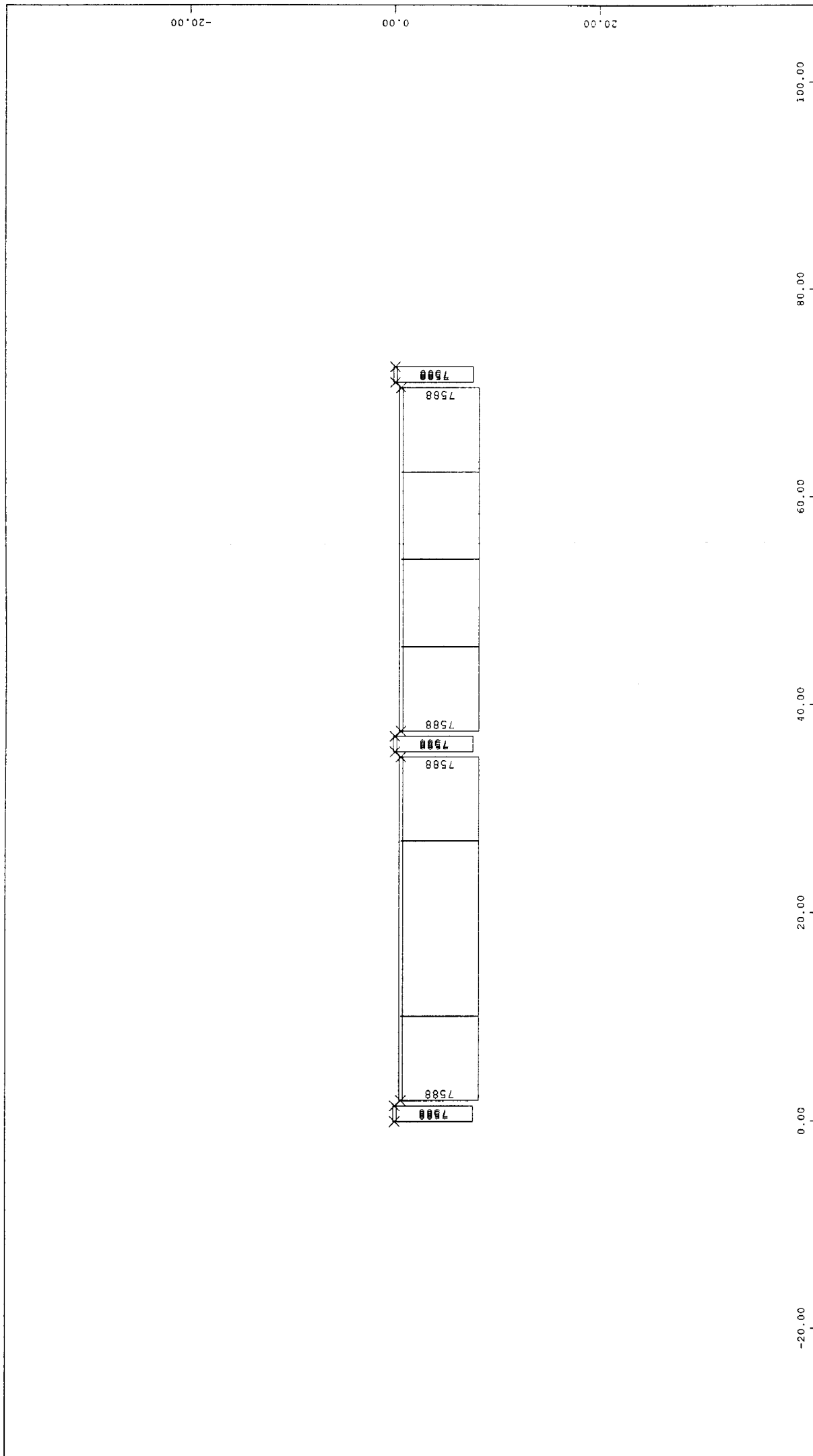
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

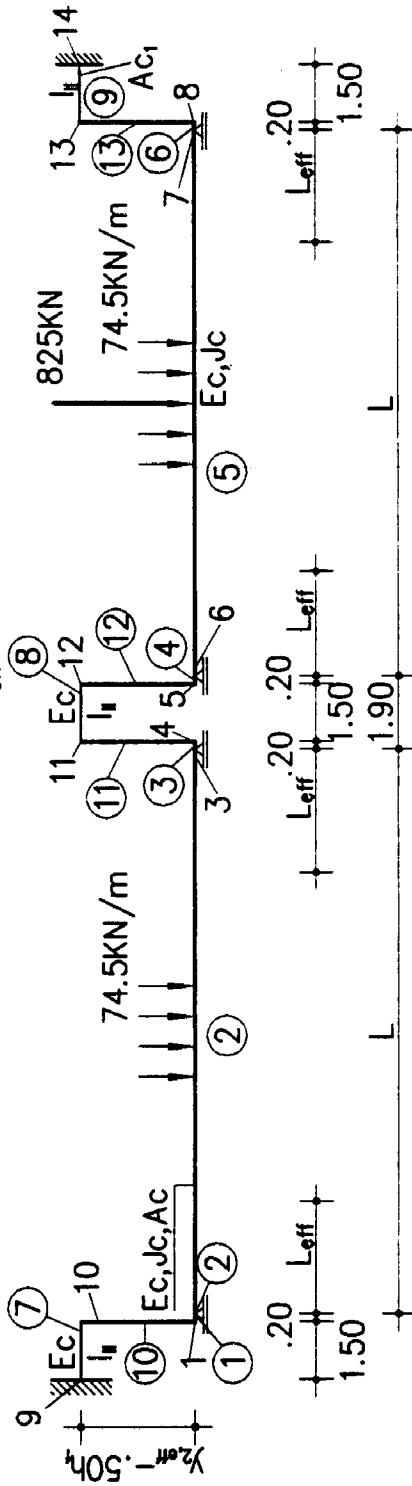
M 1 : 500





$$A_{C1} = \frac{1.50}{1.50 + L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$

$$A_{C2} = \frac{1.50}{1.50 + 2L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$

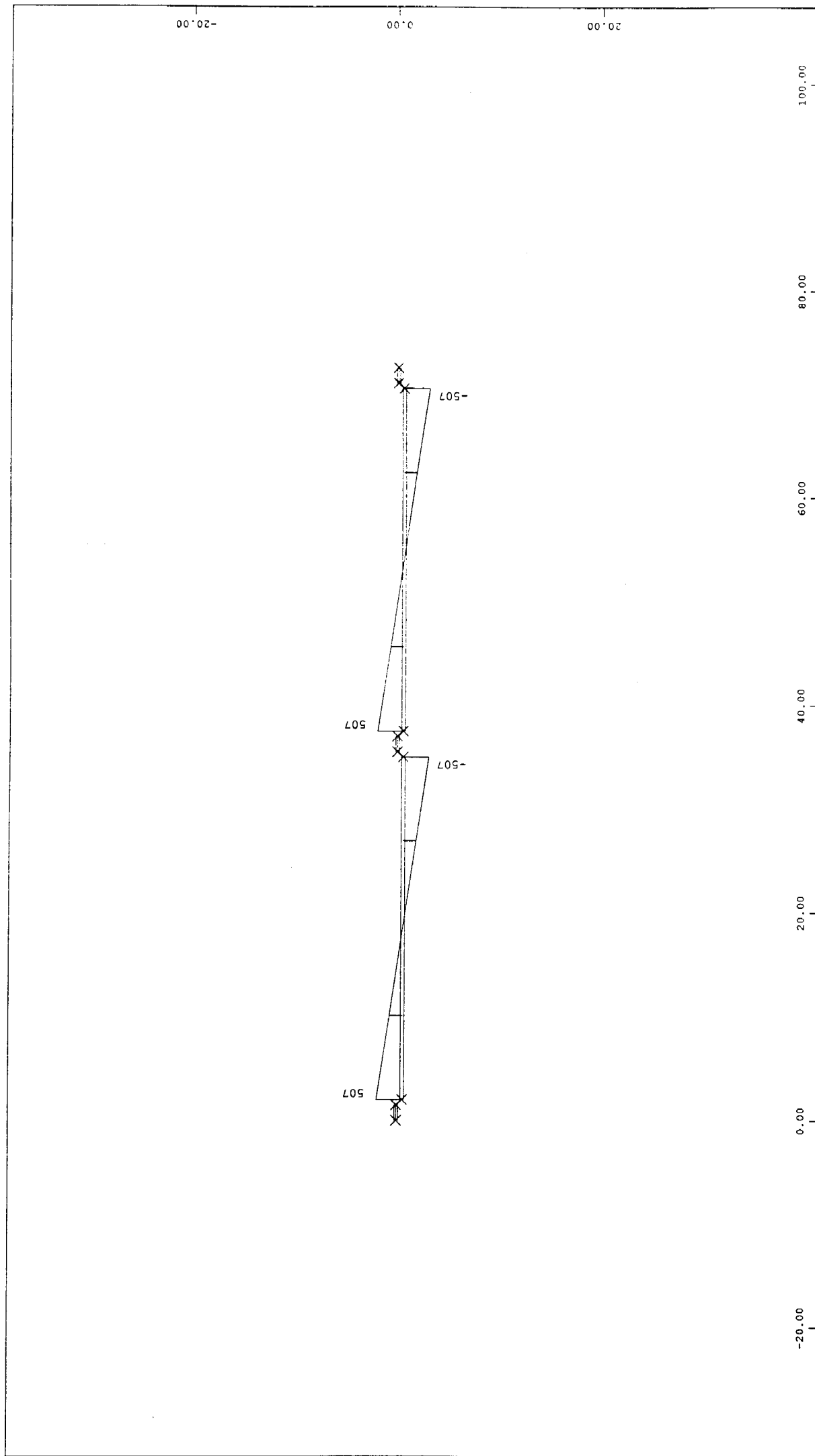


ΠΙΝΑΚΑΣ ΔΕΔΟΜΕΝΩΝ

$L = 33.0\text{m}$	$E_c = 32\text{ GPa}$
$b = 12.0\text{m}$	$\alpha = 6.25$
$A_{c,eff} = 5.100\text{m}^2$	$g_1 = 30.7\text{KN/m}$
$J_{c,eff} = 2.784\text{m}$	$q = \varnothing\text{ KN/m}$
$h_b = 2.15\text{m}$	$g_1 + q = 30.7\text{KN/m}$
$h_{ft} = 0.275\text{m}$	$Q = \varnothing\text{ KN}$
$h_{r,eff} = 0.20\text{m}$	$A_{st} = 377\text{cm}^2 (3\phi 10/75)$
$h_{(np.)} = 0.075\text{m}$	$\rho = 0.016$
$\chi_{2,eff} = 0.73\text{m}$	$A_{sb} = \varnothing$
	$T = -50^\circ\text{C}$
	$L_{eff} = L/5 = 6.6\text{m}$
$I_{II} = 3.544 \alpha \rho b h_{r,eff}^3 / 12 = 0.1772 \rho = \varnothing$	



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
-----BEAM MOMENTS MY LC 1 LOAD CASE 1 1 CM - 5000 kNm



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

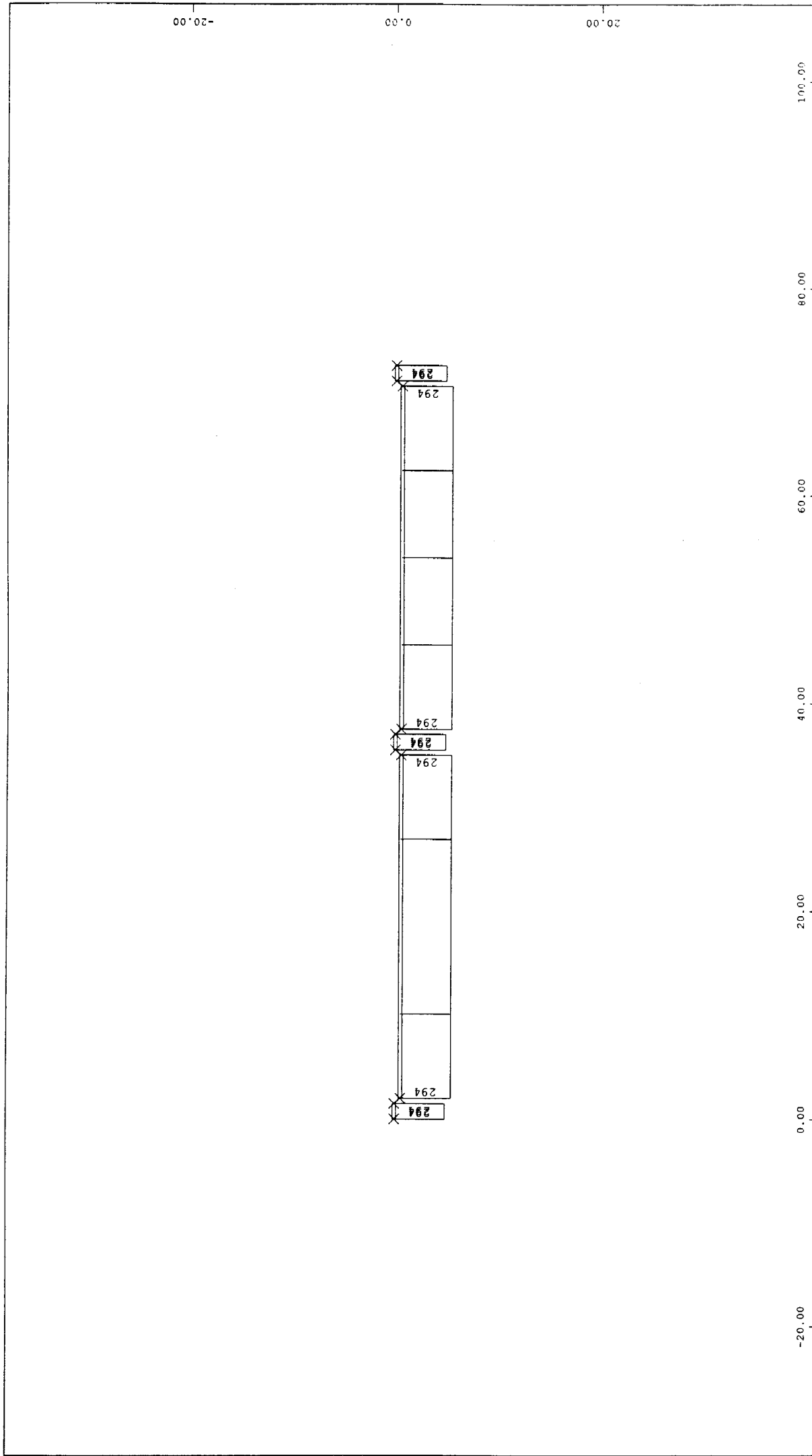
SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM SHEAR FORCES Q2 LC 1 LOAD CASE 1 1 CM = 1000 kN

M 1 : 500

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 BEAM NORMAL FORCES LC 1 LOAD CASE 1 1 CM = 300.0 kN

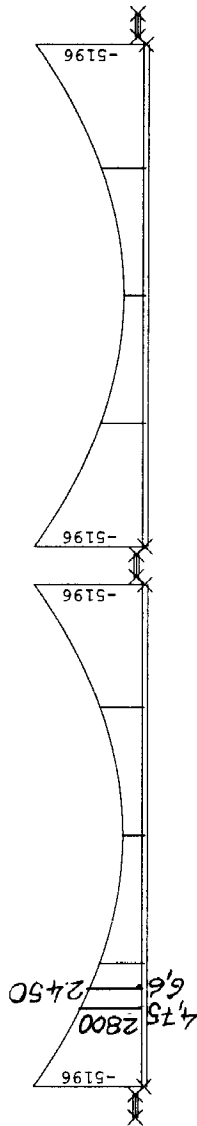
x
z



ΕΛΕΓΧΟΣ ΠΛΑΚΑΣ ΕΛΚΥΣΤΗΡΑ

$$N \approx 11650 \approx 11700 \text{ kN}, A_c = 377 \text{ cm}^2$$

$$\sigma_s^d = 11700 / 377 = 31 \text{ kN/cm}^2 = 310 \text{ MPa} < 315 \text{ MPa} \triangleq w_k = 0.1 \text{ mm} (\text{Πιν. 15.1 ΚΩΣ})$$



ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\begin{aligned} \text{στη } \Delta M(x=L_{\text{eff}}) - M_{\text{cr}} &= - \left(\gamma_{2,\text{eff}} h_{2,\text{eff}} + \frac{w_{2,\text{eff}}}{A_{c,\text{eff}}} \right) \Delta N \rightarrow 2450 - 3814 \left(3500 - \frac{8959}{5.1} \right) = -138 \Delta N_1 \rightarrow \Delta N_1 = 3043 \text{ kN} \\ N_1 &= 8959 + 3043 = 12000 \text{ kN} \rightarrow x_1 = (2 \times 6.6 + 2.65) \times 8959 / 12000 = 11.0 \text{ m} \rightarrow L_{\text{eff},1} \approx 0.5(11.0 - 2.65) = 4.175 \text{ m} \rightarrow 2800 - 6650 = \\ &= -138 \Delta N_2 \rightarrow \Delta N_2 = 2790 \text{ kN} \rightarrow N_2 \approx 11750 \text{ kN} \rightarrow x_2 = 1.585 \times 8959 / 11750 = 11.20 \text{ m} \rightarrow L_{\text{eff},2} \approx 4.85 \text{ m} \\ 2790 - 6650 &= -138 \Delta N_3 \rightarrow \Delta N_3 = 2663 \text{ kN}, N_3 = 11620 \text{ kN} \rightarrow x_3 = 1.35 \text{ m} \rightarrow L_{\text{eff},3} = 4.90 \text{ m} \rightarrow N \approx 11650 \text{ kN} \end{aligned}$$

ΠΑΡΑΤΗΡΗΣΗ

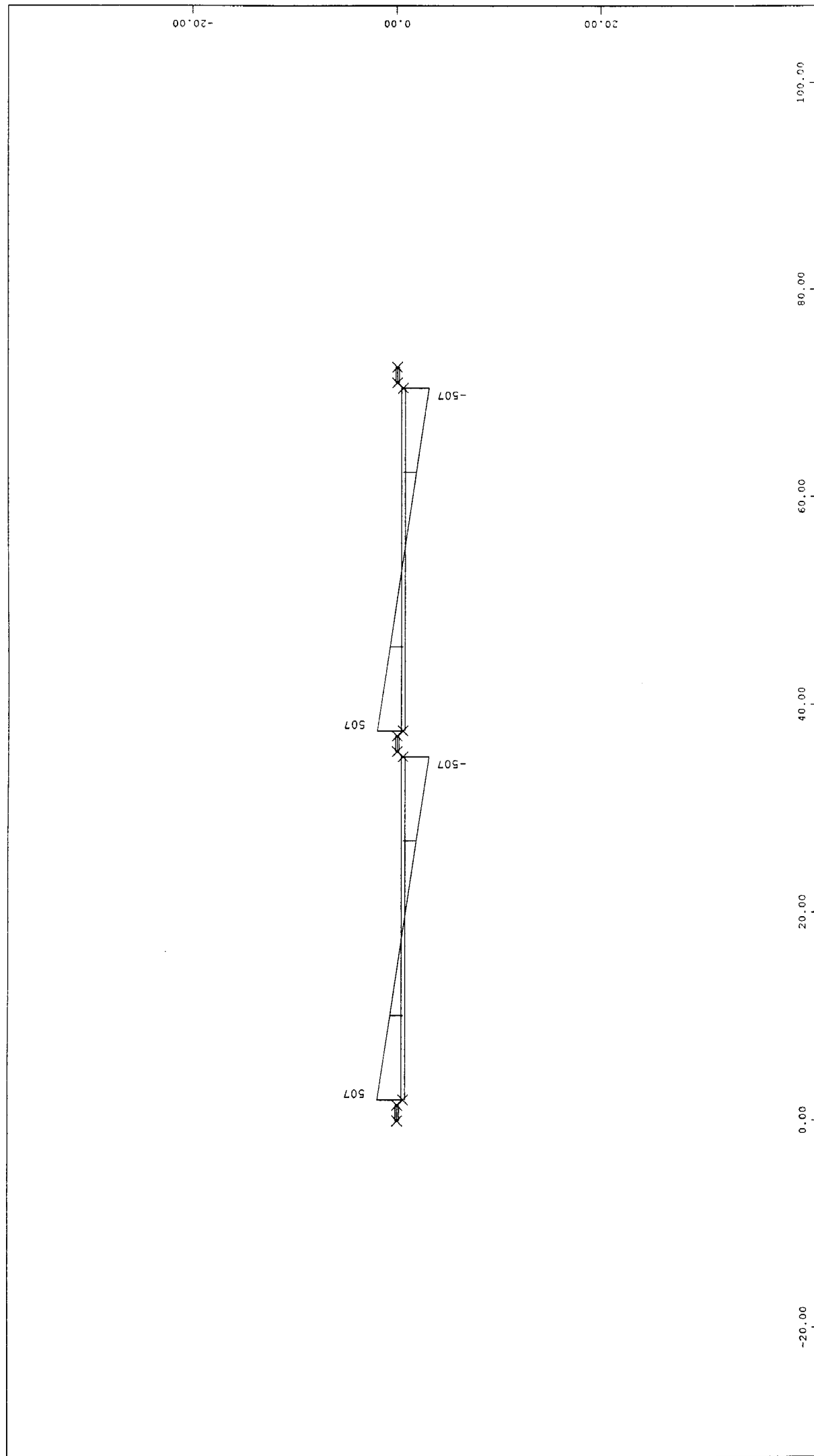
Για τα N & L_{eff} προκύπτουν τα ίδια αποτελέσματα, ως αναμένονταν, με τις δύο αλλαγές στην τιμή της ονομαστικής διατομής A_c και της επιμέρους L_{eff} .

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500

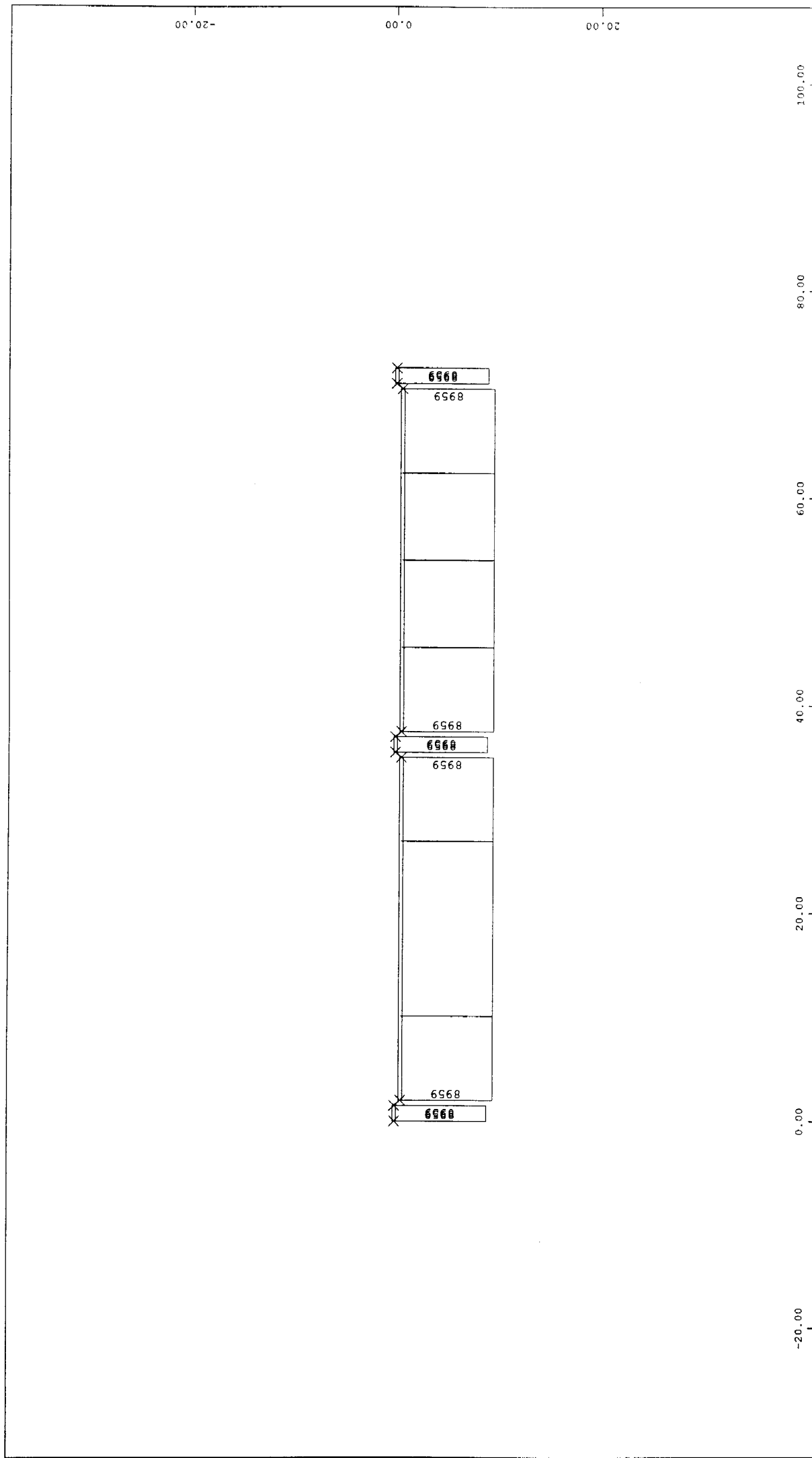


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

-----BEAM SHEAR FORCES Q2 LC 2 LOAD CASE 2 1 CM = 1000 kN

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

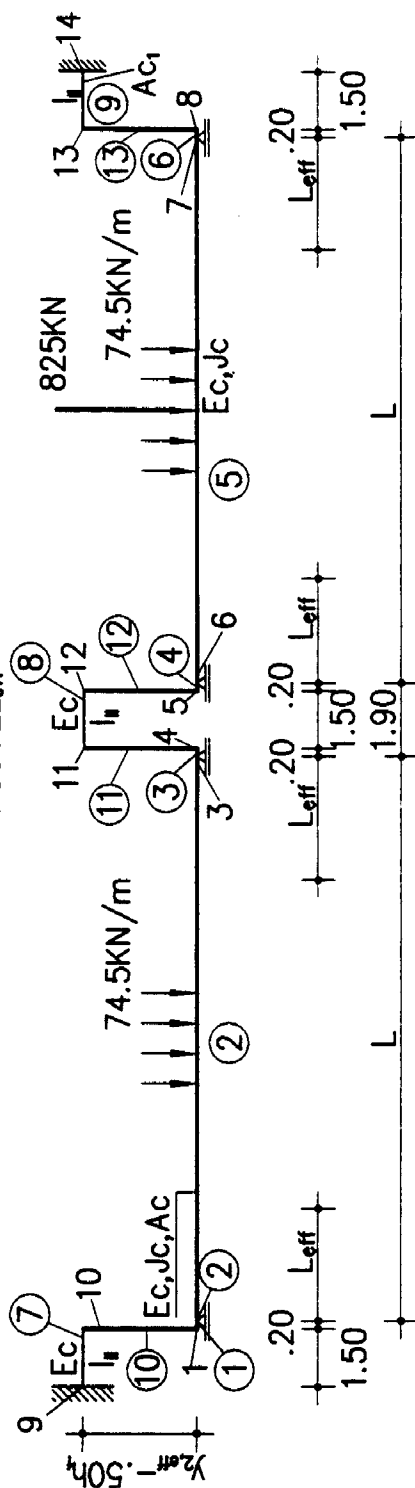
SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

M 1 : 500

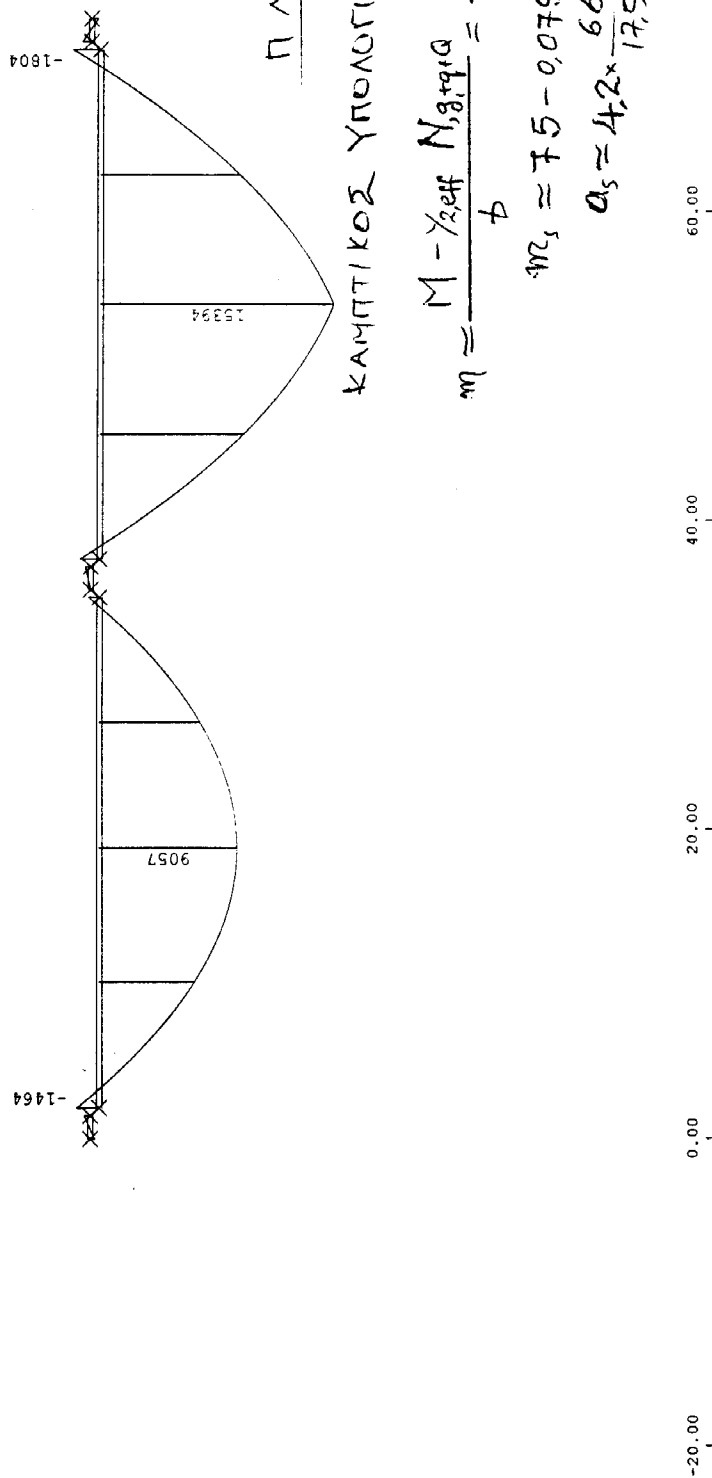
$$A_{C1} = \frac{1.50}{1.50 + L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$

$$A_{C2} = \frac{1.50}{1.50 + 2L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$



ΠΙΝΑΚΑΣ ΔΕΔΟΜΕΝΩΝ

$L = 33.0m$	$E_c = 32 \text{ GPa}$
$b = 12.0m$	$\alpha = 6.25$
$A_{c,eff} = 5.100m^2$	$g_1 = 30.7kN/m$
$J_{c,eff} = 2.784m$	$q = 43.8kN/m$
$h_b = 2.15m$	$g_1 + q = 74.5kN/m$
$h_{ff} = 0.275m$	$Q = 825kN$
$h_{t,eff} = 0.20m$	$A_{st} = 73 \frac{cm^2}{m} (\phi 14/7s)$
$h_{(np.)} = 0.075m$	$\rho = 3.1\%$
$\gamma_{2,eff} = 0.73m$	$A_{st} = 20.5 \frac{cm^2}{m} (\phi 14/7s)$
	$T = -50^\circ C$
	$L_{eff} = L/5 \approx 6.6m$
	$I_{II} = 3.544 \alpha \rho b h_{t,eff}^3 / 12 = 0.1772 \rho \approx I_y / 1.5 = 0.0053m^4$



ΚΑΜΠΤΙΚΟΣ ΥΠΟΛΟΓΙΣΜΟΣ ΕΝΑΝΤΙ ΦΟΡΤΙΩΝ
ΒΑΡΥΤΗΤΟΣ

$$m = \frac{M - \frac{1}{2} N_{g+q} \cdot \frac{12,0}{4}}{b} = \frac{1804 - 0,63 \times 1430}{4} = 7,5 \text{ kNm/m}$$

$$m_2 = 7,5 - 0,075 \times \frac{1430}{12,0} = 6,6 \text{ kNm/m}$$

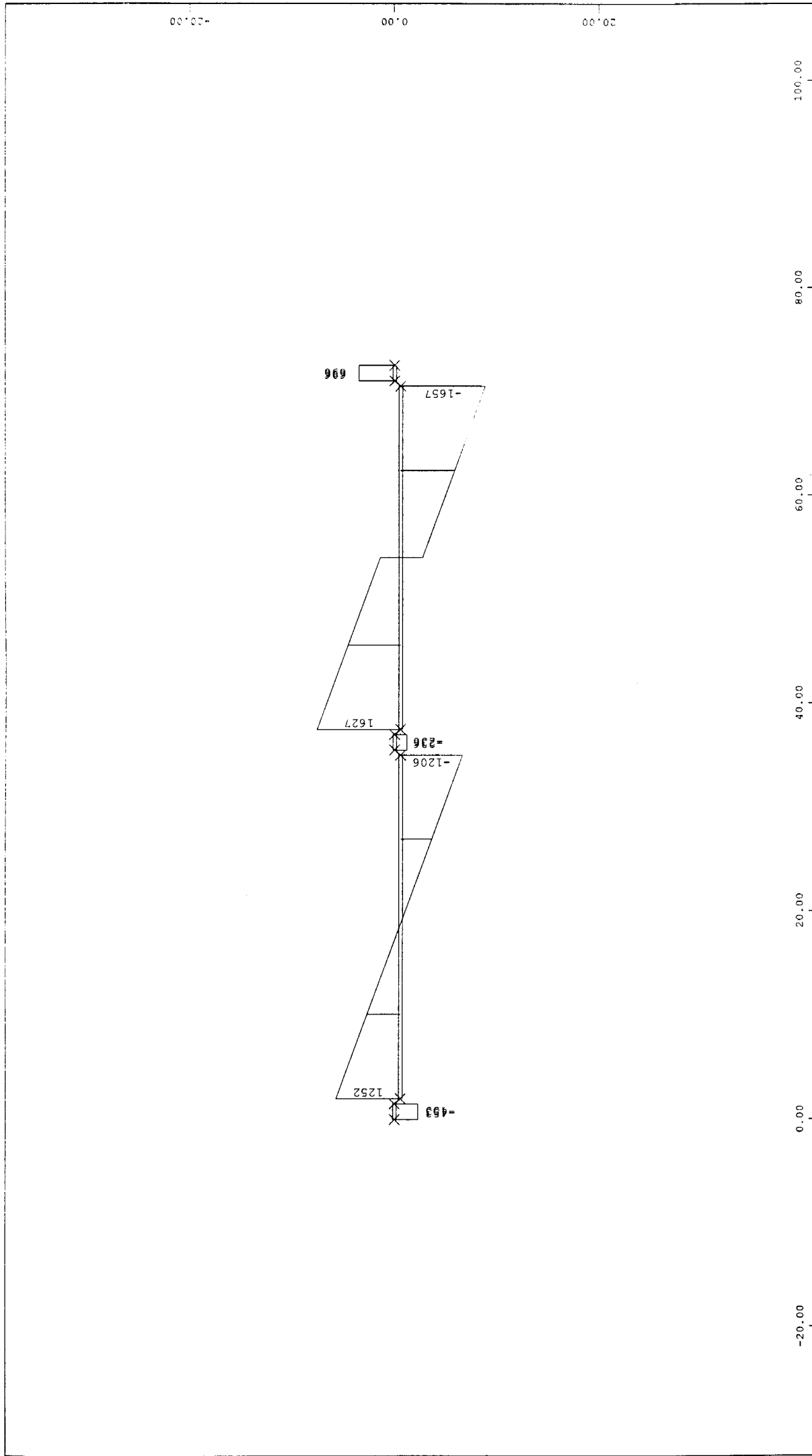
$$a_s = 4,2 \times \frac{6,6}{17,5} + \frac{11,9}{26} = 19 < 2 \times 20,5 = 41 \text{ cm}^2/\text{m}$$

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

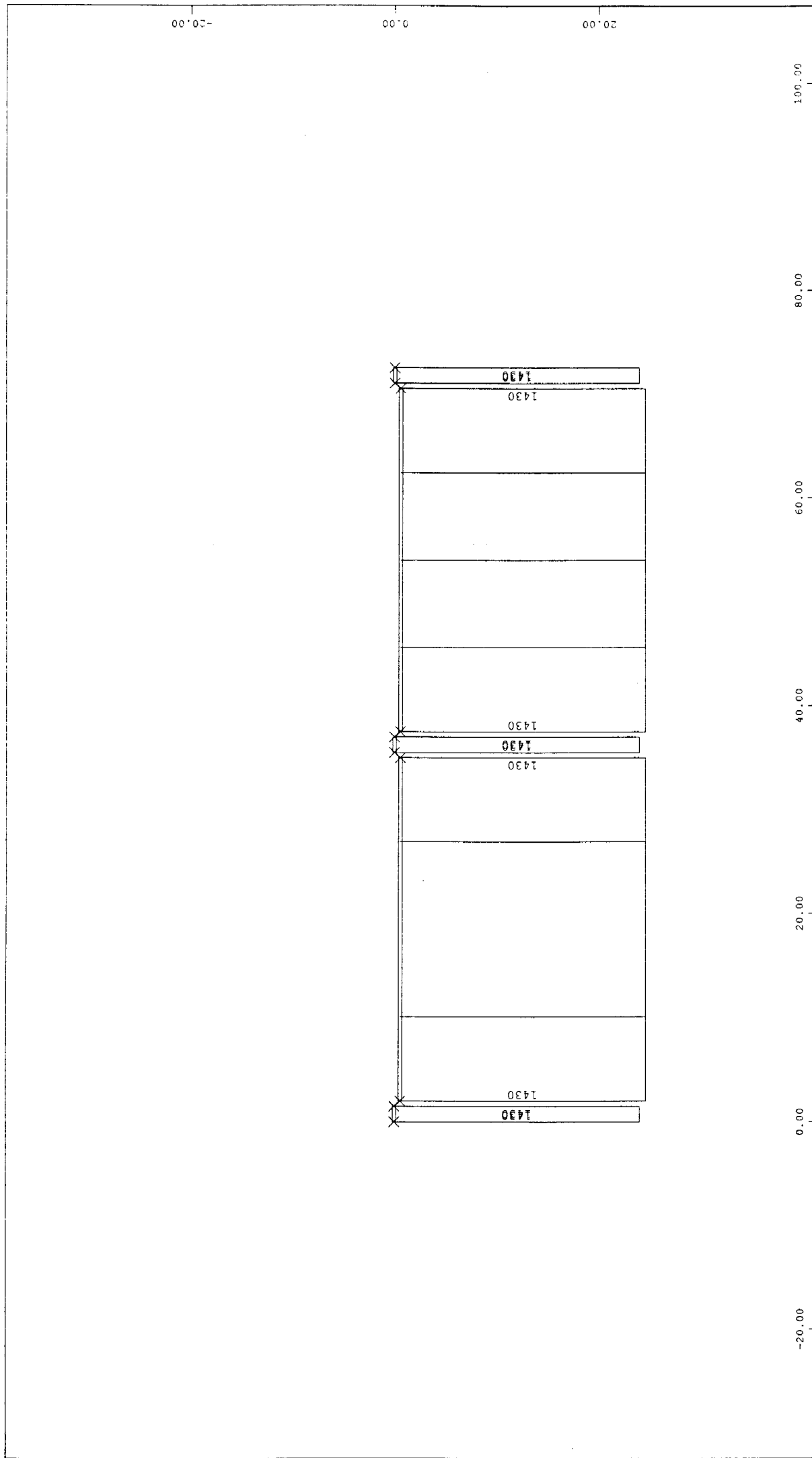
BEAM MOMENTS MY LC 1 LOAD CASE 1 1 CM = 5000 kNm

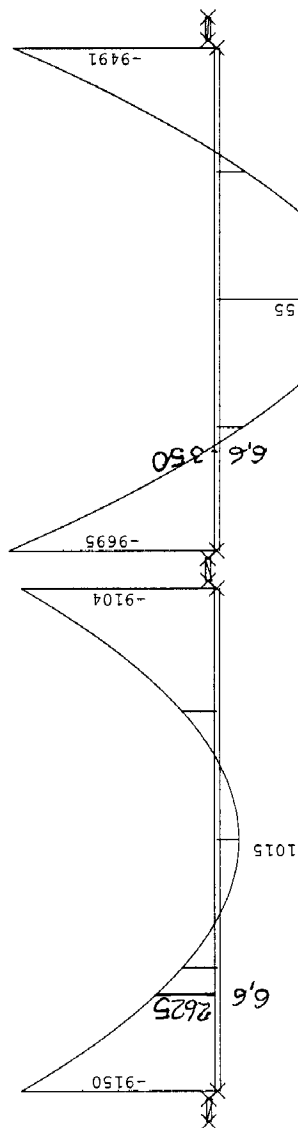
M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
----- BEAM SHEAR FORCES Q_z LC 1 LOAD CASE 1 1 CM = 1000 kN

M 1 : 500





ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$M_{cr} = - \left(\gamma_{2eff} \frac{1}{2} h_{eff} + \frac{V_{2eff}}{A_{eff}} \right) \Delta N$$

$$N = 16244 - 208 = 16036 \text{ kN} \rightarrow X = 1585 \times 16244 / 16036 = 1490 \text{ m} \rightarrow L_{eff} = 6.7 \text{ m} \rightarrow N = 16050 \text{ kN} \text{ (κατά τη διεύθυνση των ορίων)}$$

ΚΑΜΠΤΙΚΟΣ ΕΛΕΓΧΟΣ ΠΛΑΚΑΣ ΓΙΑ ΚΑΘΟΛΙΚΗ ΕΝΤΑΣΗ

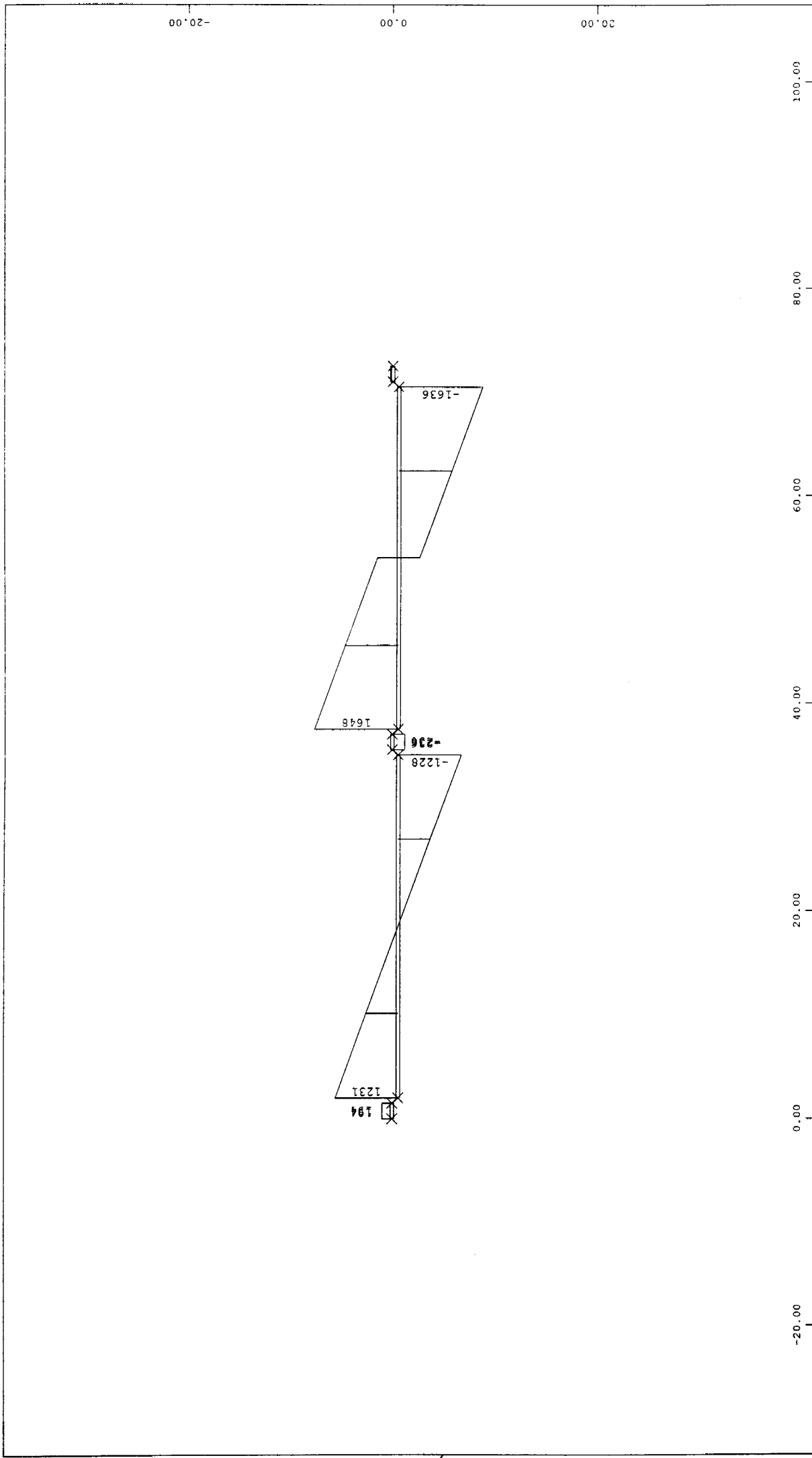
$$M = 9695 - 0.63 \times 16244 = 539 \text{ kNm}, e = 539 / 16244 = 0.033 \text{ m} < \gamma_s = 0.075 \text{ m}$$

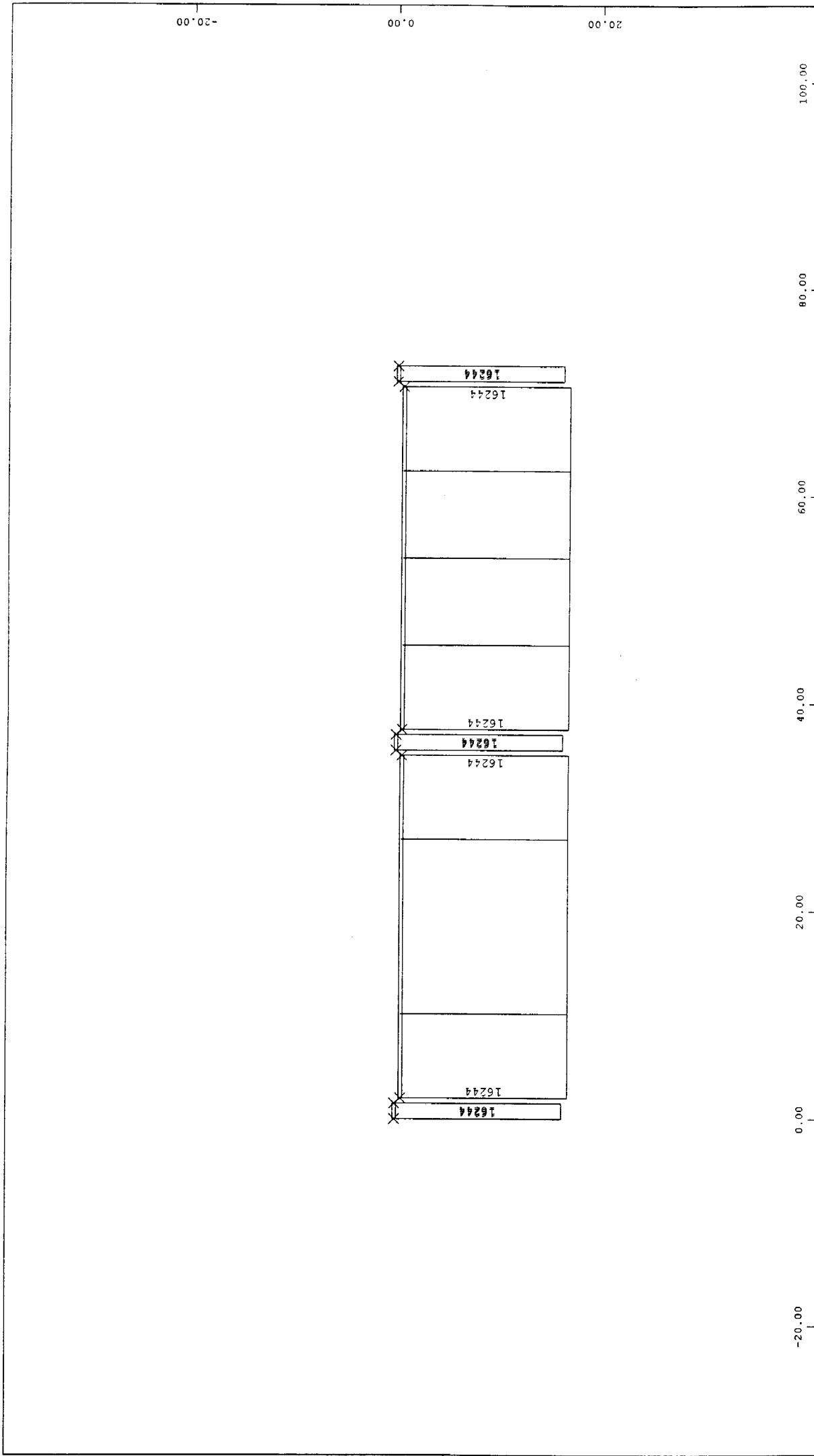
$$\text{υπ } A_s = 739 + 492 = 1231 \text{ cm}^2, \text{ υπ } \sigma_s = \frac{16244}{1231} \left(1 + \frac{0.033}{0.075} \right) = 19 < 26 \text{ kN/cm}^2 \text{ (ανεβείτε σε ευρος ρωγμές)}$$

$$\text{ΠΑΡΑΤΗΡΗΣΗ: } \epsilon_{ενδ} \approx N = 16050 \text{ kN} \text{ δεν χρειάζεται διόρθωση } \sigma_{δρδ} \text{ (από τον } \sigma_{δρδ} \text{ στον } \sigma_{δρδ} \text{)}$$

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500





INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

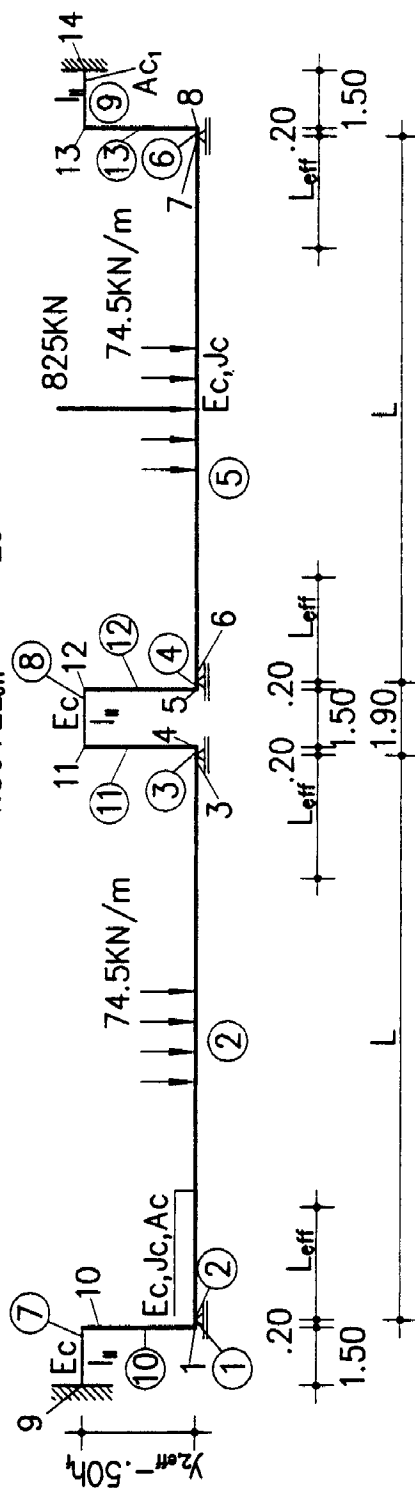
SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

M 1 : 500

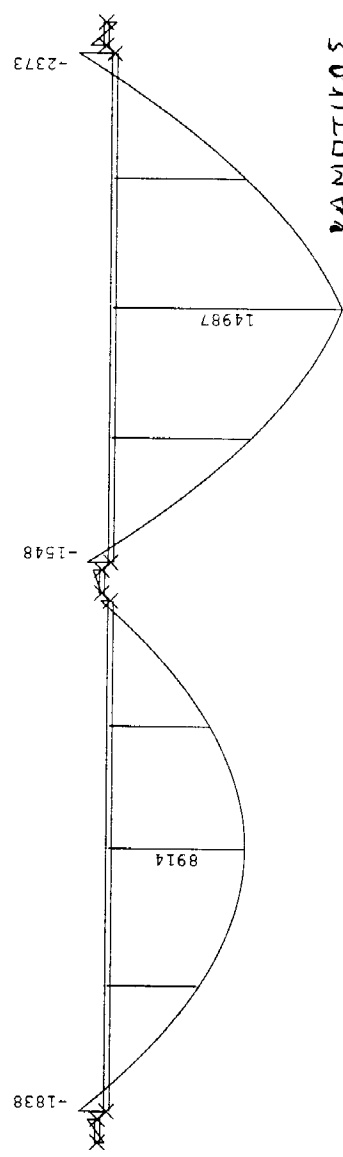
$$A_{C1} = \frac{1.50}{1.50 + L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$

$$A_{C2} = \frac{1.50}{1.50 + 2L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$



ΠΙΝΑΚΑΣ ΔΕΔΟΜΕΝΩΝ

$L = 33.0\text{m}$	$E_c = 32\text{ GPa}$
$b = 12.0\text{m}$	$a = 6.25$
$A_{c,eff} = 5.100\text{m}^2$	$g_1 = 30.7\text{kN/m}$
$J_{c,eff} = 2.784\text{m}$	$q = 43.8\text{kN/m}$
$h_b = 2.15\text{m}$	$g_1 + q = 74.5\text{kN/m}$
$h_{ft} = 0.275\text{m}$	$Q = 825\text{kN}$
$h_{k,eff} = 0.20\text{m}$	$A_{st} = 739\text{cm}^2 (3 \phi 14/75)$
$h(n.p.) = 0.075\text{m}$	$\rho = 3.1\%$
$y_{2,eff} = 0.73\text{m}$	$A_{sb} = 20.5\text{cm}^2 (4 \phi 14/75)$
	$T = -50\text{ C}$
	$L_{eff} = L/5 = 6.6\text{m}$
$I_{II} = 3.544apbh^3_{k,eff}/12 = 0.1772p = I_x/2.5 = 0.0031\text{m}^4$	



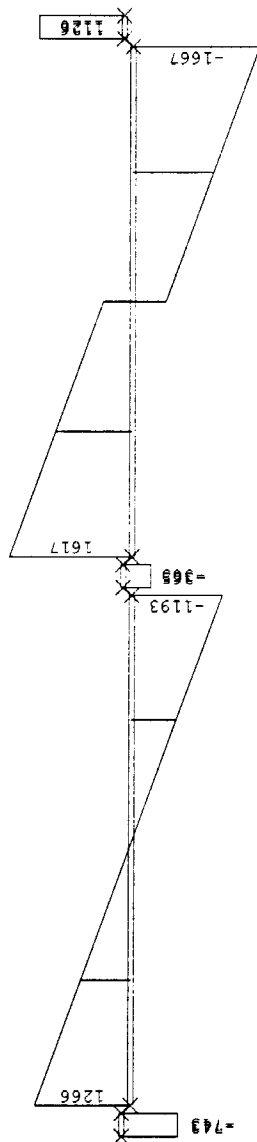
ΠΑΜΠΤΙΚΟΣ ΕΝΕΡΓΟΣ ΠΛΑΚΑΣ
ΓΙΑ ΦΟΡΤΙΑ ΒΑΡΥΤΗΤΟΣ

$$m = \frac{2373 - 0,63 \cdot 1374}{12,0} = 126 \text{ kNm/m}$$
$$m_s = 126 - 0,075 \times \frac{1374}{12,0} = 117 \text{ kNm/m}$$
$$a_s = 4,2 \times \frac{117}{17,5} + \frac{1374}{120 \times 26} = 32,5 < 2 \times 20,5 = 41 \text{ cm}^2/\text{m}$$

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0
— BEAM MOMENTS MY LC 1 LOAD CASE 1 1 CM = 5000 kNm

M 1 : 500

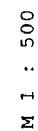


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM SHEAR FORCES QZ LC 1 LOAD CASE 1 1 CM = 1000 kN

M 1 : 500



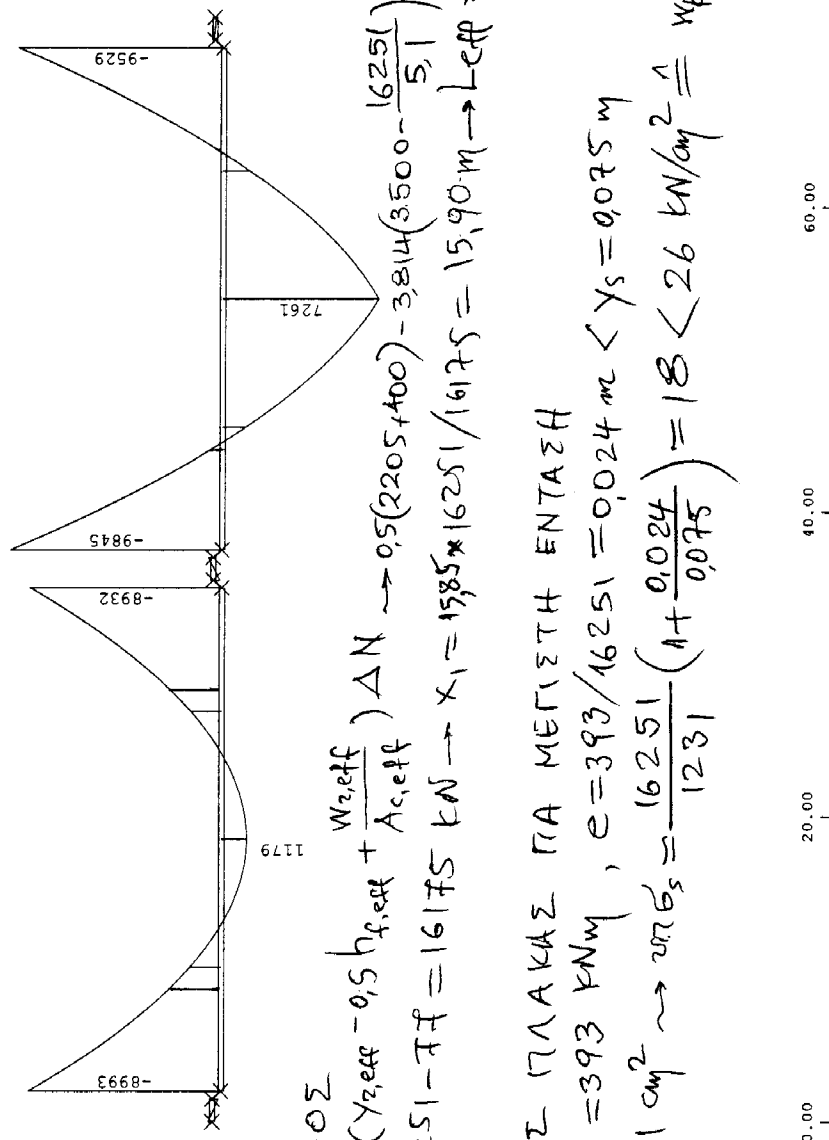
SECTOR OF SYSTEM, ELEMENT GROUP 0

SECTION OF SYSTEM, ELEMENT GROUP 0

X

Y

Z



ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$u \Delta M(x=L_{eff}) - M_{cr} = -(Y_{z,eff} - 0,5 Y_{x,eff} + \frac{W_{z,eff}}{A_{c,eff}}) \Delta N \rightarrow 0,5(2205+400) - 3814(3500 - \frac{16251}{5,1}) = -1,38 \Delta N_1 = -1196 = 10 \text{ t}$$

$$\Delta N_1 = -7 \text{ t kN} \rightarrow N_1 = 16251 - 7 \text{ t} = 16175 \text{ kN} \rightarrow x_1 = 1585 \times 16251 / 16175 = 15,90 \text{ m} \rightarrow L_{eff} = 6,6 \text{ m} \rightarrow N = 16.200 \text{ kN}$$

ΚΑΜΠΤΙΚΟΣ ΕΛΕΓΧΟΣ ΠΛΑΚΑΣ ΠΑ ΜΕΓΙΣΤΗ ΕΝΤΑΣΗ

$$M_1 = 9845 - 0,63 \times 16251 = 393 \text{ kNm}, e = 393 / 16251 = 0,024 \text{ m} < x_s = 0,075 \text{ m}$$

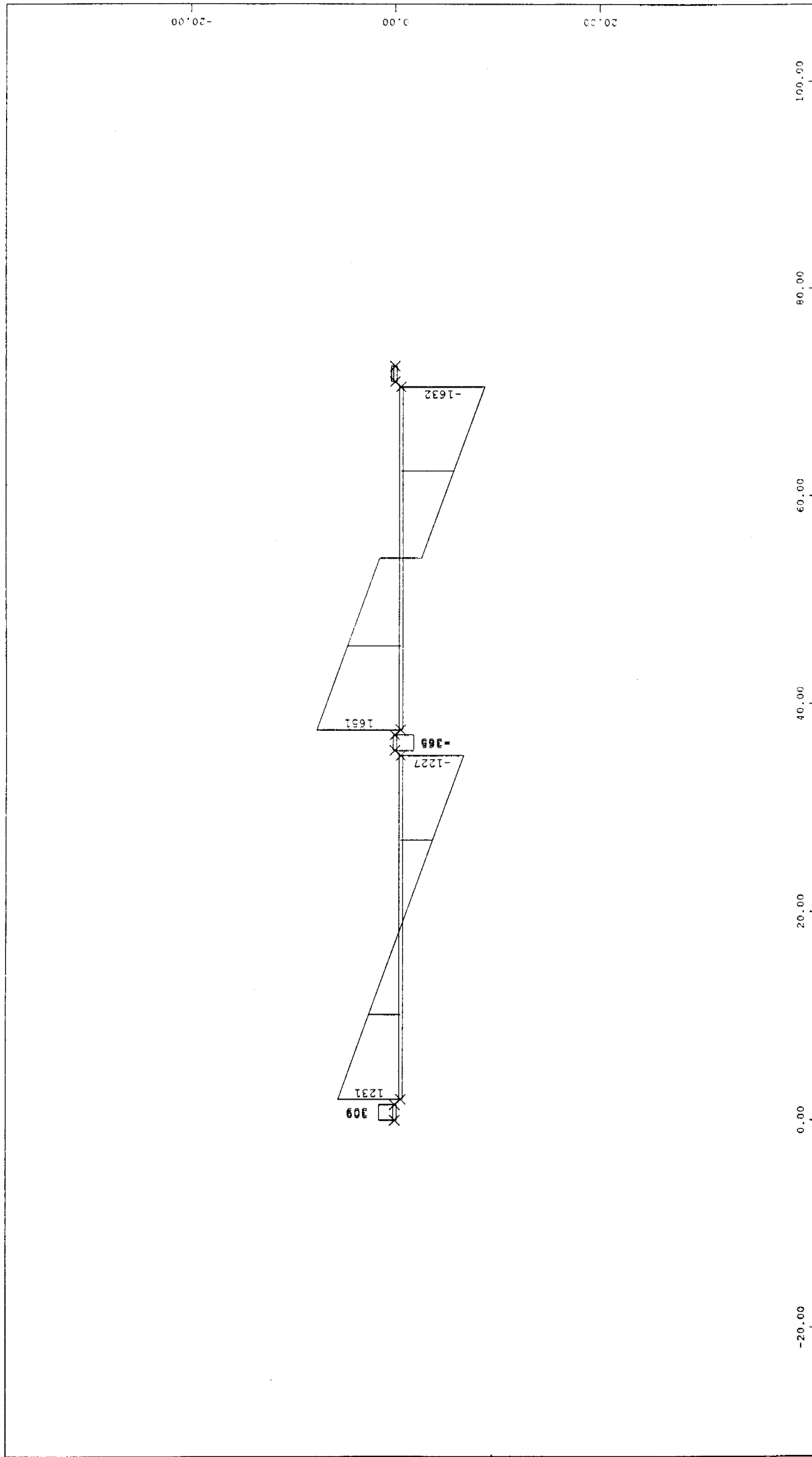
$$u \sigma A_s = 739 + 492 = 1231 \text{ cm}^2 \rightarrow \sigma_{cr} = \frac{16251}{1231} \left(1 + \frac{0,024}{0,075} \right) = 18 < 26 \text{ kN/cm}^2 \Rightarrow w_k = 0,1 \text{ mm}$$

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

----- BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500

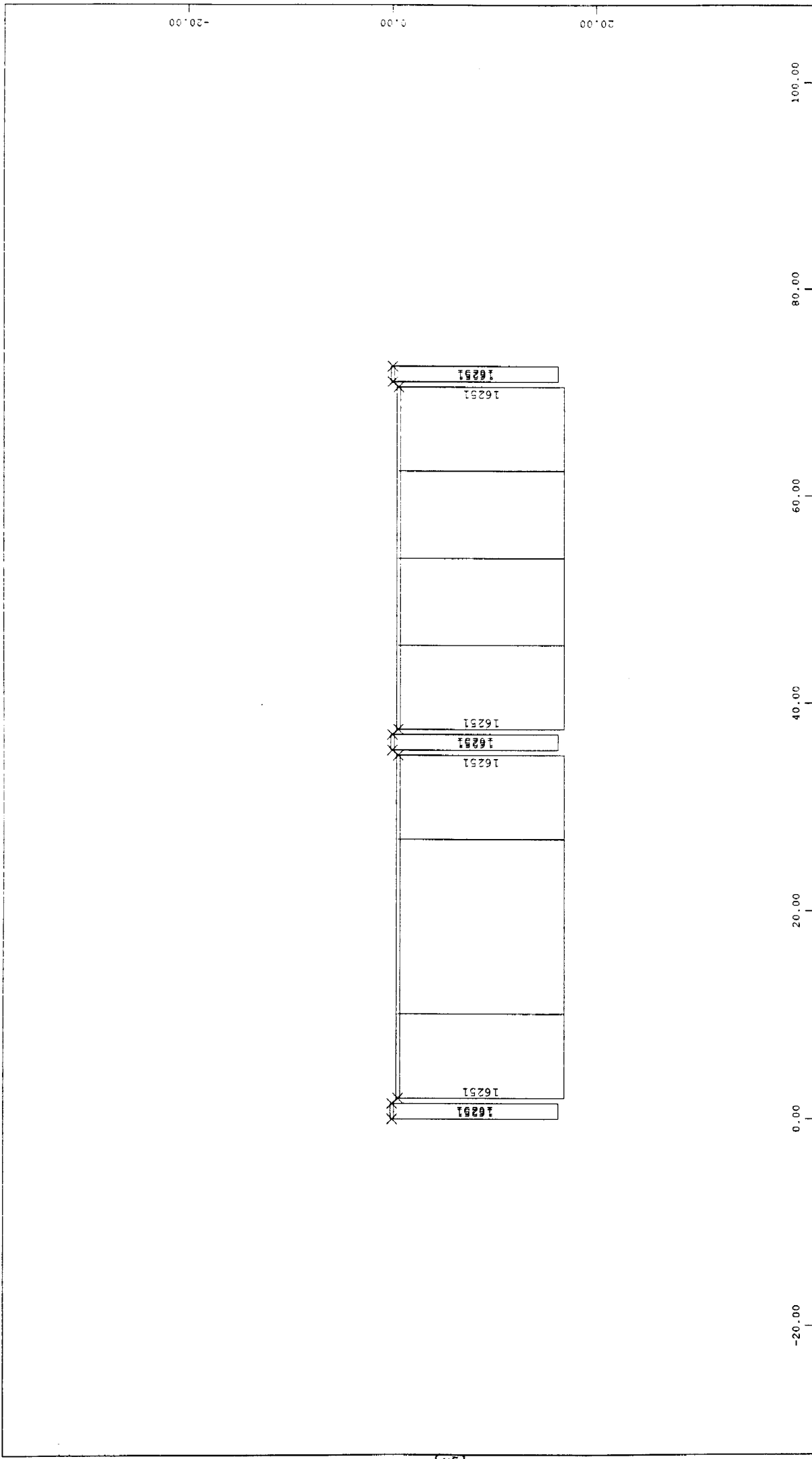


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM SHEAR FORCES Q_z LC 2 LOAD CASE 2 1 CM = 1000 kN

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

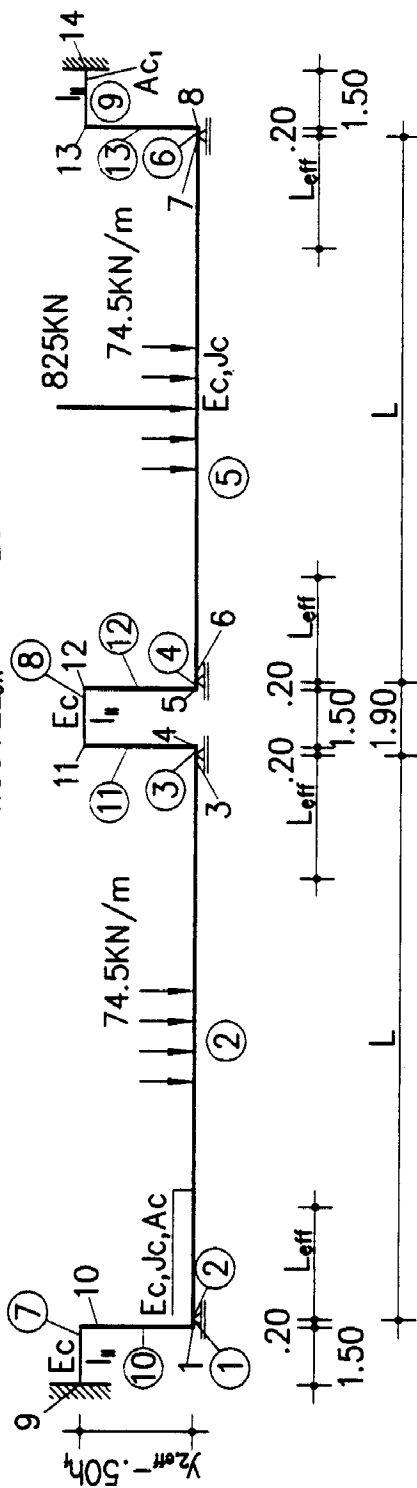
SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

M 1 : 500

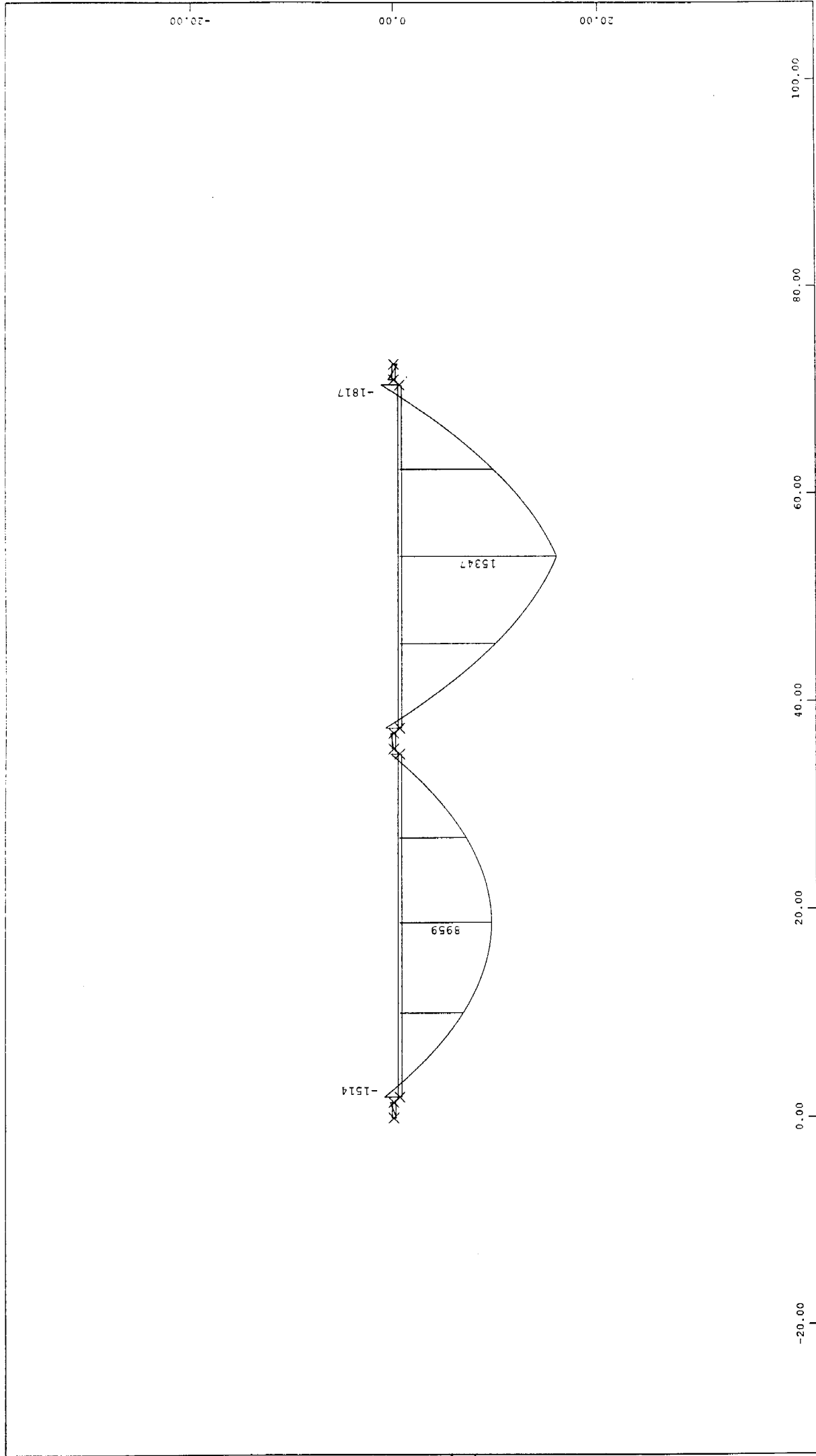
$$A_{C1} = \frac{1.50}{1.50 + L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$

$$A_{C2} = \frac{1.50}{1.50 + 2L_{eff}} \cdot 1.2 A_s \frac{E_s}{E_c}$$



ΠΙΝΑΚΑΣ ΔΕΔΟΜΕΝΩΝ

$L = 33.0\text{m}$	$E_c = 32\text{ GPa}$
$b = 12.0\text{m}$	$a = 6.25$
$A_{c,eff} = 5.100\text{m}^2$	$g_1 = 30.7\text{kN/m}$
$J_{c,eff} = 2.784\text{m}$	$q = 43.8\text{kN/m}$
$h_b = 2.15\text{m}$	$g_1 + q = 74.5\text{kN/m}$
$h_{ft} = 0.275\text{m}$	$Q = 825\text{kN}$
$h_{r,eff} = 0.20\text{m}$	$A_{st} = 986\text{cm}^2 \left(\frac{4\phi 14}{3.5} \right)$
$h_{(np.)} = 0.075\text{m}$	$\rho = 4.1\%$
$y_{2,eff} = 0.73\text{m}$	$A_{st} = 20.5\text{cm}^2 \left(\frac{\phi 14}{7.5} \right)$
	$T = -50^\circ\text{C}$
	$L_{eff} = L/5 \approx 6.6\text{m}$
$I_{II} = 3.544 a \rho b h_{r,eff}^3 / 12 = 0.1772 \rho \approx 0.0030\text{m}^4 \approx I_{I/2.5}$	

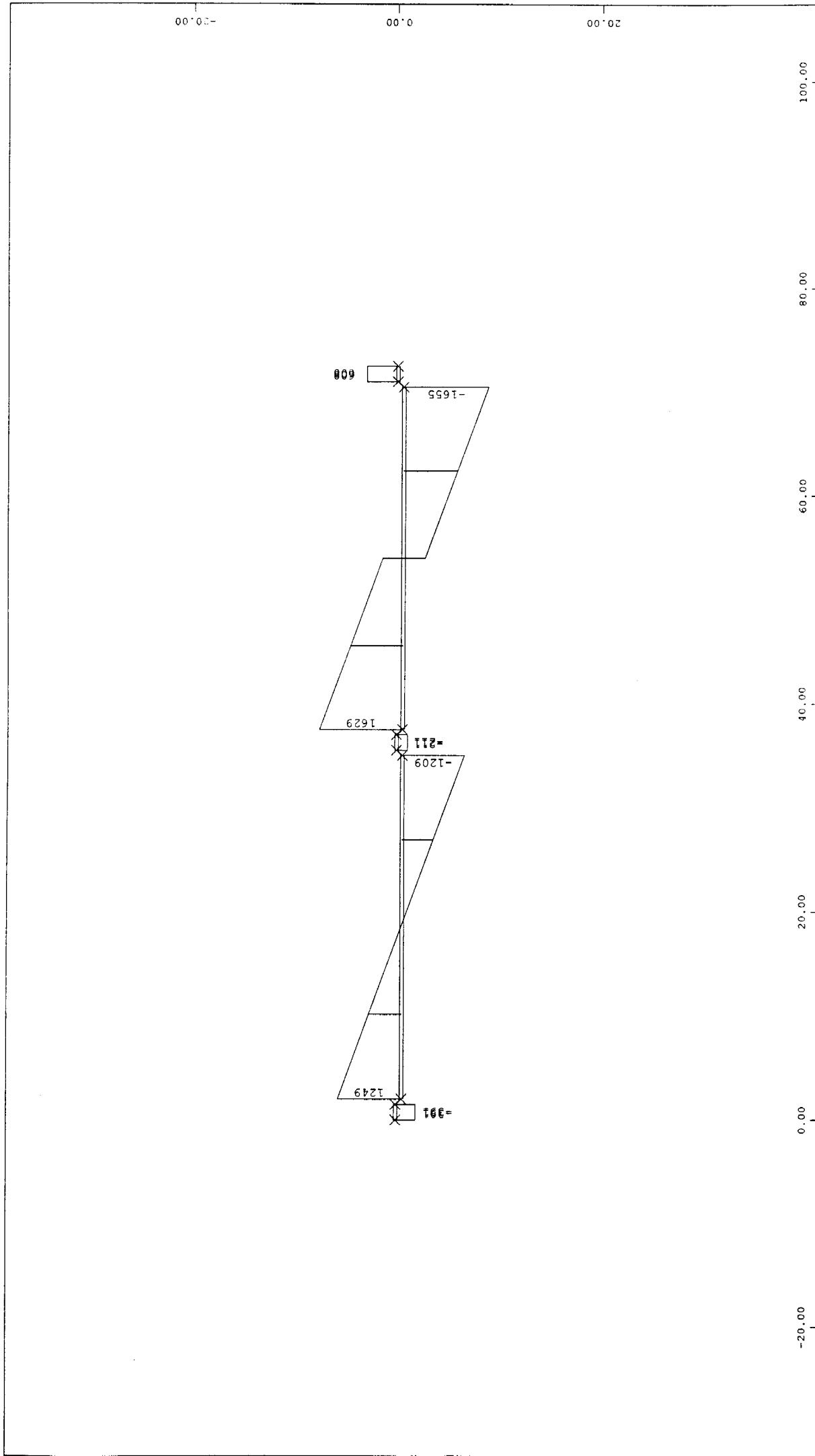


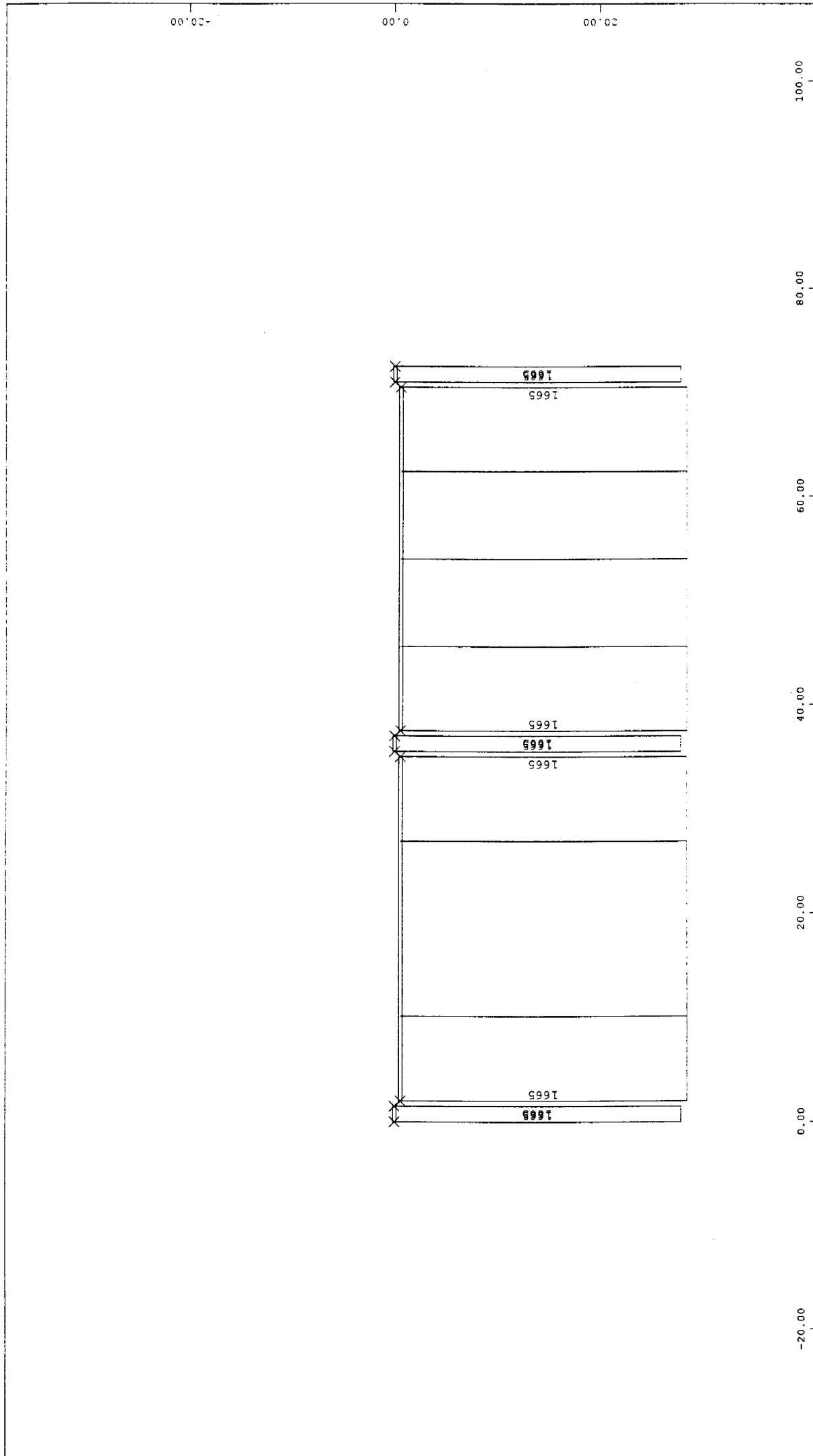
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

----- BEAM MOMENTS MY LC 1 LOAD CASE 1 1 CM = 5000 kNm

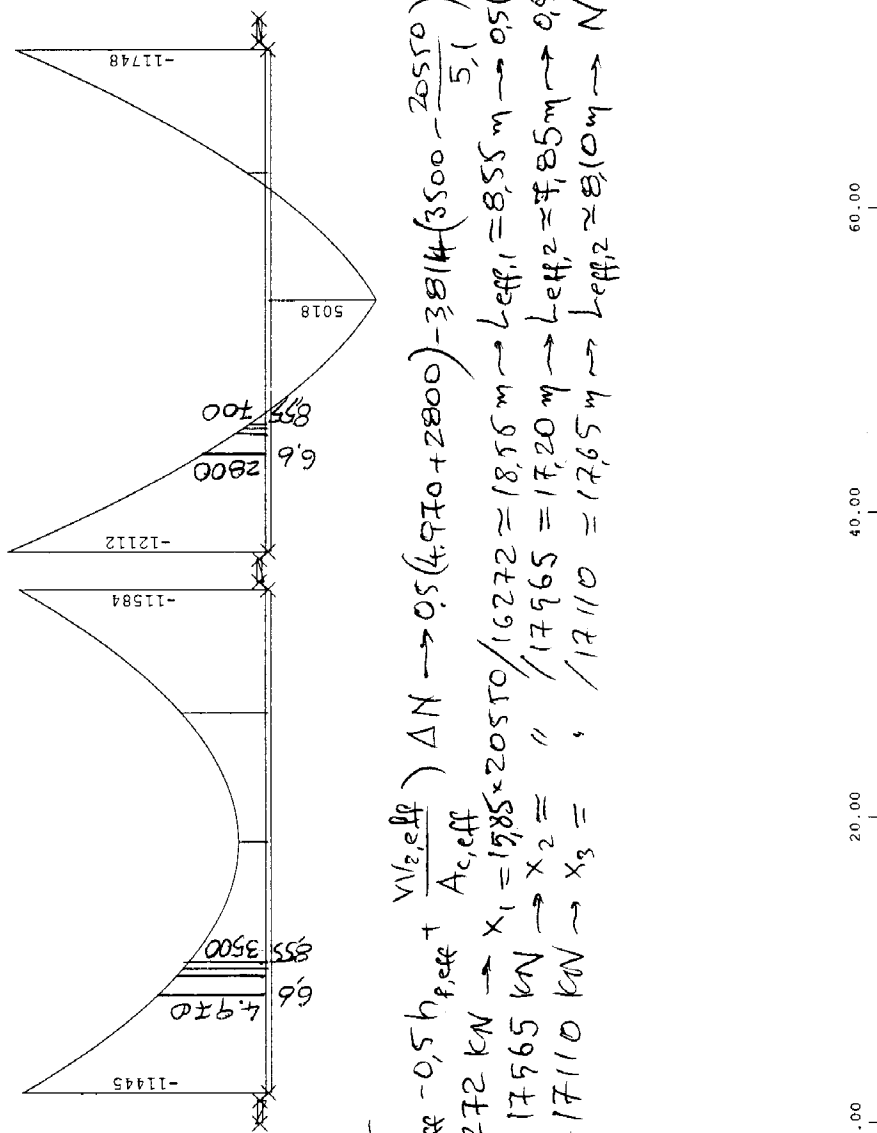
M 1 : 500





INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 BEAM NORMAL FORCES LC 1 LOAD CASE 1 1 CM = 300.0 kN

M 1 : 500

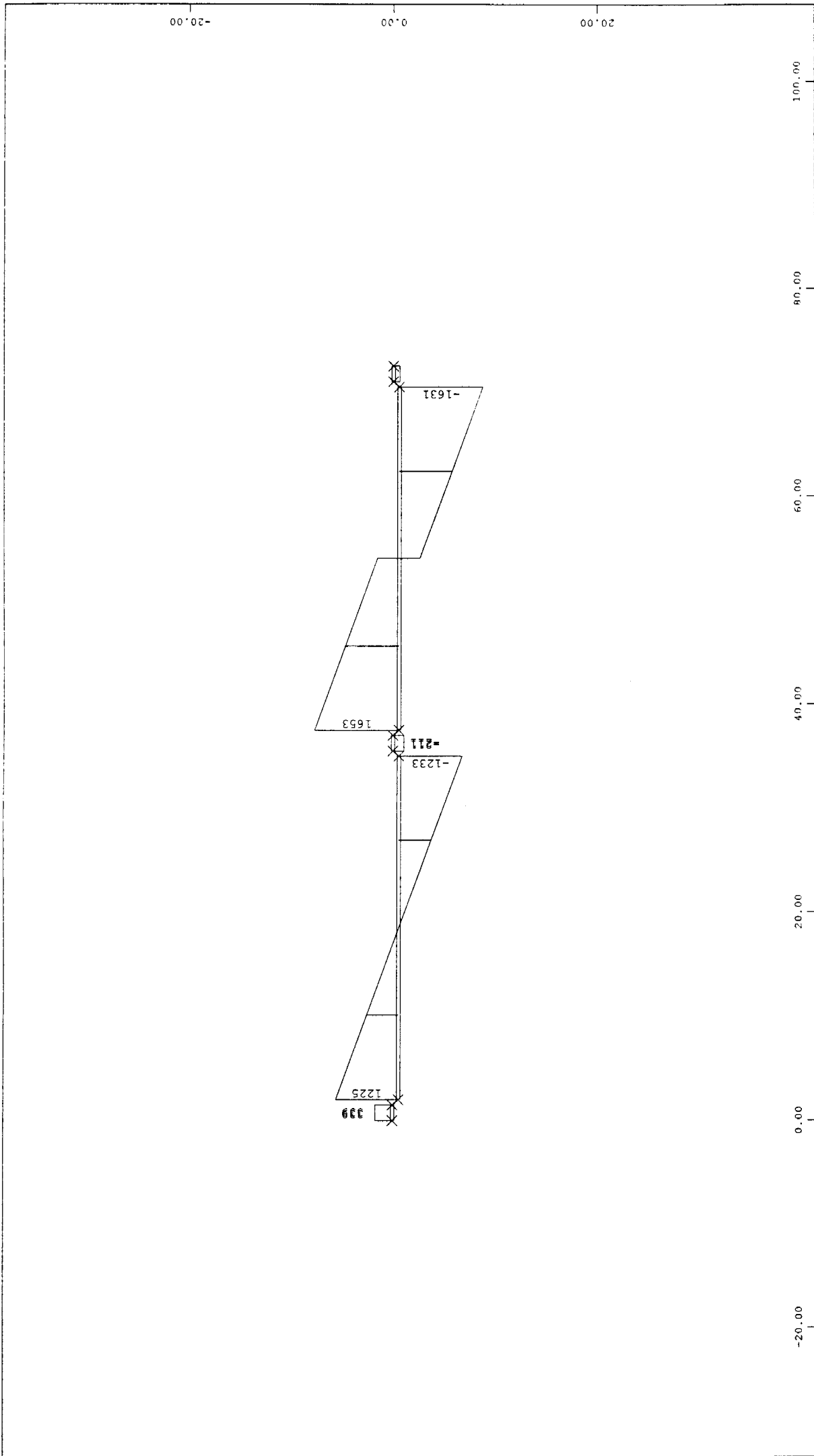


ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\begin{aligned} \Delta M(x=l_{eff}) - M_{cr} &= -(Y_{2,eff} - 0.5 h_{p,eff}) \frac{V_{1,eff}}{A_{c,eff}} \Delta N \rightarrow 0.5(4.970 + 2800) - 3814(3500 - \frac{20550}{5.1}) = 3885 + 2019 = 5904 = -138 \Delta N \\ \Delta N_1 &= -4278 \text{ kN} \rightarrow N_1 = 16272 \text{ kN} \rightarrow x_1 = 1585 \times 20550 / 16272 = 18.58 \text{ m} \rightarrow l_{eff,1} = 8.55 \text{ m} \rightarrow 0.5(3500 + 700) + 2.109 = -138 \Delta N_2 \rightarrow \\ \Delta N_2 &= -2985 \text{ kN} \rightarrow N_2 = 17565 \text{ kN} \rightarrow x_2 = " / 17965 = 17.20 \text{ m} \rightarrow l_{eff,2} = 7.85 \text{ m} \rightarrow 0.5(4130 + 1330) + 2.109 = -138 \Delta N_3 \\ \Delta N_3 &= -3441 \text{ kN} \rightarrow N_3 = 17110 \text{ kN} \rightarrow x_3 = " / 17110 = 17.65 \text{ m} \rightarrow l_{eff,2} = 8.10 \text{ m} \rightarrow N = 17150 \text{ kN} \end{aligned}$$

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
-----BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500

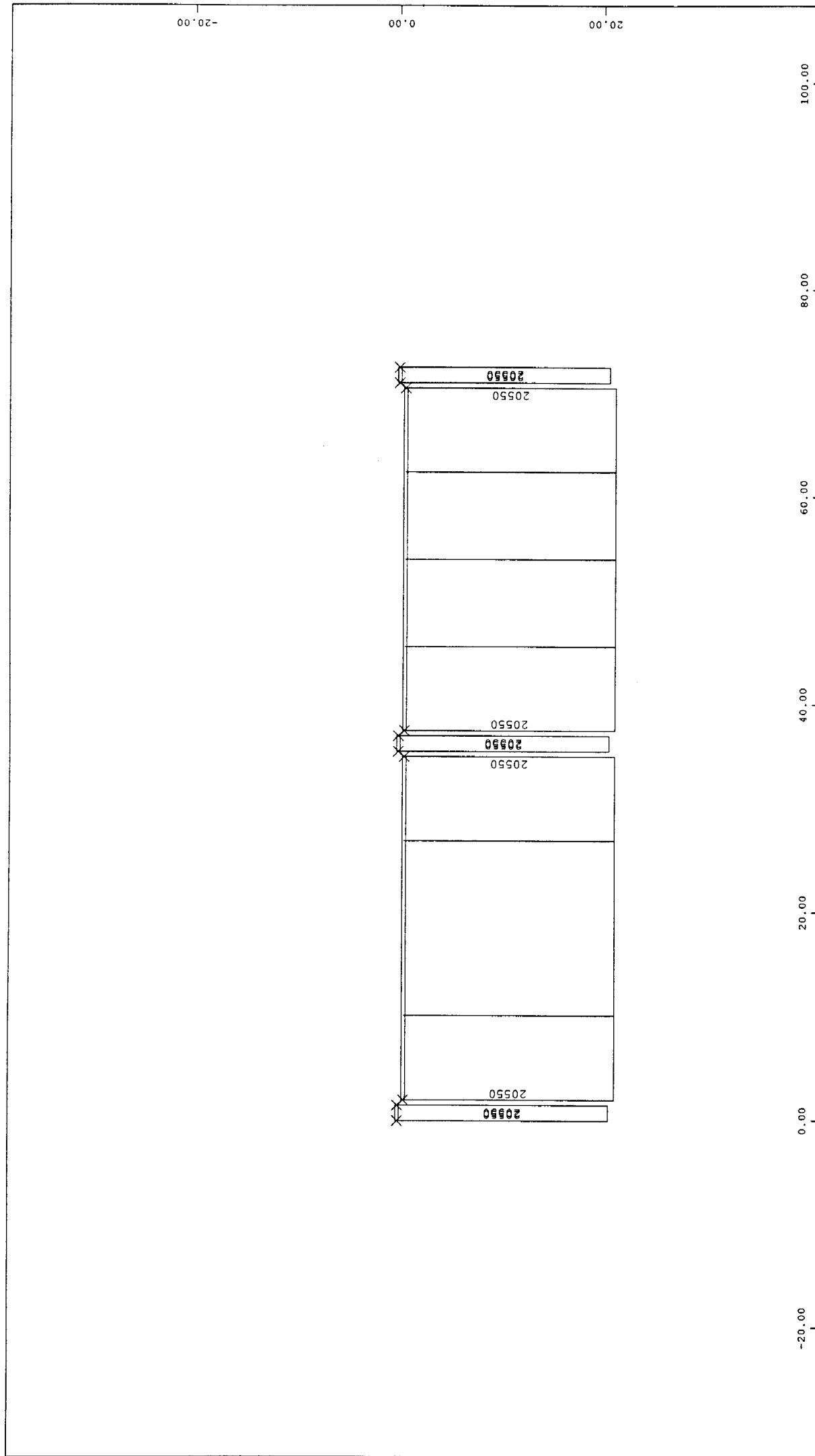


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM SHEAR FORCES QZ LC 2 LOAD CASE 2 1 CM = 1000 kN

M 1 : 500



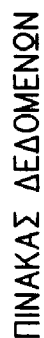
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

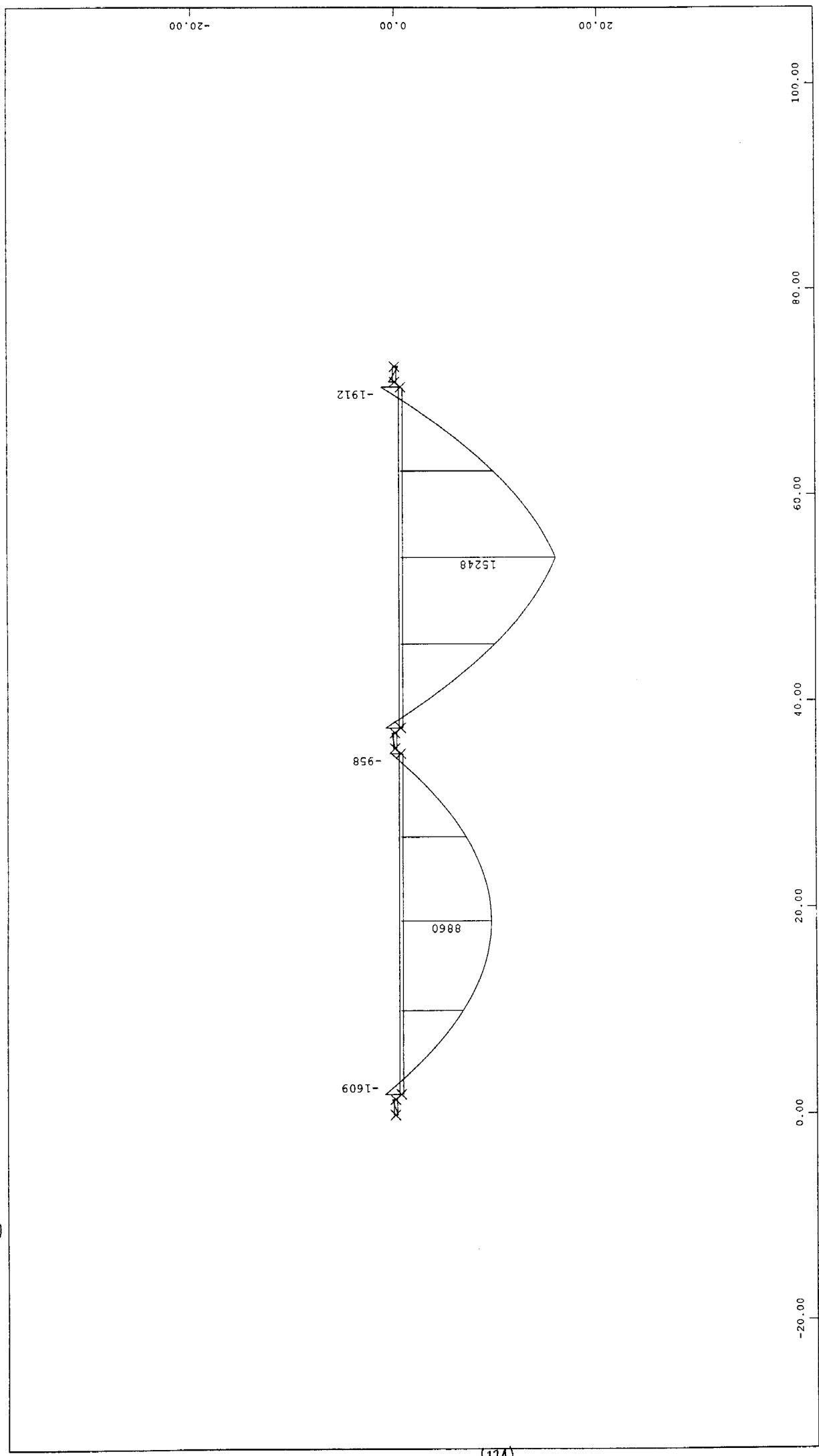
BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

M 1 : 500

$$AC_2 = \frac{1.50}{1.50 + 2L_{\text{eff}}} \quad 1.2As \frac{Es}{Ec}$$

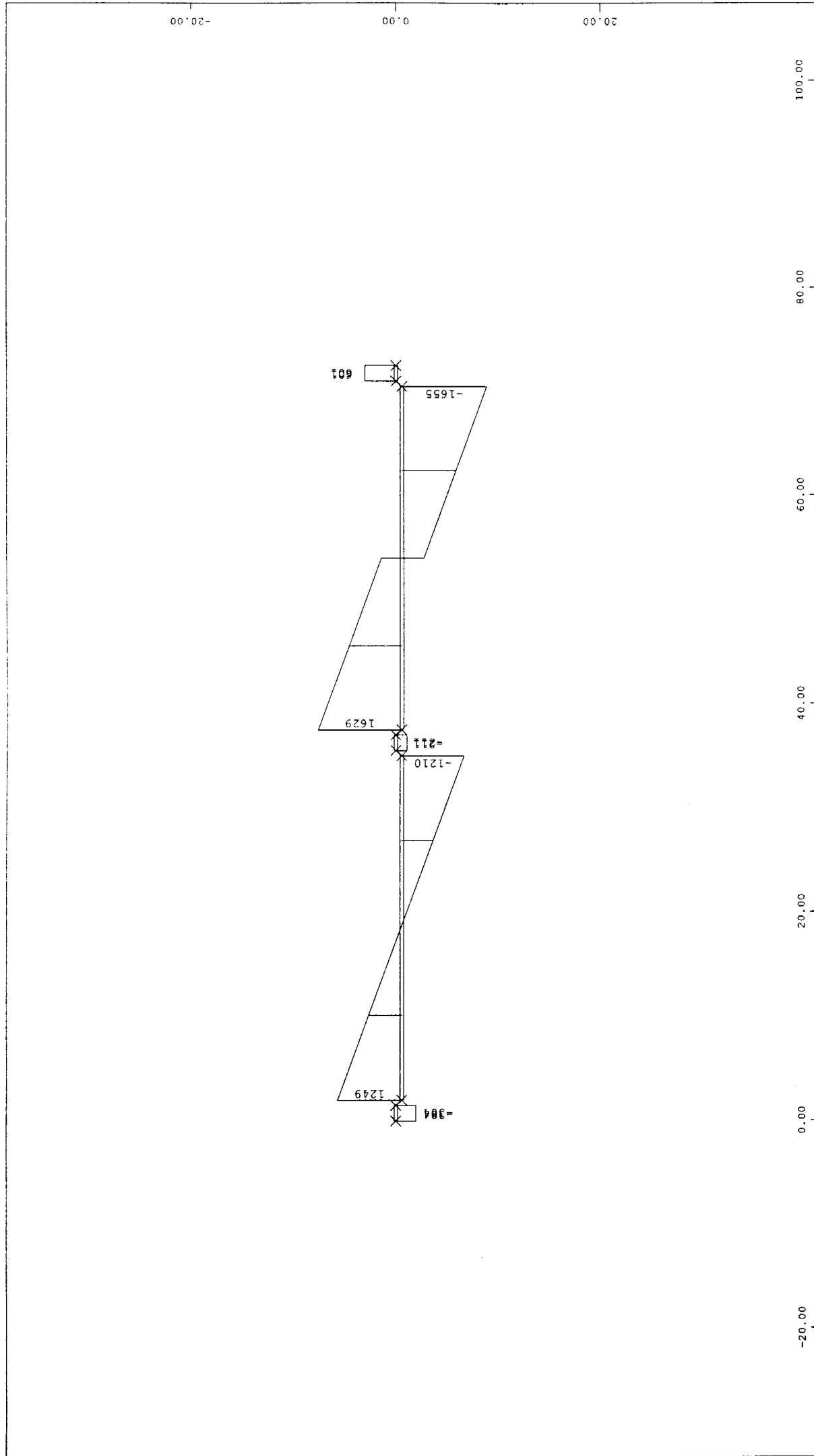


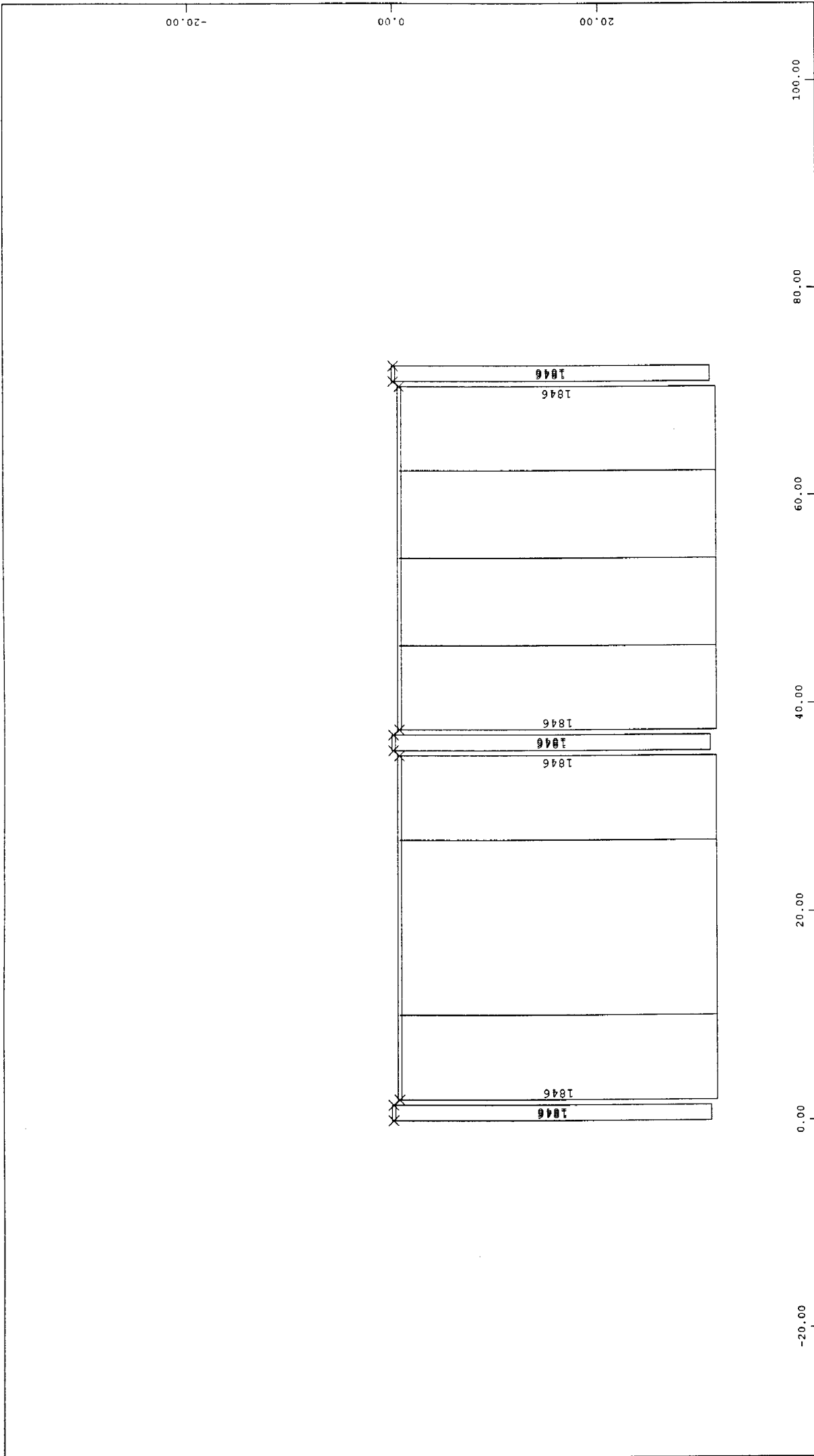
(123)



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
—— BEAM MOMENTS MY LC 1 LOAD CASE 1 1 CM = 5000 kNm

M 1 : 500

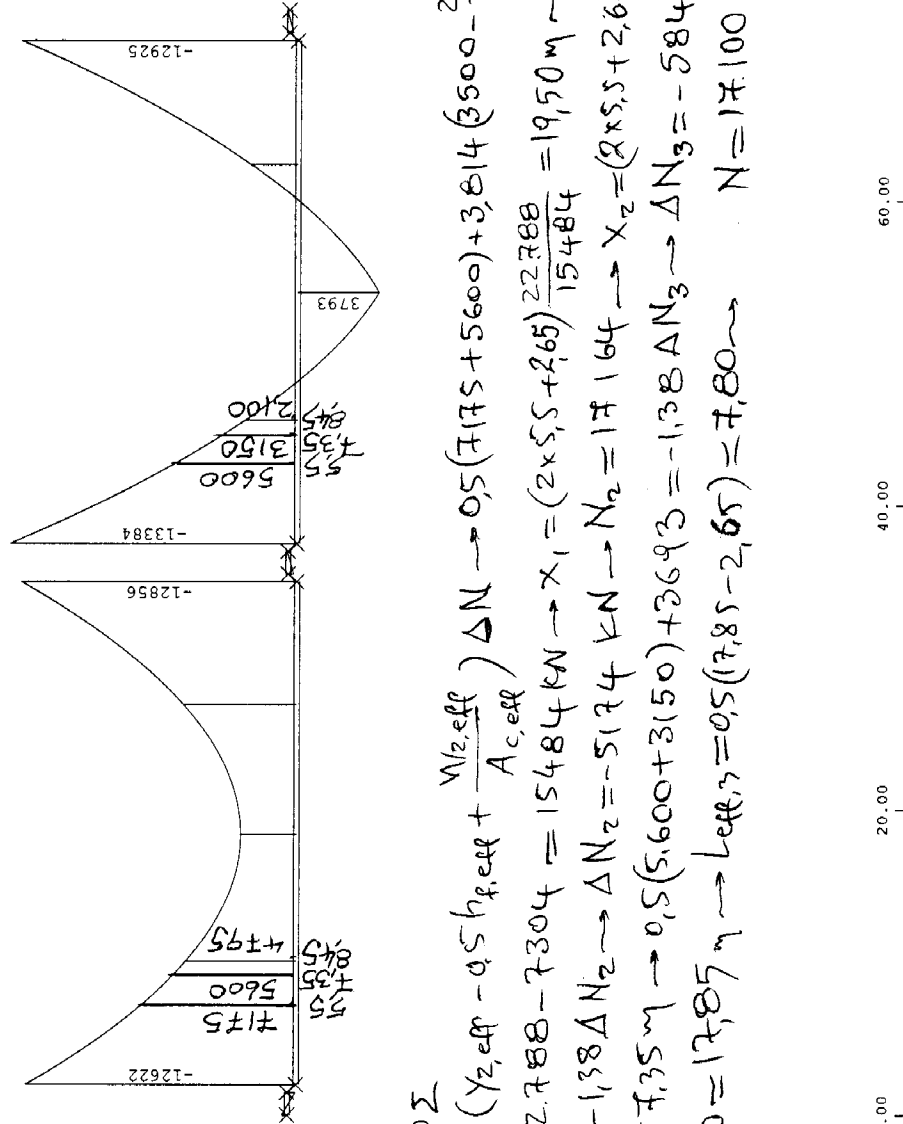




INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 ——— BEAM NORMAL FORCES LC 1 LOAD CASE 1 1 CM = 300.0 kN

x
 z

M 1 : 500



ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\Delta M(x=L_{eff}) = M_{cr} = -(Y_{2,eff} - 0,5 h_{p,eff} + \frac{V_{2,eff}}{A_{c,eff}}) \Delta N \rightarrow 0,5(7175 + 5600) + 3,814(3500 - \frac{22.788}{5,1}) = -1,38 \Delta N_1 \rightarrow$$

$$\Delta N_1 = -7304 \text{ kN} \rightarrow N_1 = 22.788 - 7304 = 15484 \text{ kN} \rightarrow X_1 = (2 \times 5,5 + 2,65) \frac{22.788}{15484} = 19,50 \text{ m} \rightarrow L_{eff,1} = 84,5 \text{ m} \rightarrow$$

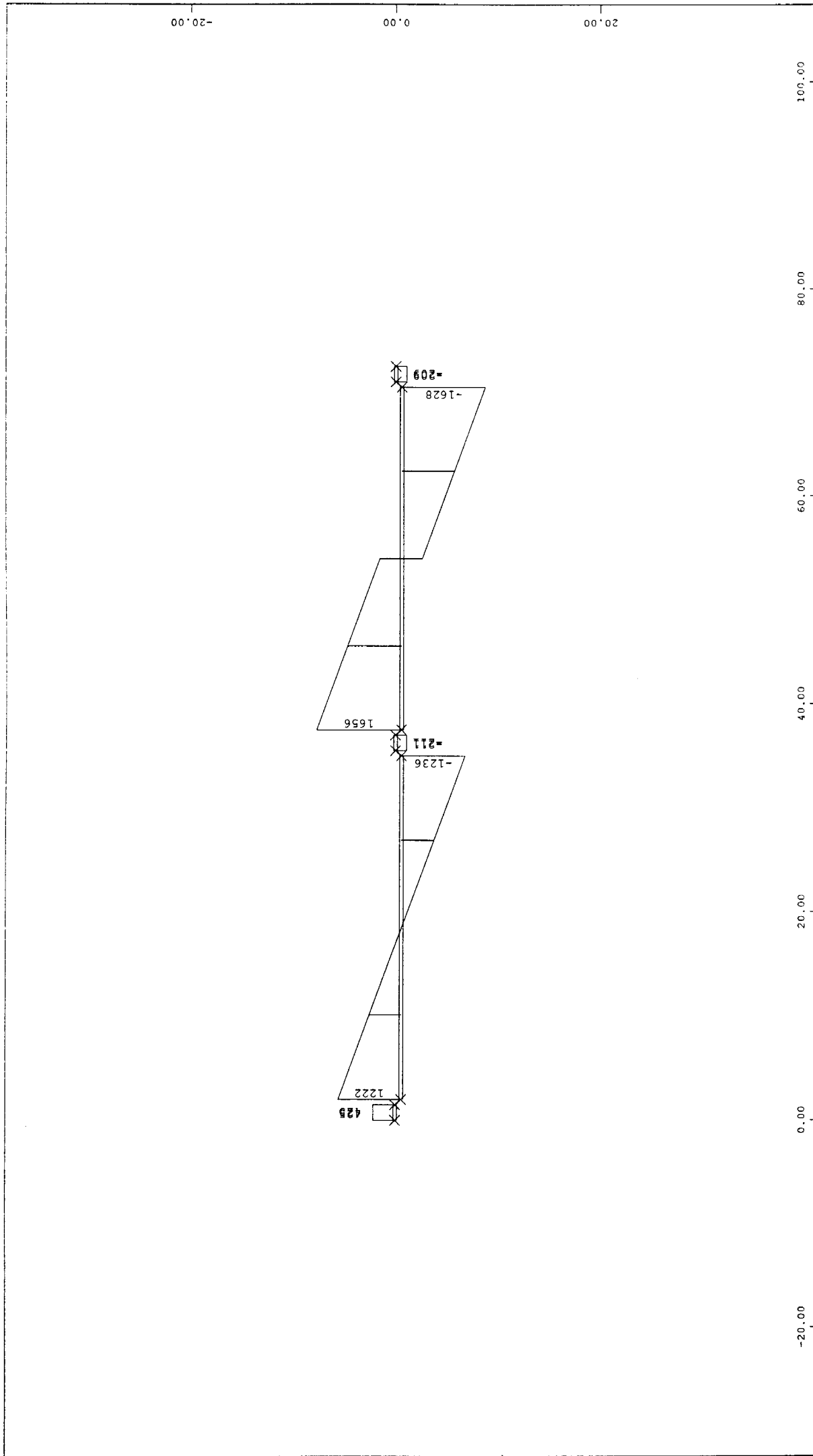
$$0,5(4795 + 2100) + 3693 = -1,38 \Delta N_2 \rightarrow \Delta N_2 = -5174 \text{ kN} \rightarrow N_2 = 17164 \rightarrow X_2 = (2 \times 5,5 + 2,65) \frac{22.788}{17614} = 17,10 \text{ m}$$

$$L_{eff,2} = 0,5(17,10 - 2,25) = 7,35 \text{ m} \rightarrow 0,5(51600 + 3(50) + 3693) = -1,38 \Delta N_3 \rightarrow \Delta N_3 = -5846 \text{ kN} \rightarrow N_3 = 16940 \text{ kN}$$

$$X_3 = 13,5 \times 22.788 / 16940 = 17,85 \text{ m} \rightarrow L_{eff,3} = 0,5(17,85 - 2,65) = 7,80 \text{ m} \rightarrow N = 17100 \text{ kN}$$

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
SECTOR OF SYSTEM, ELEMENT GROUP 0
BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500

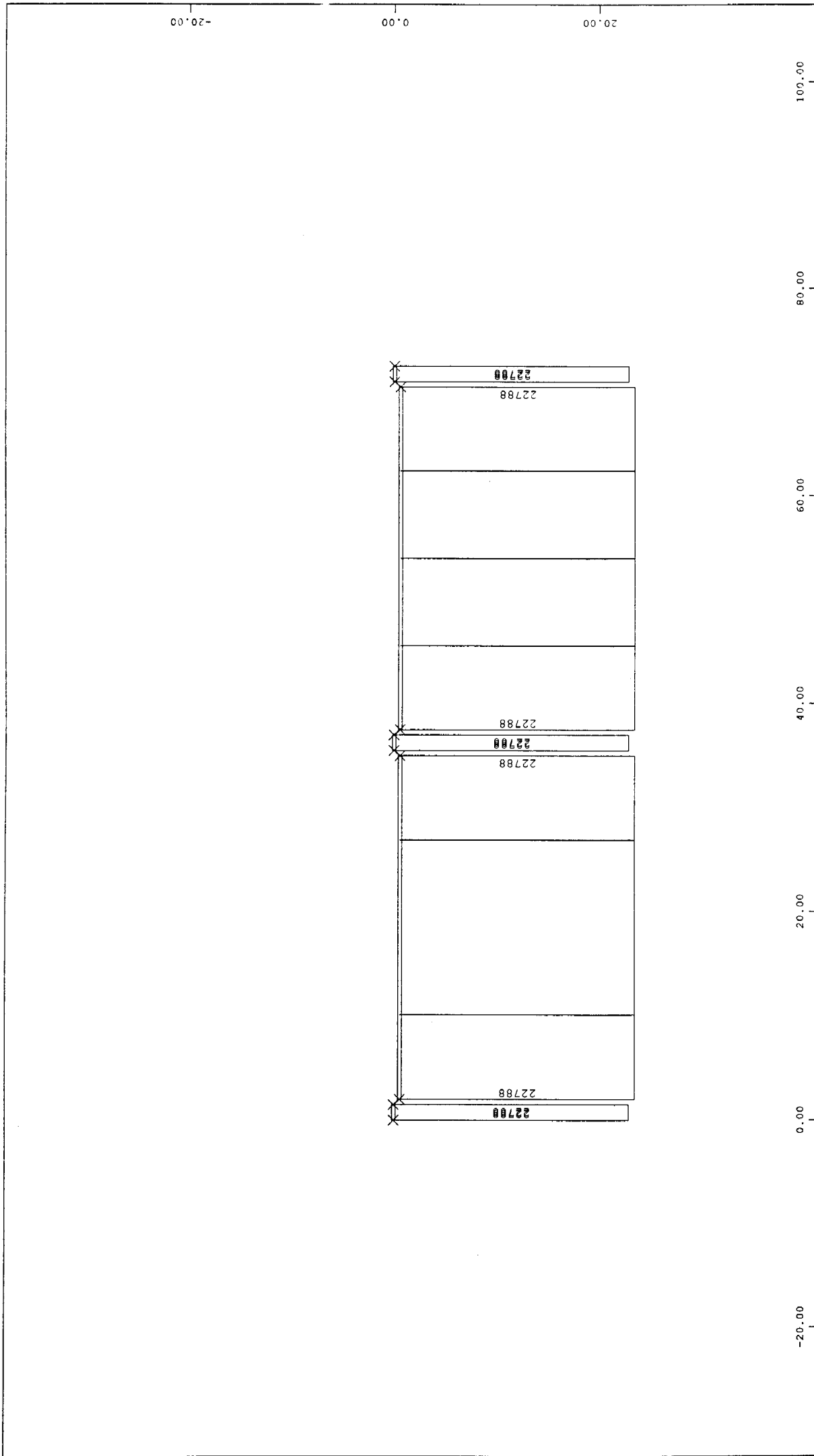


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

BEAM SHEAR FORCES Q_z LC 2 LOAD CASE 2 1 CM = 1000 kN

M 1 : 500



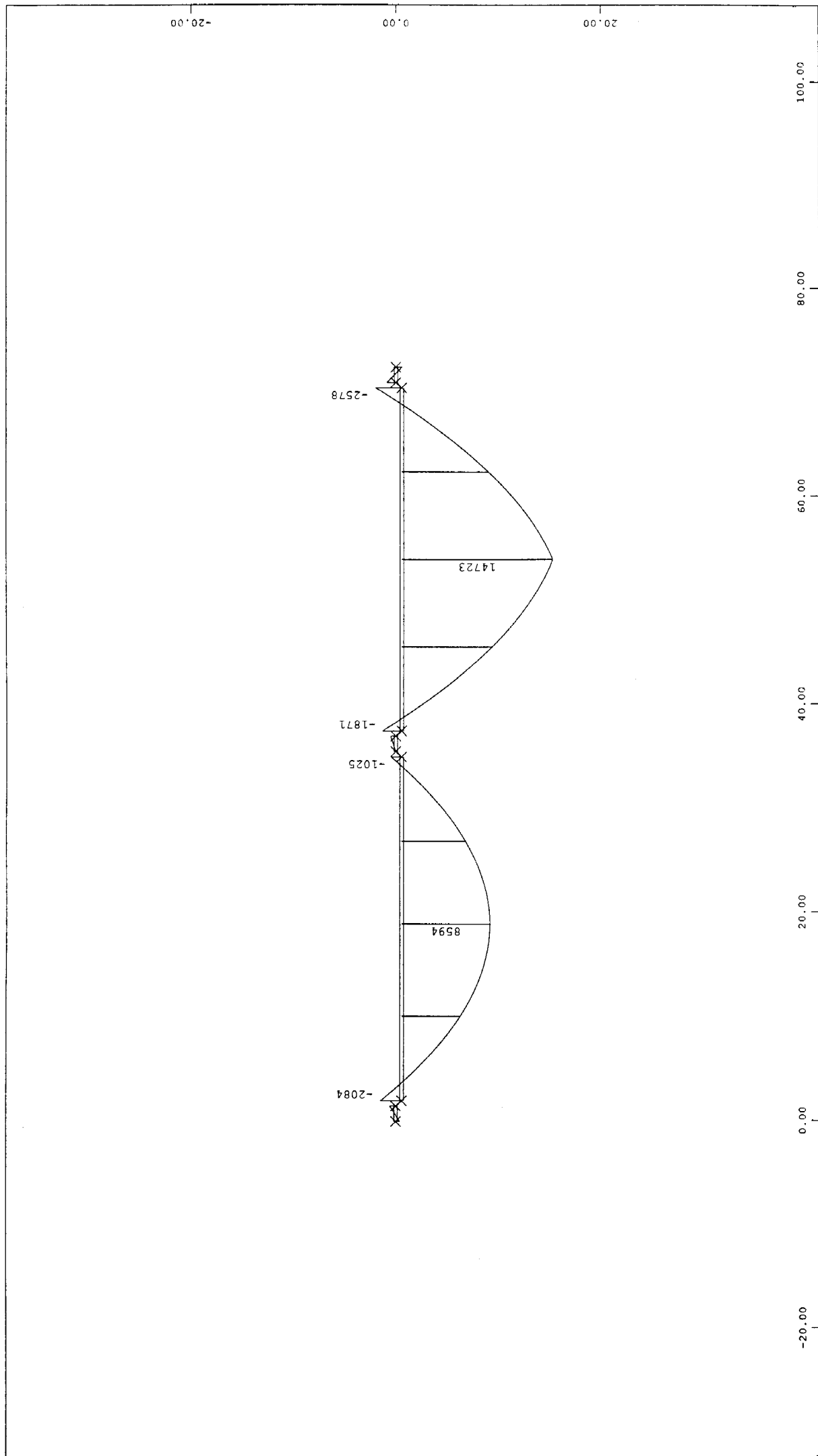
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

——— BEAM NORMAL FORCES LC 2 LOAD CASE 2 1 CM = 5000 kN

M 1 : 500





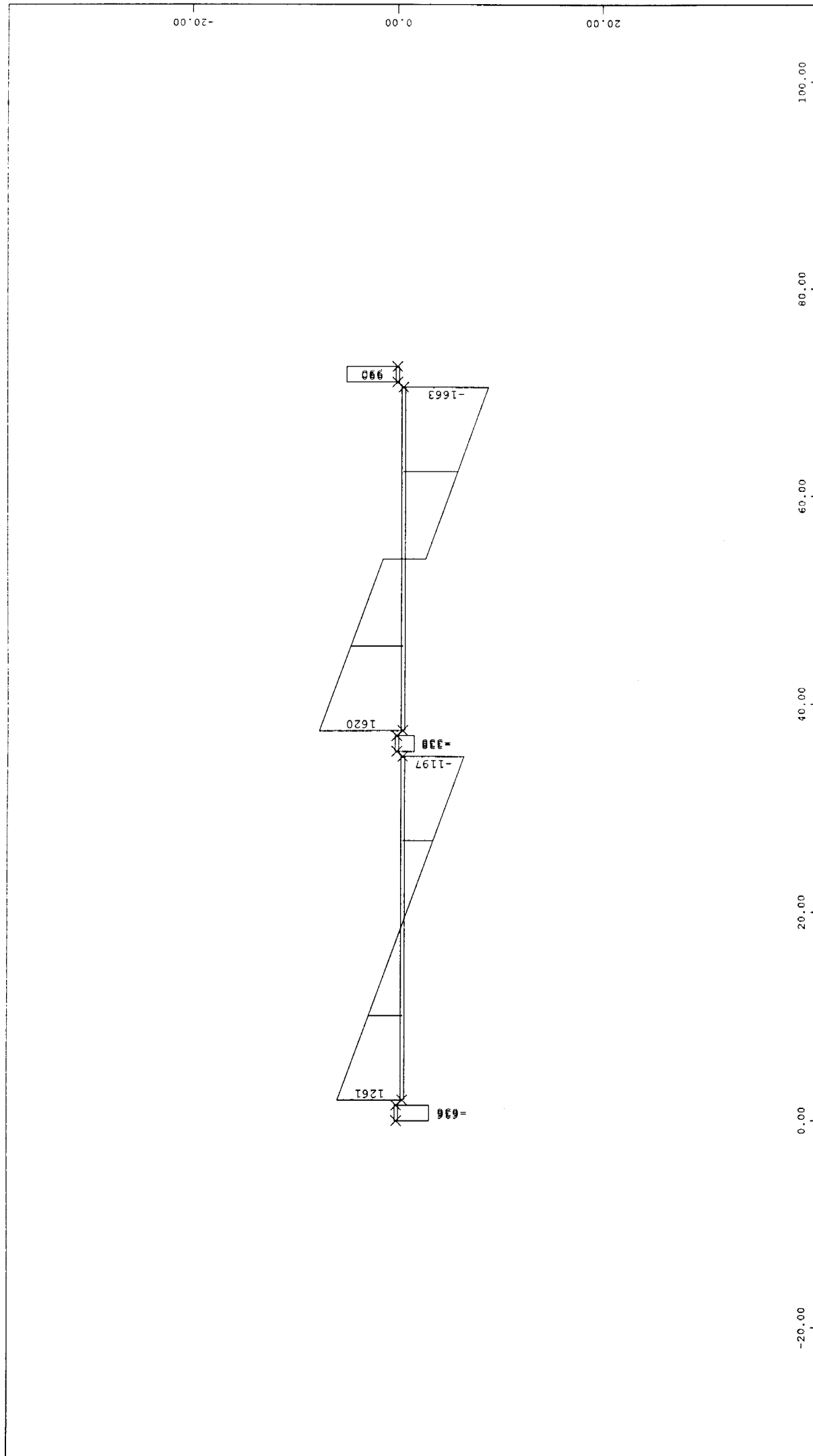
INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

— BEAM MOMENTS MY LC 1 LOAD CASE 1 1 CM = 5000 kNm

M 1 : 500

x
y
z

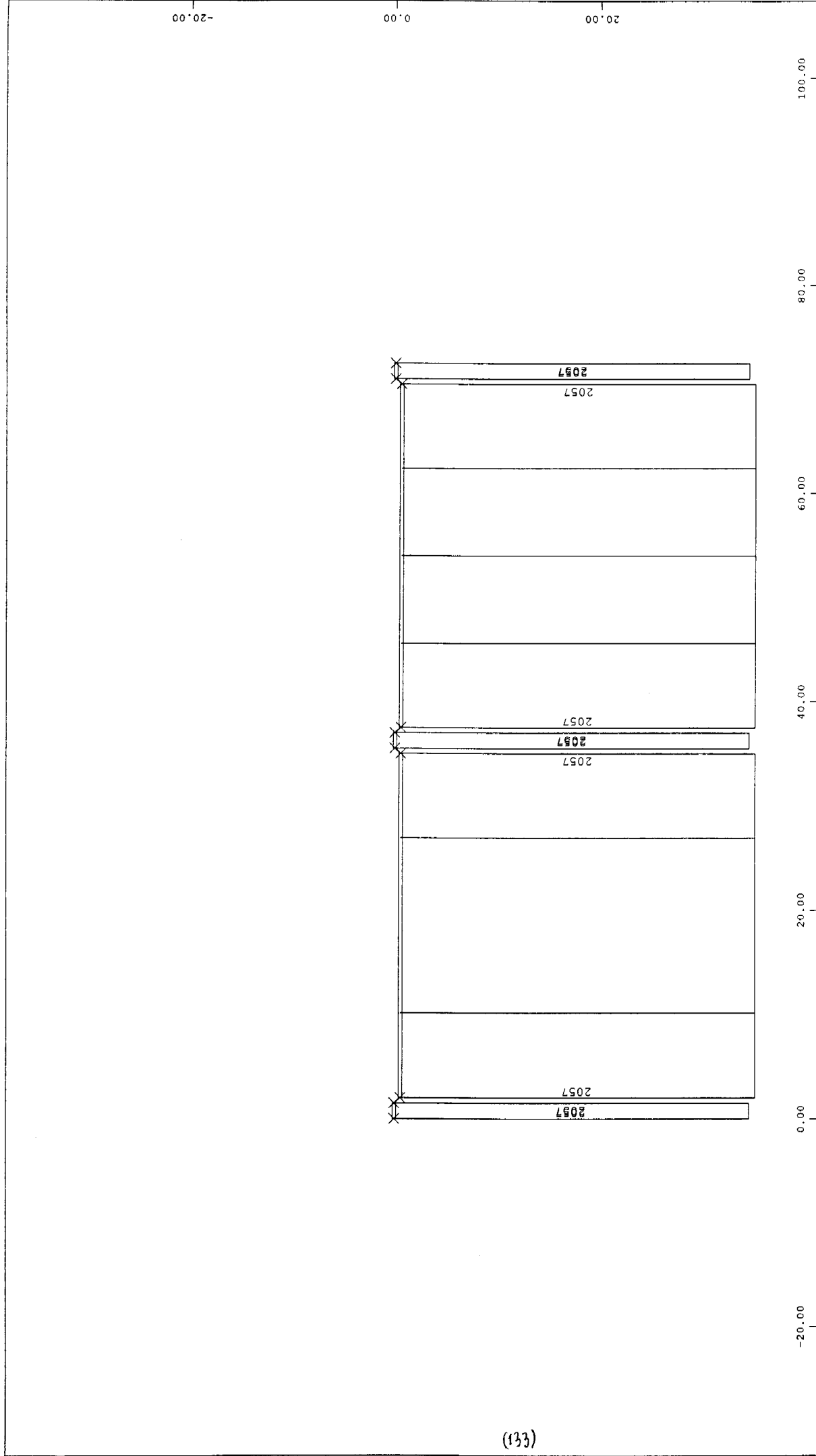


INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

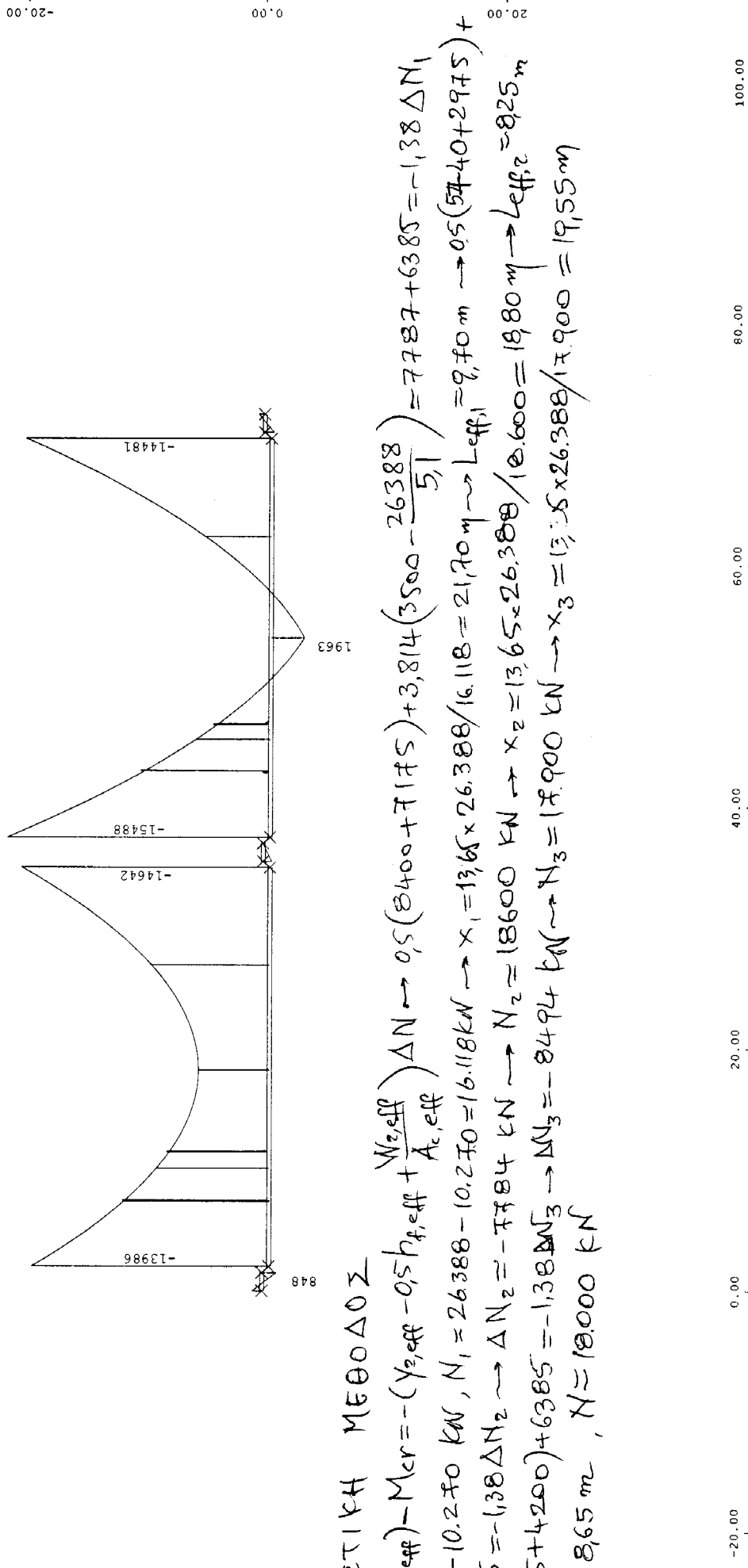
— BEAM SHEAR FORCES QZ LC 1 LOAD CASE 1 1 CM = 1000 kN

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 BEAM NORMAL FORCES LC 1 LOAD CASE 1 1 CM = 300.0 kN

M 1 : 500



ΘΑΜΙΣΤΙΚΗ ΜΕΘΟΔΟΣ

$$\Delta M(L_{eff}) - M_{cr} = -(Y_{2,eff} - 0.5 h_{p,eff} + \frac{W_{2,eff}}{A_{c,eff}}) \Delta N \rightarrow 0.5(8400 + 7175) + 3,814(3500 - \frac{26388}{5.1}) = 7787 + 6385 = -1,38 \Delta N_1$$

$$\Delta N_1 = -10.270 \text{ kN}, N_1 = 26388 - 10.270 = 16.118 \text{ kN} \rightarrow x_1 = 13.65 \times 26.388 / 16.118 = 21.70 \text{ m} \rightarrow L_{eff,1} \approx 2.70 \text{ m} \rightarrow 0.5(57.40 + 2975) + 6385 = -1.38 \Delta N_2 \rightarrow \Delta N_2 = -7784 \text{ kN} \rightarrow N_2 = 18600 \text{ kN} \rightarrow x_2 = 13.65 \times 26.388 / 18.600 = 19.80 \text{ m} \rightarrow L_{eff,2} \approx 8.25 \text{ m}$$

$$0.5(6475 + 4200) + 6385 = -1.38 \Delta N_3 \rightarrow \Delta N_3 = -8494 \text{ kN} \rightarrow N_3 = 17900 \text{ kN} \rightarrow x_3 = 13.65 \times 26.388 / 17.900 = 19.55 \text{ m}$$

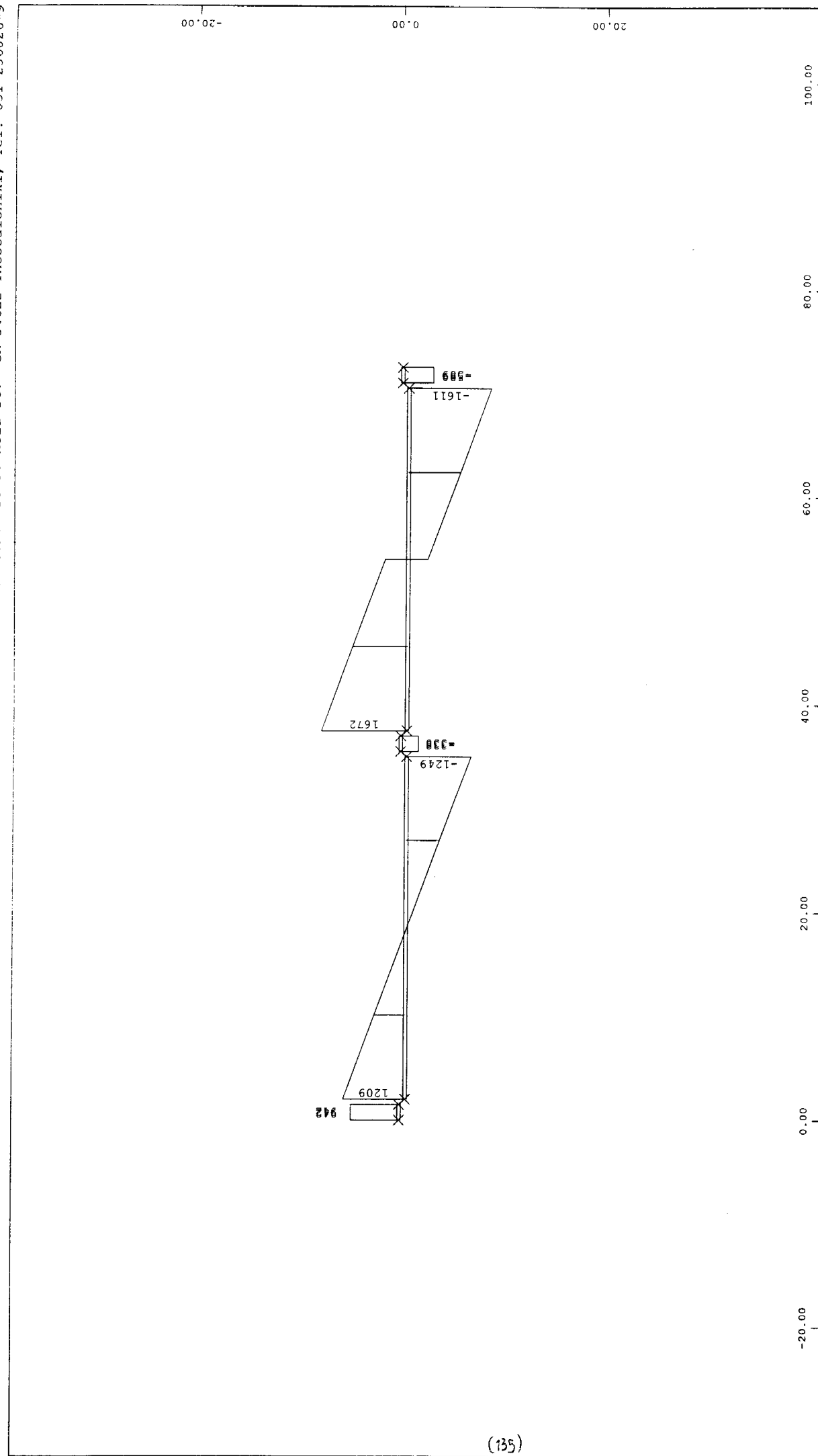
$$L_{eff} \approx 8.65 \text{ m}, N \approx 18.000 \text{ kN}$$

INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE

SECTOR OF SYSTEM, ELEMENT GROUP 0

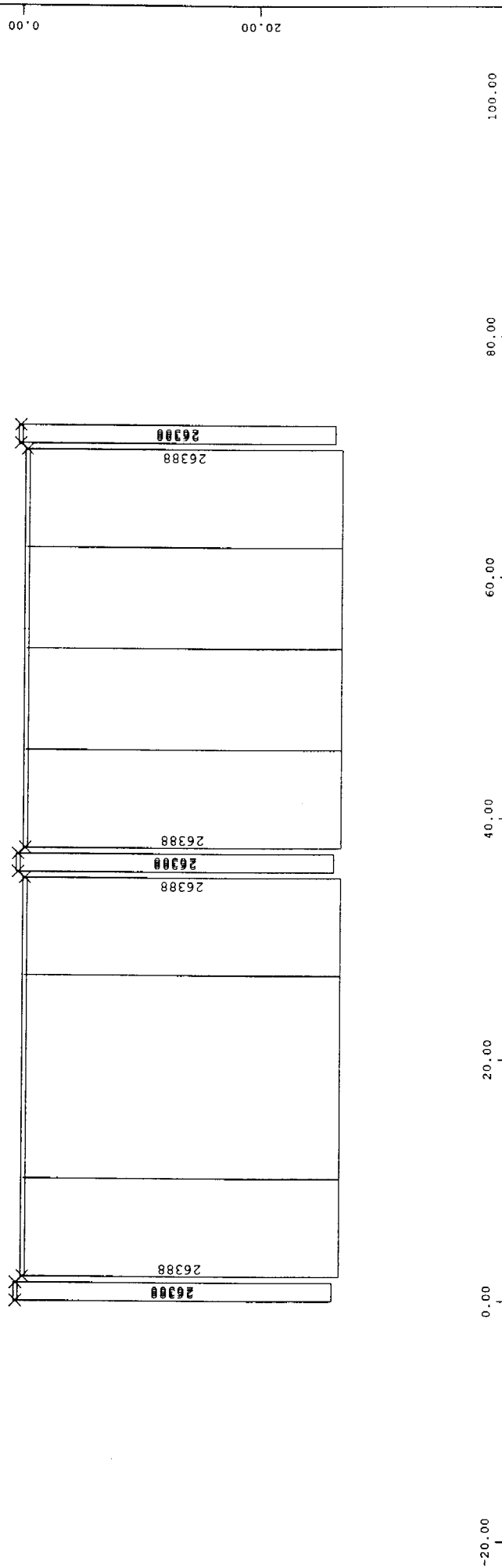
-----BEAM MOMENTS MY LC 2 LOAD CASE 2 1 CM = 3500 kNm

M 1 : 500



INTERNAL FORCED OF BRIDGE SUPERSTRUCTURE
 SECTOR OF SYSTEM, ELEMENT GROUP 0
 BEAM SHEAR FORCES QZ LC 2 LOAD CASE 2 1 CM = 1000 kN

M 1 : 500



M 1 : 500